Fast CFD Based Optimization of Coal Moving Bed Gasifier



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Coal/biomass gasifier simulation





Pilot scale gasifier at Sotacarbo, Italy

NERGY

Challenges

- Experiment takes several hours to reach steady state
- 3D CFD simulation can only simulate about several seconds to several minutes

Strategies

- Long time (several hours) 1D simulation to provide initial condition for 3D simulation
- Coarse grained DEM simulate to speed up 3d simulation and optimization

1-D: DEM3-D: coarse-grained DEM

Coarse Grained DEM





Moving Bed Gasifier Experiment^[1]



- Coal: 24kg/h, Usibelli, 1300kg/m³
- Air+H2O=57.6+3.7 at 250 Celcius
- 140Kpa, coal diameter 5mm-15mm, isolated wall, thermocouple close to center.
- Data for model validation:
- a. Syngas compositions (mole fraction, dry basis)
- b. Bed temperature profile

Proximate Analysis		Ultimate Analy	vsis (by weight)
Fixed Carbon	31.34	С	48.56
Moisture	17.64	Н	5.96
Volatiles	41	N	0.50
Ash	10.02	S	0.18
		0	17.14
Bulk Density (kg/m ³)	800	Moisture+Ash	17.64+10.02



[1] C Frau, F Ferrara, A Orsini, A Perrinau. Characterization of several kinds of coal and biomass for pyrolysis and gasification. Fuel, 2014





SOTACARBO SUSTAINABLE ENERGY RESEARCH CENTRE

Particle diameter shrinkage model



Constant density for fuel particles:



The diameter of the biomass particles is: $d_p = (\frac{6m_p}{\pi \rho})^{1/3}$



Kinetics



ſ	coal	Π				
		Categories @	Reactions &			
gas outlet		gas outlet		Forward reaction.	Backward reaction.	÷
<u> </u>			Drying 🖓	Moisture(coal) \rightarrow H ₂ O(gas) \sim		
drying zone pyrolysis zone		Pyrolysis 🗸	Volatiles → $0.6088CO + 0.3962CH_4 + 2.2469H_2 + 0.4665H_2O + 0.093tar + 0.1932CO_2 + 0.093tar + $			
		Gasification @	$Char+H_2O \rightarrow CO+H_2 e^2$	$CO + H_2 \rightarrow Char + H_2O_{e^2}$	÷	
			$Char+CO_2 \rightarrow 2CO^{\circ}$	$2CO \rightarrow Char + CO_2 C$	÷	
				$\text{Char} + 2\text{H}_2 \rightarrow \text{CH}_4 \text{P}$	$CH_4 \rightarrow Char + 2H_2 +$	÷
gas inlet combustion zone gas inlet			$\text{Char} + \text{O}_2 \rightarrow \text{CO}_2^{+2}$		÷	
	Gas phase	$CO+\frac{1}{2}O_2 \rightarrow CO_2^{\circ}$		÷		
	reactions @	$H_2 + \frac{1}{2}O_2 \rightarrow H_2O^{-\varphi}$		÷		
			$CH_4 + 2O_2 \rightarrow CO_2 + 2H_2O^{+2}$		÷	
			$CO+H_2O \rightarrow CO_2+H_2$		÷	
				$CO_2 + H_2 \rightarrow C$	C0 + H ₂ 0 ^J	÷









1D-4 hour simulation to steady state





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Solid phase mapping:

1. Solid compositions





3-D CGDEM 10min simulation







3D-CGDEM simulation results at steady state











ENERGY INSTANT STREET AND SCIENCE

Optimization Gas Products: IGCC or F-T



Integrated gasification combined cycle or the Fischer–Tropsch process



Ref: H Ghezel-Ayagh, Stephen Jolly, Dilip Patel, and David Stauffer. Solid Oxide Fuel Cell System Utilizing Syngas from Coal Gasifiers. Process Engineering of Energy Systems. dx.doi.org/10.1021/ie300841m | Ind. Eng. Chem. Res. 2013, 52, 3112–3120



Optimization Cases

Major parameters:

ER =

actual air/fuel ratio air $\frac{dH}{fuel}$ ratio for stoichiometric combustion 0.6 0.5 0.4 <u>с</u> 0.3 0.2 0.1 0 0.05 0.2 0 0.1 0.15 0.25 S/B



S/B=Water/Biomass mass ratio



Optimization For IGCC



For IGCC: the goal is to use the conserved energy, we search for the maximum heating value

LHV(MJ/m³)=CO×12.636+H2×10.798+CH4×35.818+C2H4×59.036+C2H6×63.772 Total LHV(kwh)=LHV(MJ/m³) ×Flowrate (m³/s)*1000(MJ/kJ)



Optimization for F-T



Fischer-Tropsch process:

$$(2n+1)$$
 H₂ + n CO \rightarrow C_n H_(2n+2) + n H₂C

We search for H₂/CO at 2.0





Scaleup to 1MW - Demonstration







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Multiphase Flow with Interphase eXchanges













NETL Multiphase Flow Science

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