



Meso-scale structures in bidisperse fluidized suspensions

William Holloway, Sofiane Benyahia, Christine Hrenya, and Sankaran Sundaresan

NETL Workshop on Multiphase Flow Science
Pittsburgh, PA, 2010

- Project objective
- Current status of GHD theory in MFIX
- Connection to Roadmap
- Model framework
- Test cases
- Model predictions
- Grid resolution effects
- Range of validity of kinetic theory formulation
- Summary

Project objective



Goal:

Study the segregation behavior of binary gas-solid flows in risers predicted by the kinetic theory model framework of Garzó, Hrenya, and Dufty¹ (GHD theory) with the fluid-particle drag model developed by Holloway, Yin and Sundaresan (HYS).^{2,3,4}

¹Garzó, Hrenya, and Dufty, *Phys. Rev. E*, 2007

²Holloway, Yin, and Sundaresan, *AIChE J.*, 2010

³Yin and Sundaresan, *AIChE J.*, 2009

⁴Yin and Sundaresan, *Ind. Eng. Chem. Res.*, 2008

Goal:

Study the segregation behavior of binary gas-solid flows in risers predicted by the kinetic theory model framework of Garzó, Hrenya, and Dufty¹ (GHD theory) with the fluid-particle drag model developed by Holloway, Yin and Sundaresan (HYS).^{2,3,4}

Necessitates the robust operation of HYS drag model and GHD theory in MFIX.

¹Garzó, Hrenya, and Dufty, *Phys. Rev. E*, 2007

²Holloway, Yin, and Sundaresan, *AIChE J.*, 2010

³Yin and Sundaresan, *AIChE J.*, 2009

⁴Yin and Sundaresan, *Ind. Eng. Chem. Res.*, 2008

Goal:

Study the segregation behavior of binary gas-solid flows in risers predicted by the kinetic theory model framework of Garzó, Hrenya, and Dufty¹ (GHD theory) with the fluid-particle drag model developed by Holloway, Yin and Sundaresan (HYS).^{2,3,4}

Demonstrated

Necessitates the robust operation of **HYS drag model** and GHD theory in MFIX.

¹Garzó, Hrenya, and Dufty, *Phys. Rev. E*, 2007

²Holloway, Yin, and Sundaresan, *AIChE J.*, 2010

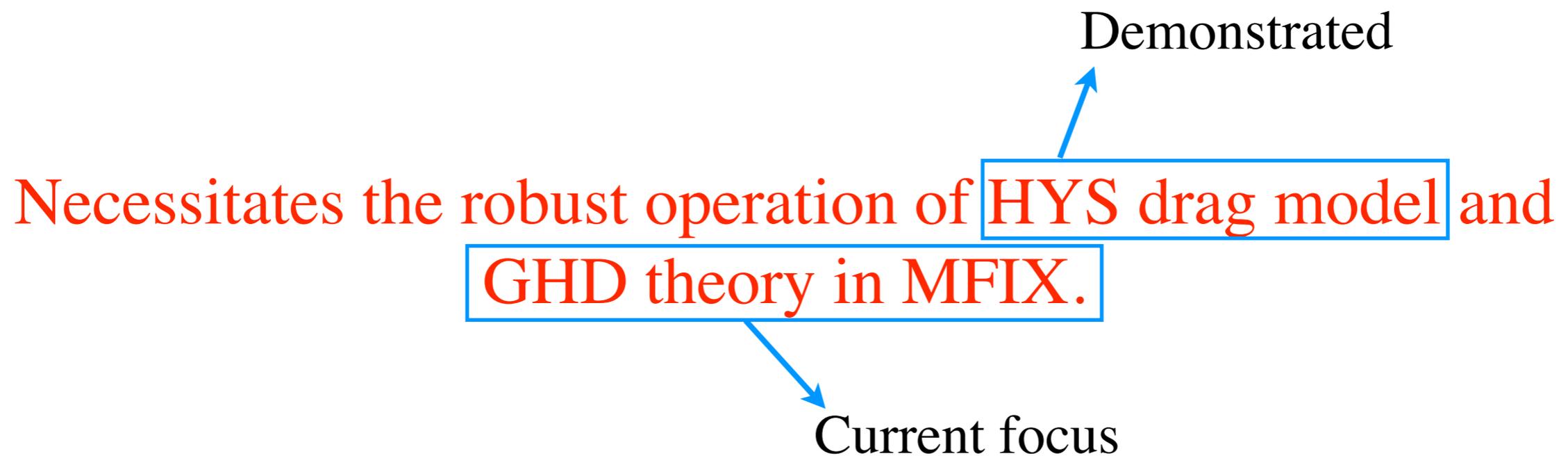
³Yin and Sundaresan, *AIChE J.*, 2009

⁴Yin and Sundaresan, *Ind. Eng. Chem. Res.*, 2008

Project objective

Goal:

Study the segregation behavior of binary gas-solid flows in risers predicted by the kinetic theory model framework of Garzó, Hrenya, and Dufty¹ (GHD theory) with the fluid-particle drag model developed by Holloway, Yin and Sundaresan (HYS).^{2,3,4}



¹Garzó, Hrenya, and Dufty, *Phys. Rev. E*, 2007

²Holloway, Yin, and Sundaresan, *AIChE J.*, 2010

³Yin and Sundaresan, *AIChE J.*, 2009

⁴Yin and Sundaresan, *Ind. Eng. Chem. Res.*, 2008

Current status of GHD theory in MFIX



Current status of GHD theory in MFIX



- GHD theory has been successfully incorporated within the MFIX framework and has been tested extensively.



- GHD theory has been successfully incorporated within the MFIX framework and has been tested extensively.
- The GHD theory implementation has operated robustly for both homogeneous and inhomogeneous gas-solid flows with binary particle size distributions (PSD).

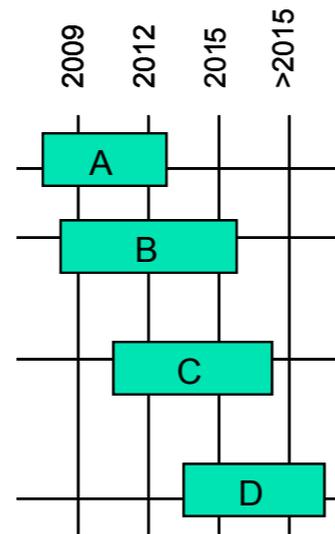


- GHD theory has been successfully incorporated within the MFIX framework and has been tested extensively.
- The GHD theory implementation has operated robustly for both homogeneous and inhomogeneous gas-solid flows with binary particle size distributions (PSD).
- Currently GHD theory implementation is only compatible with binary mixtures.

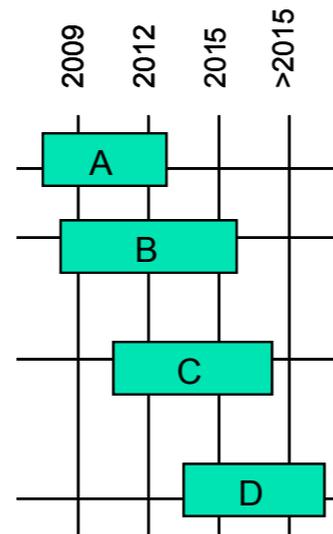


- GHD theory has been successfully incorporated within the MFIX framework and has been tested extensively.
- The GHD theory implementation has operated robustly for both homogeneous and inhomogeneous gas-solid flows with binary particle size distributions (PSD).
- Currently GHD theory implementation is only compatible with binary mixtures.
- Only two drag relations have been implemented with GHD theory at this point (namely, HYS and Wen-Yu).

Connection to Roadmap



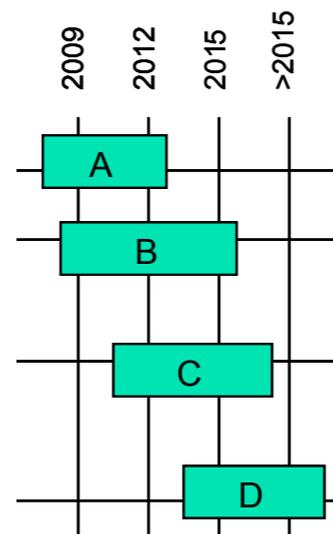
Princeton Tasks



Task 4.6:

The MFIX framework, modified to account for the new physical models will be developed as part of this work and compared to experimental data obtained from high-velocity systems.

Princeton Tasks



Roadmap

Task 4.6:

The MFIX framework, modified to account for the new physical models will be developed as part of this work and compared to experimental data obtained from high-velocity systems.

Near Term:

- Perform high-fidelity, transient 3-D multiphase flow computations with PSD (particle size distribution).
- Identify deficiencies of current models developed for gas-solid flows.

Continuum models for polydisperse flows



Continuity

$$\frac{\partial n_i}{\partial t} + \nabla \cdot (n_i \mathbf{V}) = -\frac{1}{m_i} \nabla \cdot \mathbf{j}_i$$

Continuum models for polydisperse flows

Continuity

$$\frac{\partial n_i}{\partial t} + \nabla \cdot (n_i \mathbf{V}) = -\frac{1}{m_i} \nabla \cdot \mathbf{j}_{0i}$$

Momentum

$$\rho_s \phi \left(\frac{\partial \mathbf{V}}{\partial t} + \mathbf{V} \cdot \nabla \mathbf{V} \right) = -\nabla \cdot \sigma_s + \sum_{i=1}^s n_i \mathbf{F}_i$$

$$\mathbf{j}_{0i} = -\sum_{j=1}^s \frac{m_i m_j n_j}{\rho} D_{ij} \nabla \ln(n_j) - \rho D_i^T \nabla \ln(T) - \sum_{j=1}^s D_{ij}^F \mathbf{F}_j$$

Continuum models for polydisperse flows

Continuity

$$\frac{\partial n_i}{\partial t} + \nabla \cdot (n_i \mathbf{V}) = -\frac{1}{m_i} \nabla \cdot \mathbf{j}_{0i}$$

Momentum

$$\rho_s \phi \left(\frac{\partial \mathbf{V}}{\partial t} + \mathbf{V} \cdot \nabla \mathbf{V} \right) = -\nabla \cdot \sigma_s + \sum_{i=1}^s n_i \mathbf{F}_i$$

$$\mathbf{j}_{0i} = -\sum_{j=1}^s \frac{m_i m_j n_j}{\rho} D_{ij} \nabla \ln(n_j) - \rho D_i^T \nabla \ln(T) - \sum_{j=1}^s D_{ij}^F \mathbf{F}_j$$

Fluctuating energy

$$\frac{3n}{2} \left(\frac{\partial T}{\partial t} + \mathbf{V} \cdot \nabla T \right) = -\nabla \cdot \mathbf{q} - \sigma_s : \nabla \mathbf{V} - \frac{3n\zeta T}{2} + \frac{3T}{2} \sum_{i=1}^s \frac{1}{m_i} \nabla \cdot \mathbf{j}_{0i} + \sum_{i=1}^s \frac{\mathbf{F}_i \cdot \mathbf{j}_{0i}}{m_i}$$

$$\mathbf{q} = -\lambda \nabla T - \left(\sum_{i=1}^s \sum_{j=1}^s T^2 D_{q,ij} \nabla \ln(n_j) + L_{ij} \mathbf{F}_j \right)$$

External forces in polydisperse systems



$$\mathbf{j}_i = - \sum_{j=1}^s \frac{m_i m_j n_j}{\rho} D_{ij} \nabla \ln(n_j) - \rho D_i^T \nabla \ln(T) - \sum_{j=1}^s D_{ij}^F \mathbf{F}_j$$

External forces in polydisperse systems



$$\mathbf{j}_{0i} = - \sum_{j=1}^s \frac{m_i m_j n_j}{\rho} D_{ij} \nabla \ln(n_j) - \rho D_i^T \nabla \ln(T) - \sum_{j=1}^s D_{ij}^F \mathbf{F}_j$$
$$\mathbf{F}_j = m_j \mathbf{g} + V_j \nabla P_g + \mathbf{F}_{Dj}$$

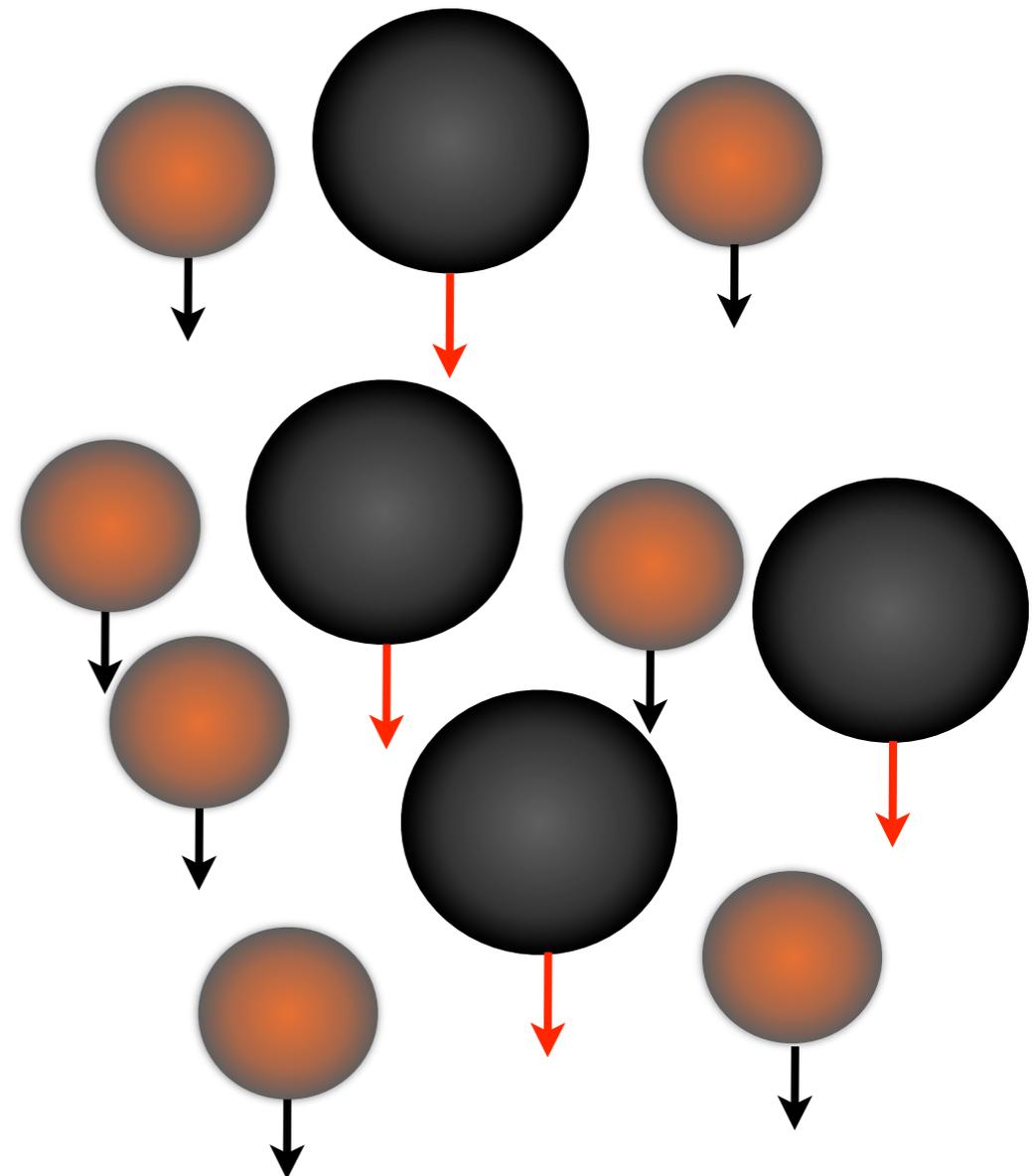
External forces in polydisperse systems

$$\mathbf{j}_{0i} = - \sum_{j=1}^s \frac{m_i m_j n_j}{\rho} D_{ij} \nabla \ln(n_j) - \rho D_i^T \nabla \ln(T) - \sum_{j=1}^s D_{ij}^F \mathbf{F}_j$$

$$\mathbf{F}_j = m_j \mathbf{g} + V_j \nabla P_g + \mathbf{F}_{Dj}$$

Fluid-particle drag model (HYS):^{2,3,4}

$$\mathbf{F}_{Dj} = - \frac{\beta_j}{n_j} (\mathbf{V}_j - \mathbf{V}_g)$$



²Holloway, Yin, and Sundaresan, *AIChE J.*, 2010

³Yin and Sundaresan, *AIChE J.*, 2009

⁴Yin and Sundaresan, *Ind. Eng. Chem. Res.*, 2008

External forces in polydisperse systems

$$\mathbf{j}_{0i} = - \sum_{j=1}^s \frac{m_i m_j n_j}{\rho} D_{ij} \nabla \ln(n_j) - \rho D_i^T \nabla \ln(T) - \sum_{j=1}^s D_{ij}^F \mathbf{F}_j$$

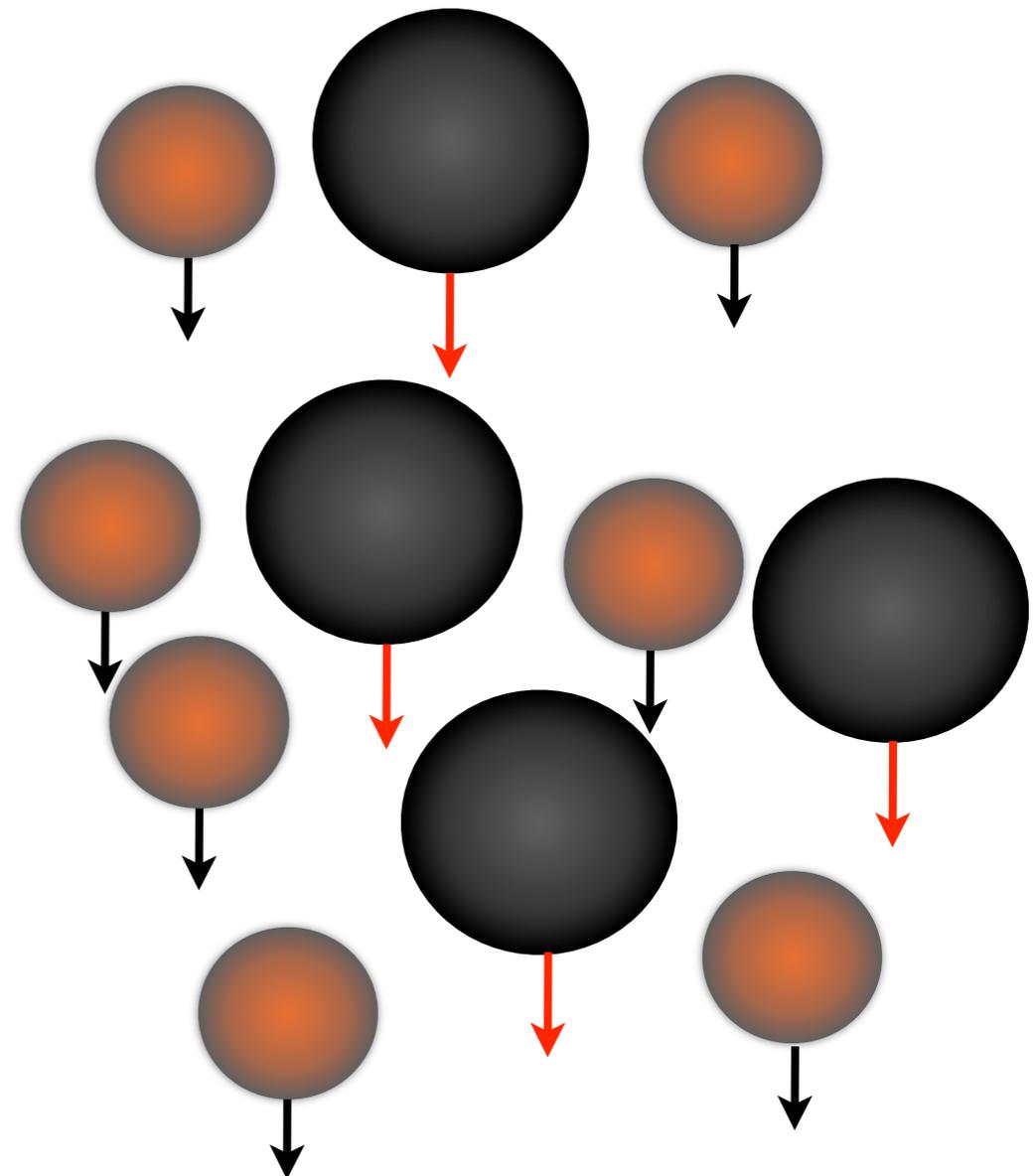
$$\mathbf{F}_j = m_j \mathbf{g} + V_j \nabla P_g + \mathbf{F}_{Dj}$$

Fluid-particle drag model (HYS):^{2,3,4}

$$\mathbf{F}_{Dj} = - \frac{\beta_j}{n_j} (\mathbf{V}_j - \mathbf{V}_g) - \sum_{i \neq j}^s \frac{\beta_{ji}}{n_j} (\mathbf{V}_i - \mathbf{V}_j)$$

$$\beta_{ji} = - \frac{2\alpha \phi_i \phi_j}{\frac{\phi_i}{\beta_i} + \frac{\phi_j}{\beta_j}}$$

Off-diagonal friction coefficient



²Holloway, Yin, and Sundaresan, *AIChE J.*, 2010

³Yin and Sundaresan, *AIChE J.*, 2009

⁴Yin and Sundaresan, *Ind. Eng. Chem. Res.*, 2008

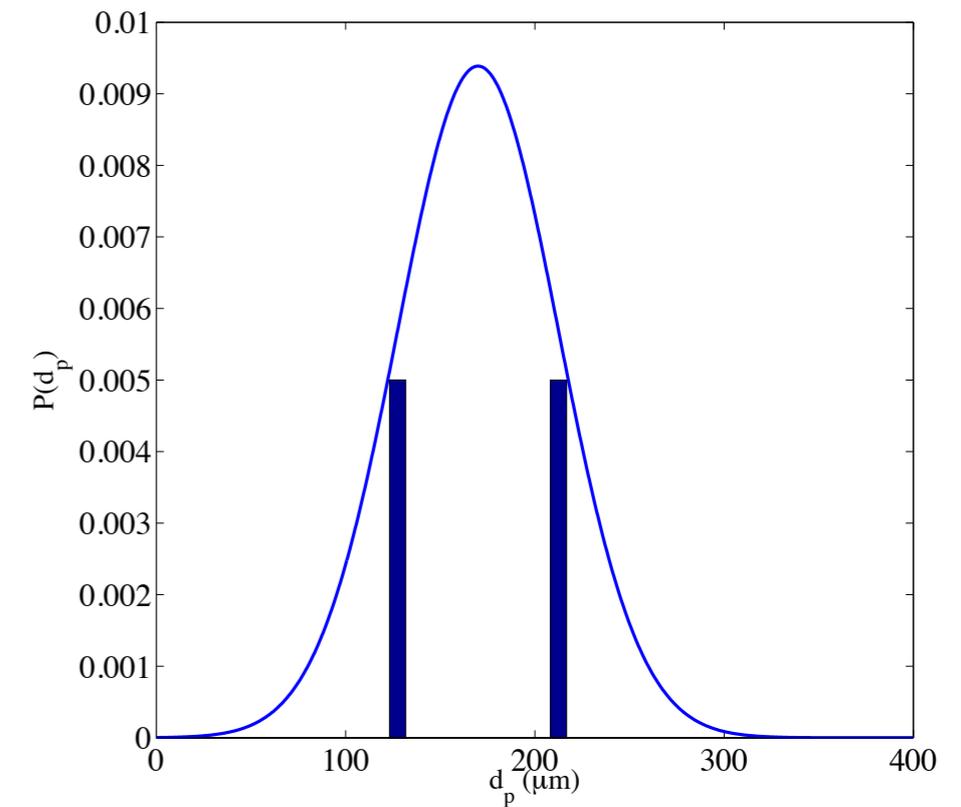
Test cases



Broad PSD

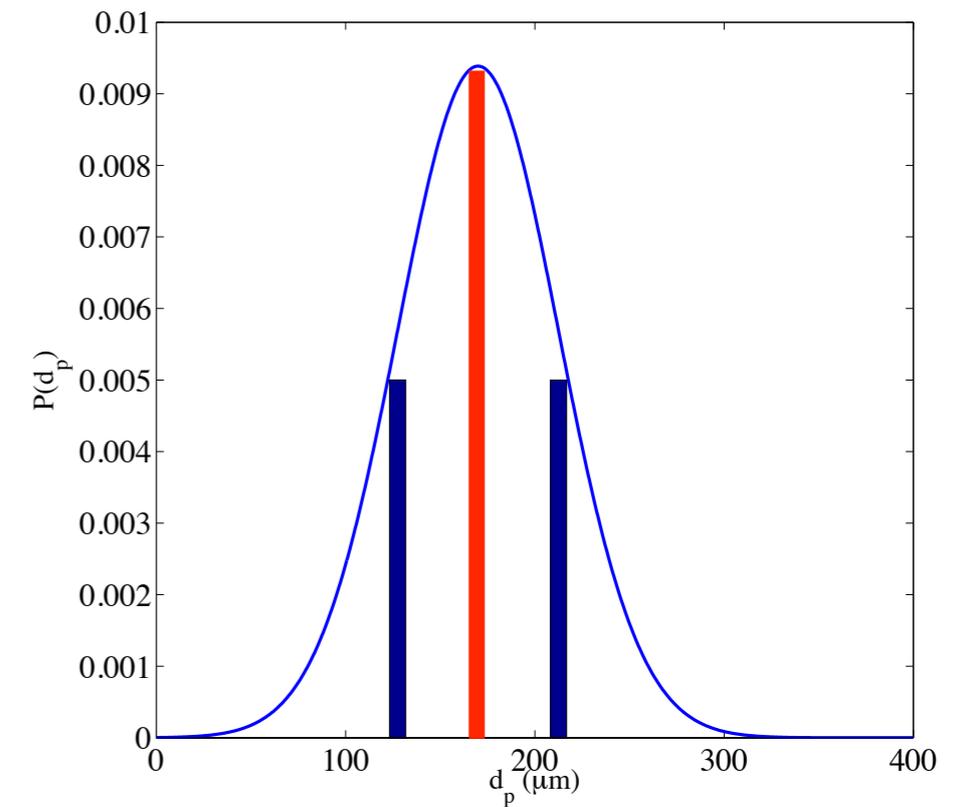
Broad PSD

- Binary approximation
 - $d_1 = 212.5 \mu\text{m}$, $d_2 = 127.5 \mu\text{m}$
 - $\phi = 0.15$



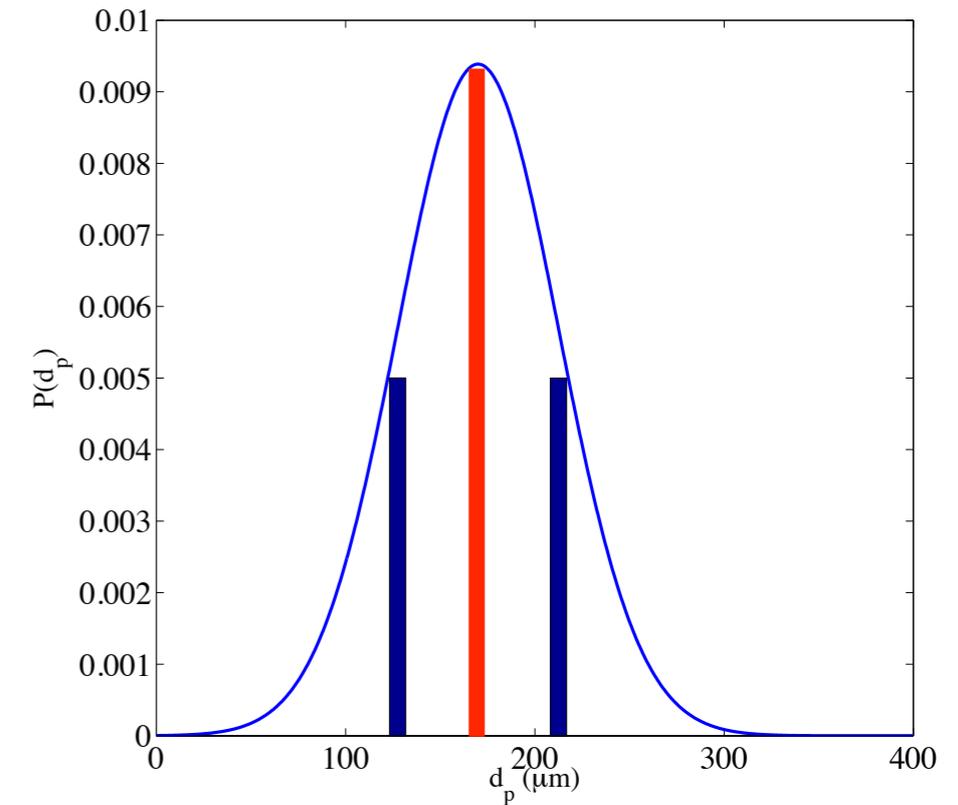
Broad PSD

- Binary approximation
 - $d_1 = 212.5 \mu\text{m}$, $d_2 = 127.5 \mu\text{m}$
 - $\phi = 0.15$
- Monodisperse approximation
 - $d = 170 \mu\text{m}$
 - $\phi = 0.15$

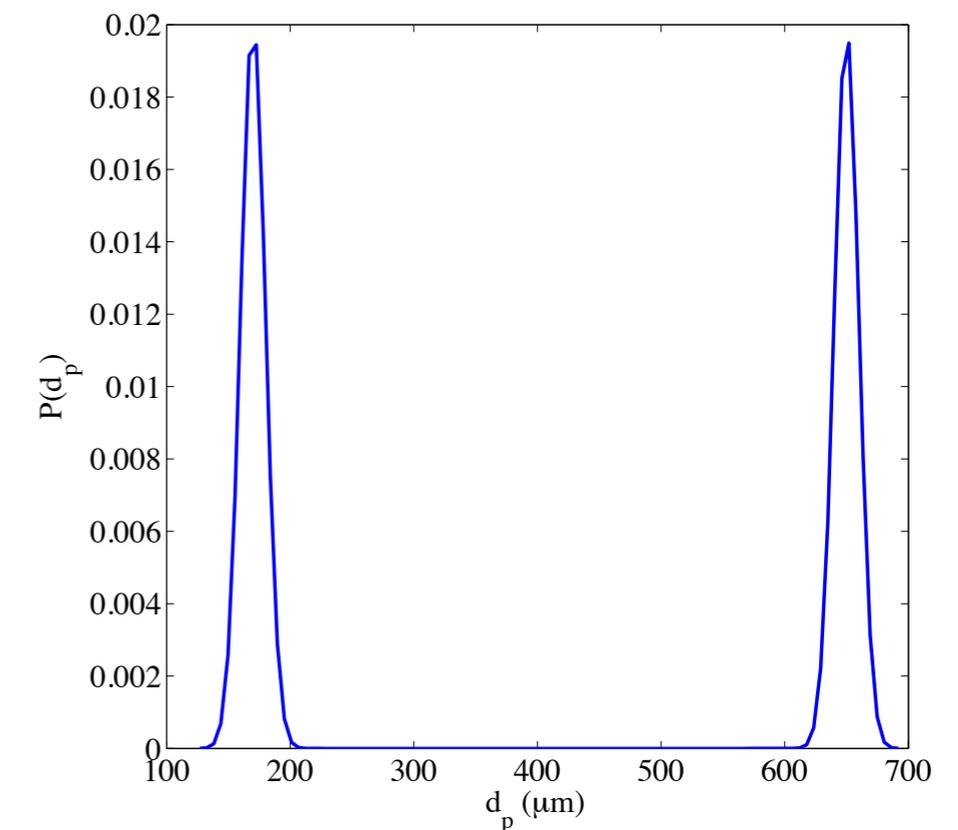


Broad PSD

- Binary approximation
 - $d_1 = 212.5 \mu\text{m}$, $d_2 = 127.5 \mu\text{m}$
 - $\phi = 0.15$
- Monodisperse approximation
 - $d = 170 \mu\text{m}$
 - $\phi = 0.15$

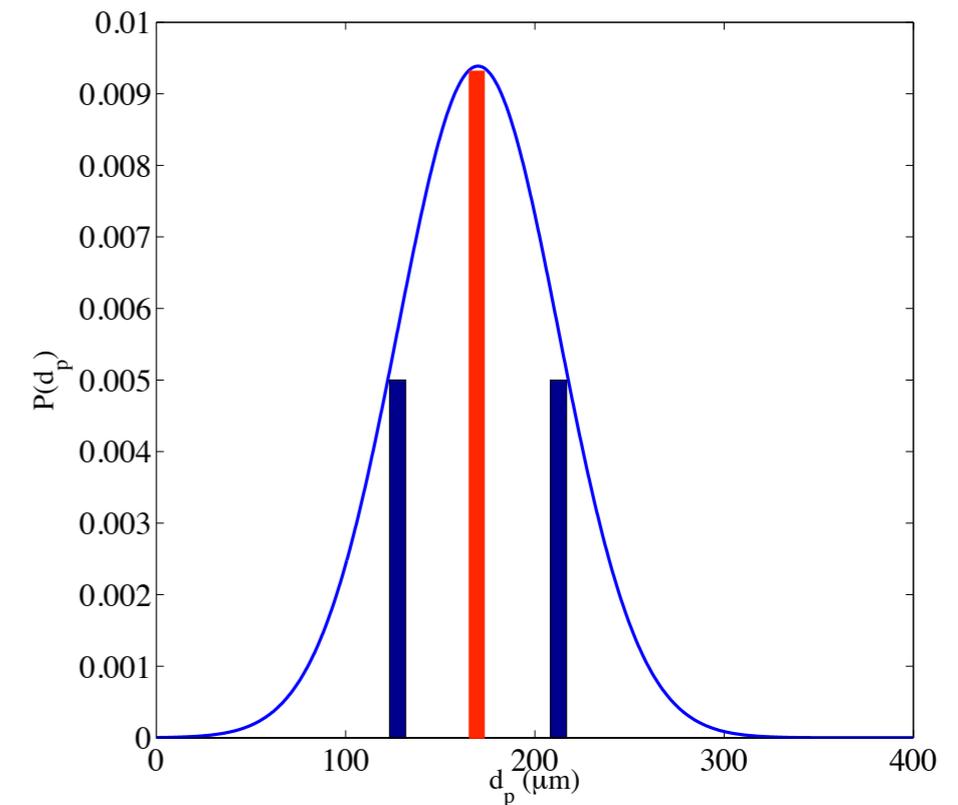


Bimodal PSD with disparate size ratio



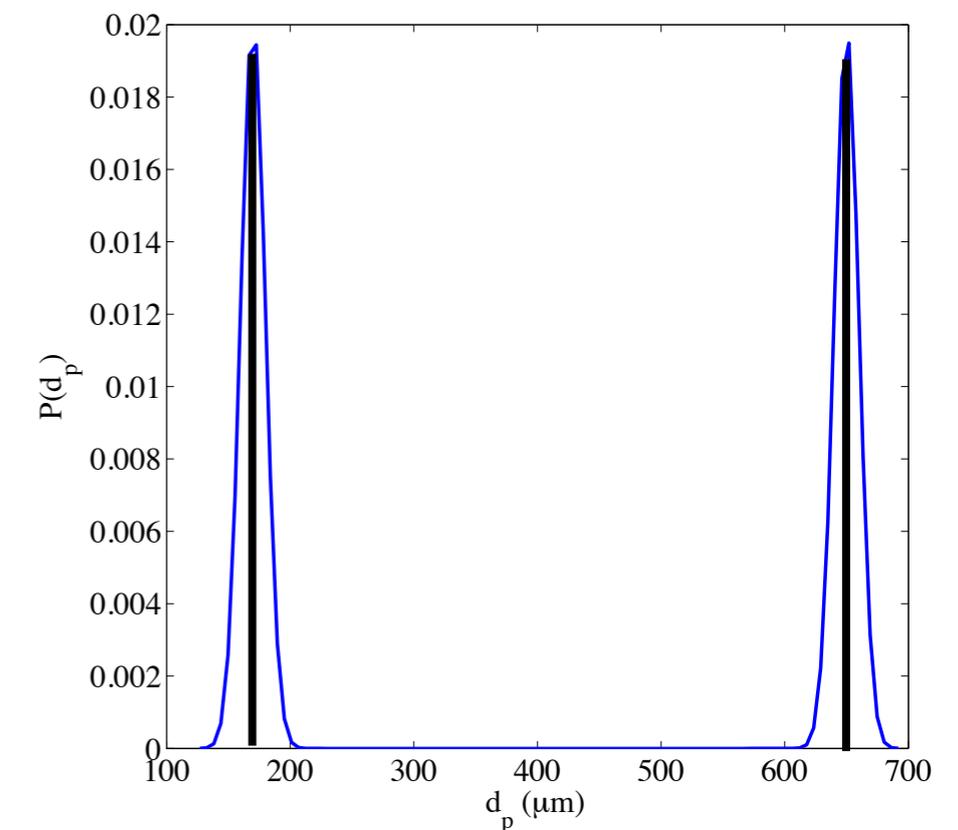
Broad PSD

- Binary approximation
 - $d_1 = 212.5 \mu\text{m}$, $d_2 = 127.5 \mu\text{m}$
 - $\phi = 0.15$
- Monodisperse approximation
 - $d = 170 \mu\text{m}$
 - $\phi = 0.15$



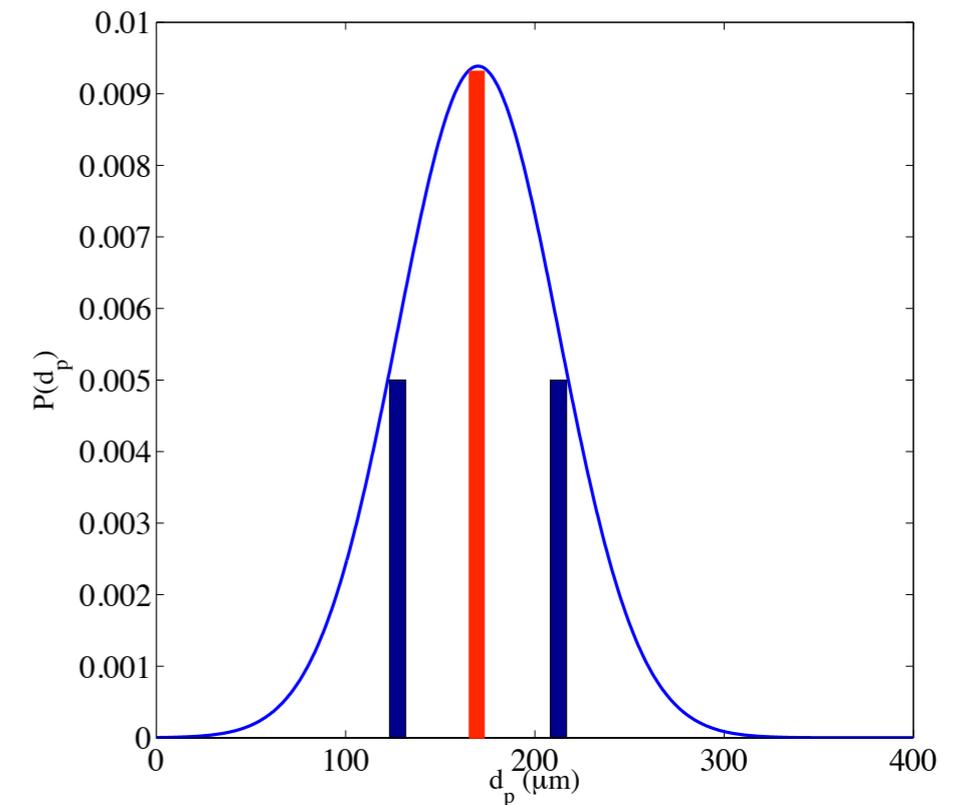
Bimodal PSD with disparate size ratio

- Binary approximation
 - $d_1 = 650 \mu\text{m}$, $d_2 = 170 \mu\text{m}$
 - $\phi = 0.15$



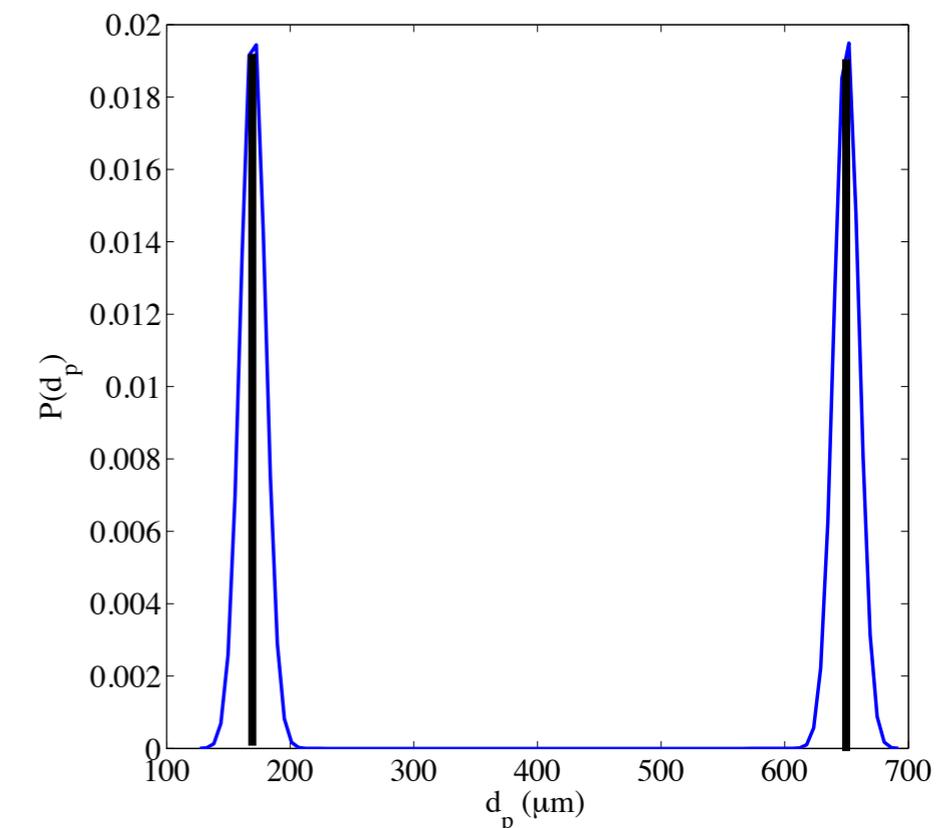
Broad PSD

- Binary approximation
 - $d_1 = 212.5 \mu\text{m}$, $d_2 = 127.5 \mu\text{m}$
 - $\phi = 0.15$
- Monodisperse approximation
 - $d = 170 \mu\text{m}$
 - $\phi = 0.15$



Bimodal PSD with disparate size ratio

- Binary approximation
 - $d_1 = 650 \mu\text{m}$, $d_2 = 170 \mu\text{m}$
 - $\phi = 0.15$
- Monodisperse approximation
 - $d = 270 \mu\text{m}$
 - $\phi = 0.15$



Model predictions



Broad PSD ($e = 0.95$)

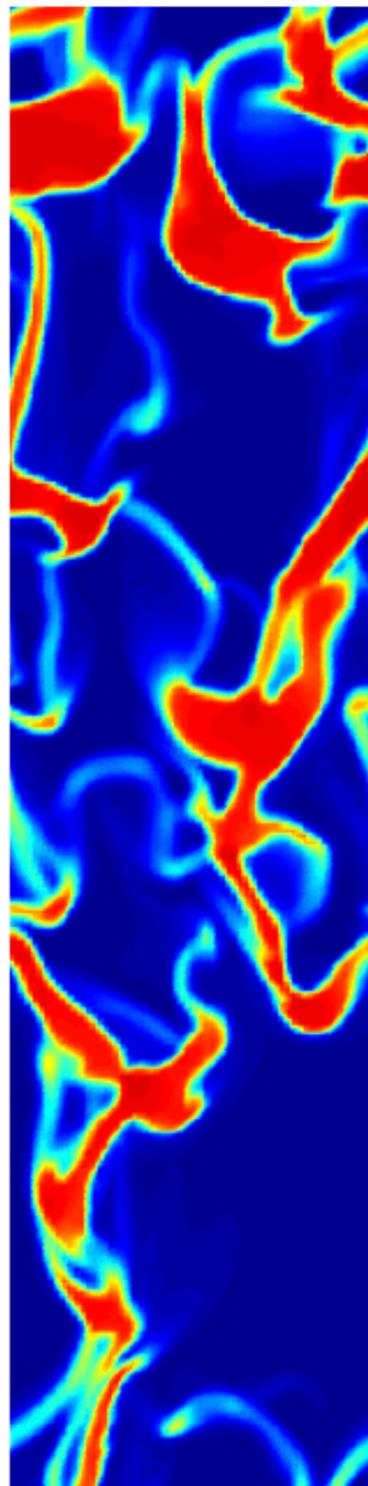
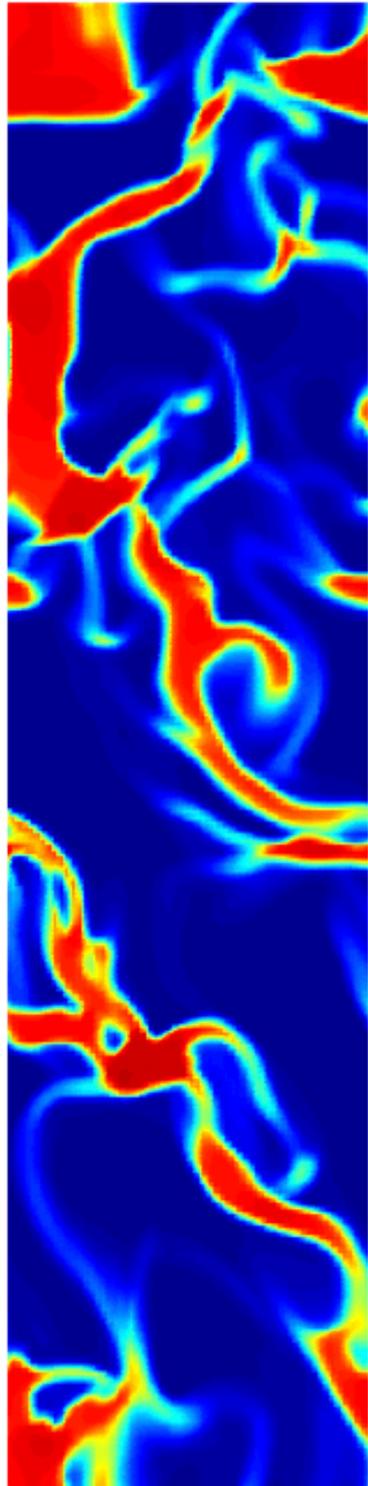
Model predictions



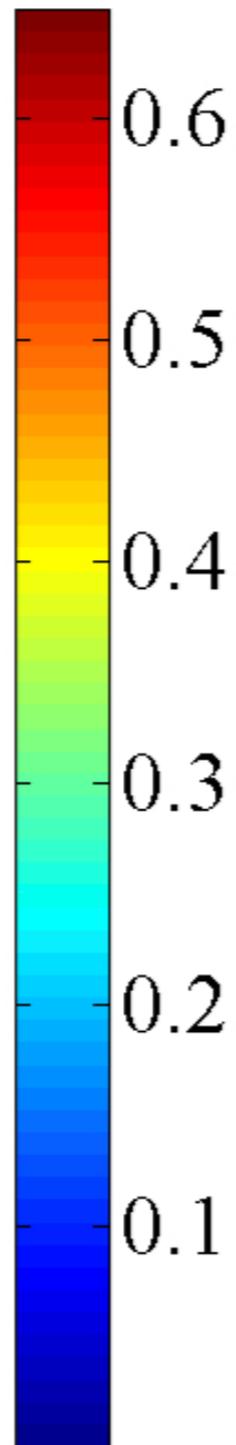
Broad PSD ($e = 0.95$)

Bidisperse

Monodisperse



ϕ



MFIX simulations:

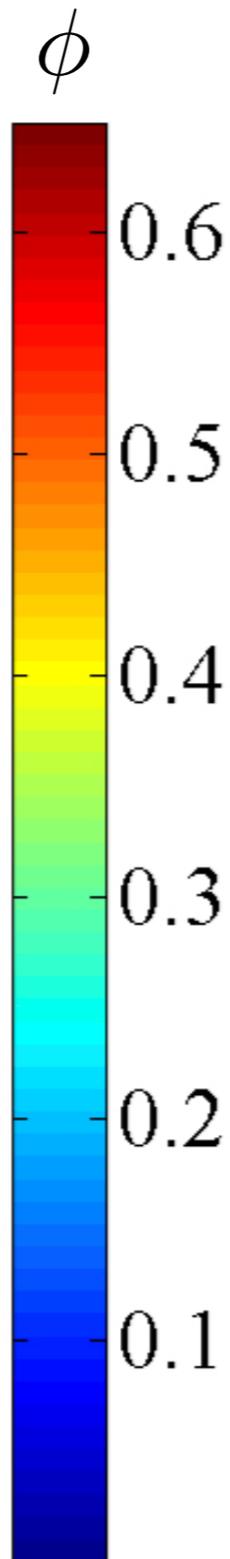
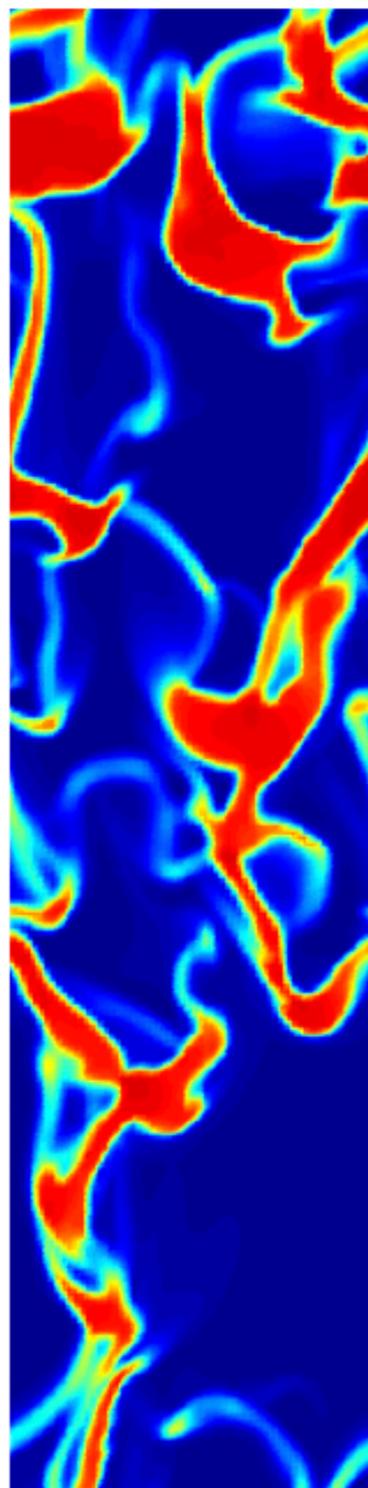
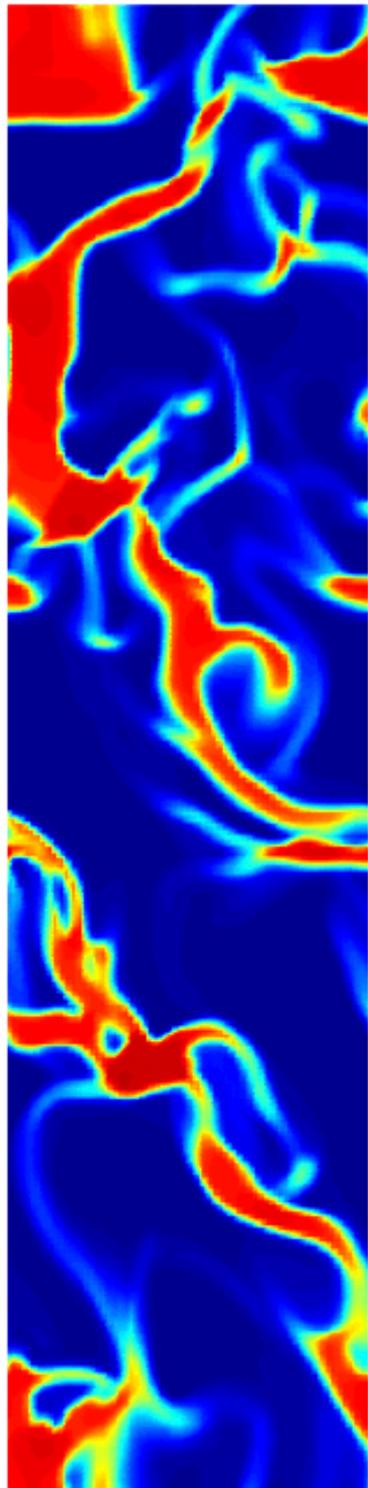
- $d_1=212.5 \mu m, d_2=127.5 \mu m$
- $\langle \phi_1 \rangle = 0.125, \langle \phi_2 \rangle = 0.025$
- Doubly periodic
- 16 cm x 64 cm
- 0.25 cm grids

Model predictions

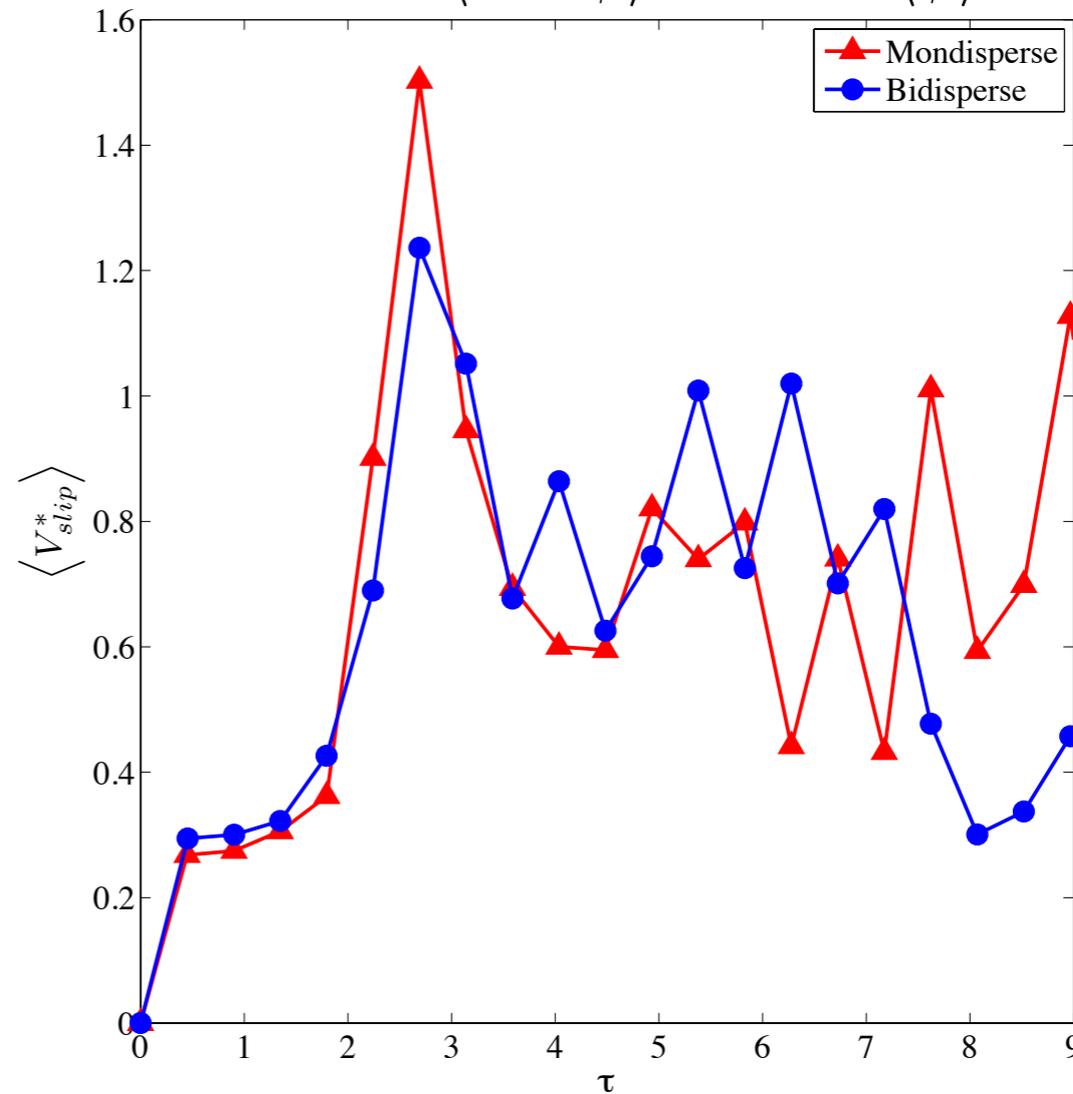
Broad PSD ($e = 0.95$)

Bidisperse

Monodisperse



$$\langle V_{slip} \rangle = \frac{\langle (1 - \phi) V_g \rangle}{\langle 1 - \phi \rangle} - \frac{\langle \phi V_{s_{mix}} \rangle}{\langle \phi \rangle}$$



MFIX simulations:

- $d_1 = 212.5 \mu m, d_2 = 127.5 \mu m$
- $\langle \phi_1 \rangle = 0.125, \langle \phi_2 \rangle = 0.025$
- Doubly periodic
- 16 cm x 64 cm
- 0.25 cm grids

$$\langle V_{slip}^* \rangle = \frac{\langle V_{slip} \rangle}{V_t}$$

$$\tau = t \frac{g}{V_t}$$

Model predictions



Broad PSD ($e = 0.99$)

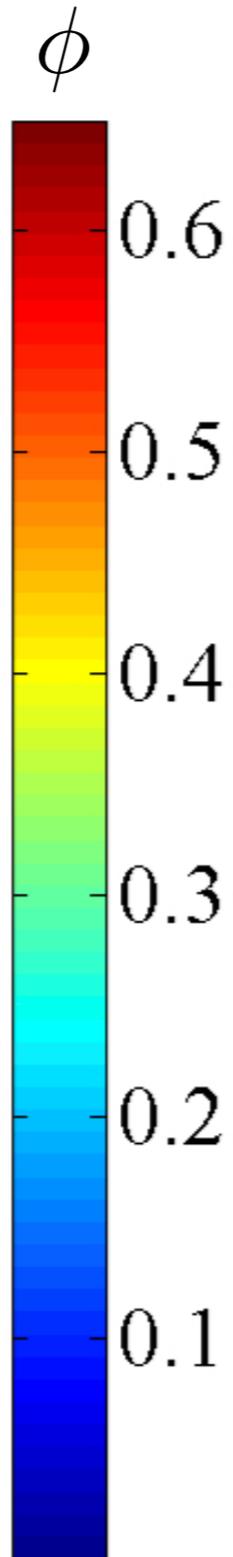
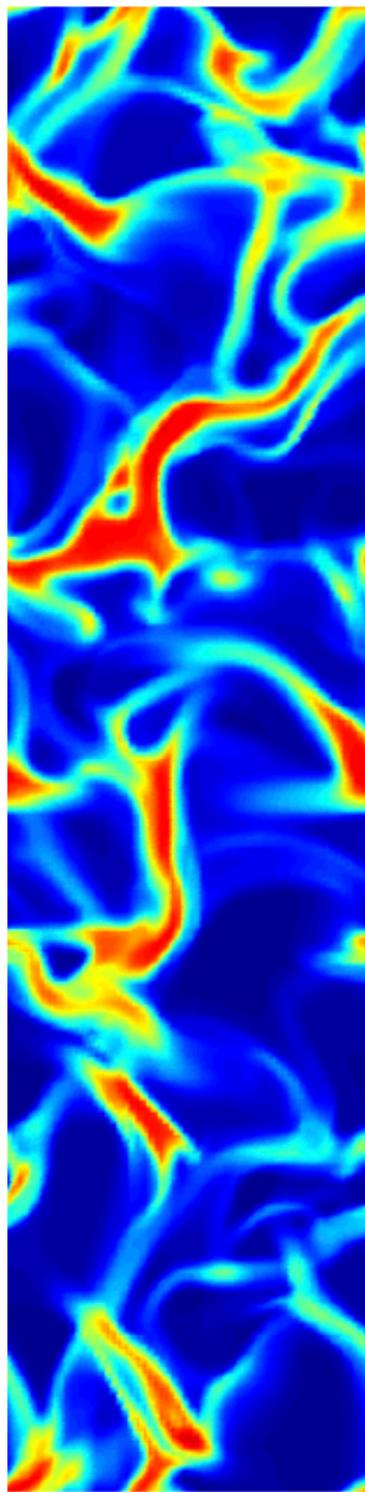
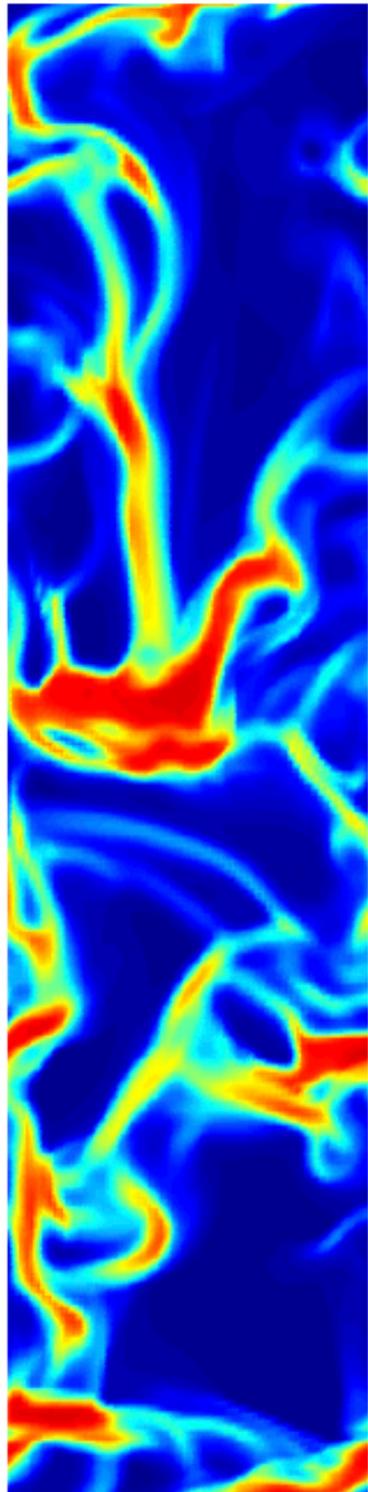
Model predictions



Broad PSD ($e = 0.99$)

Bidisperse

Monodisperse



MFIX simulations:

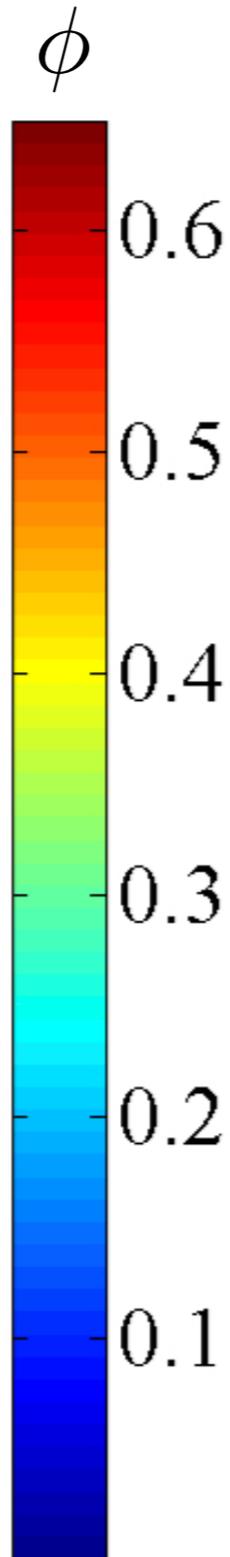
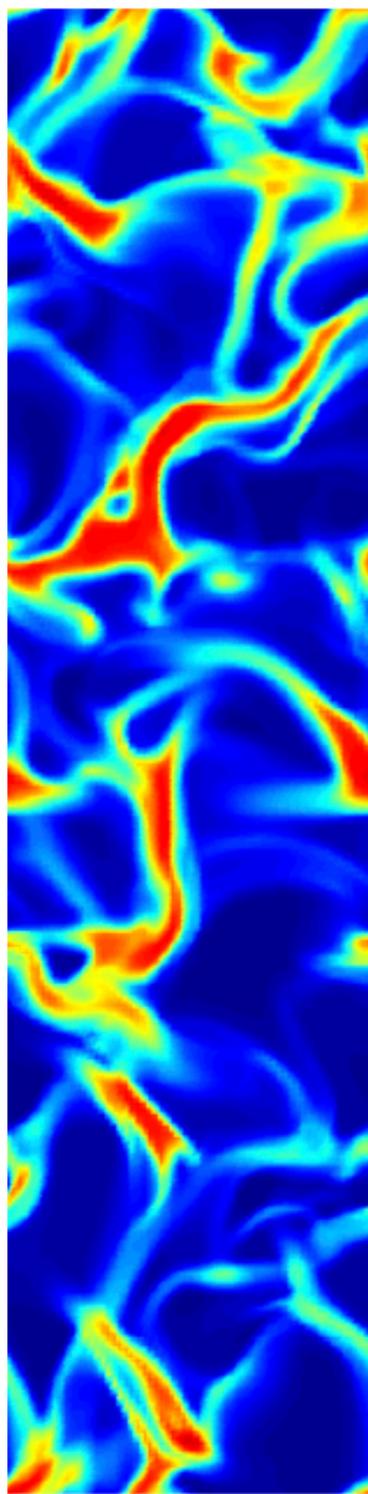
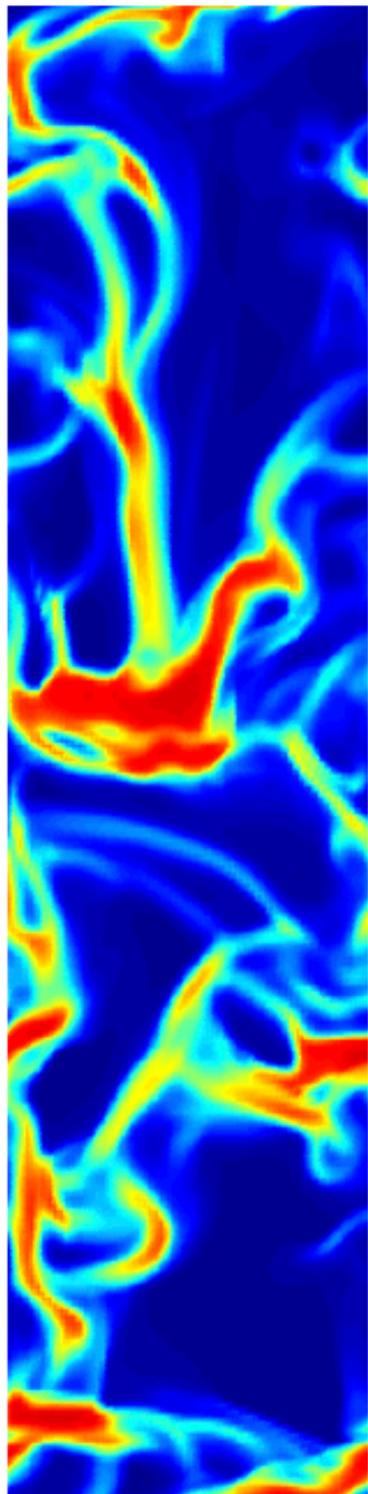
- $d_1=212.5 \mu m, d_2=127.5 \mu m$
- $\langle \phi_1 \rangle = 0.125, \langle \phi_2 \rangle = 0.025$
- Doubly periodic
- 16 cm x 64 cm
- 0.25 cm grids

Model predictions

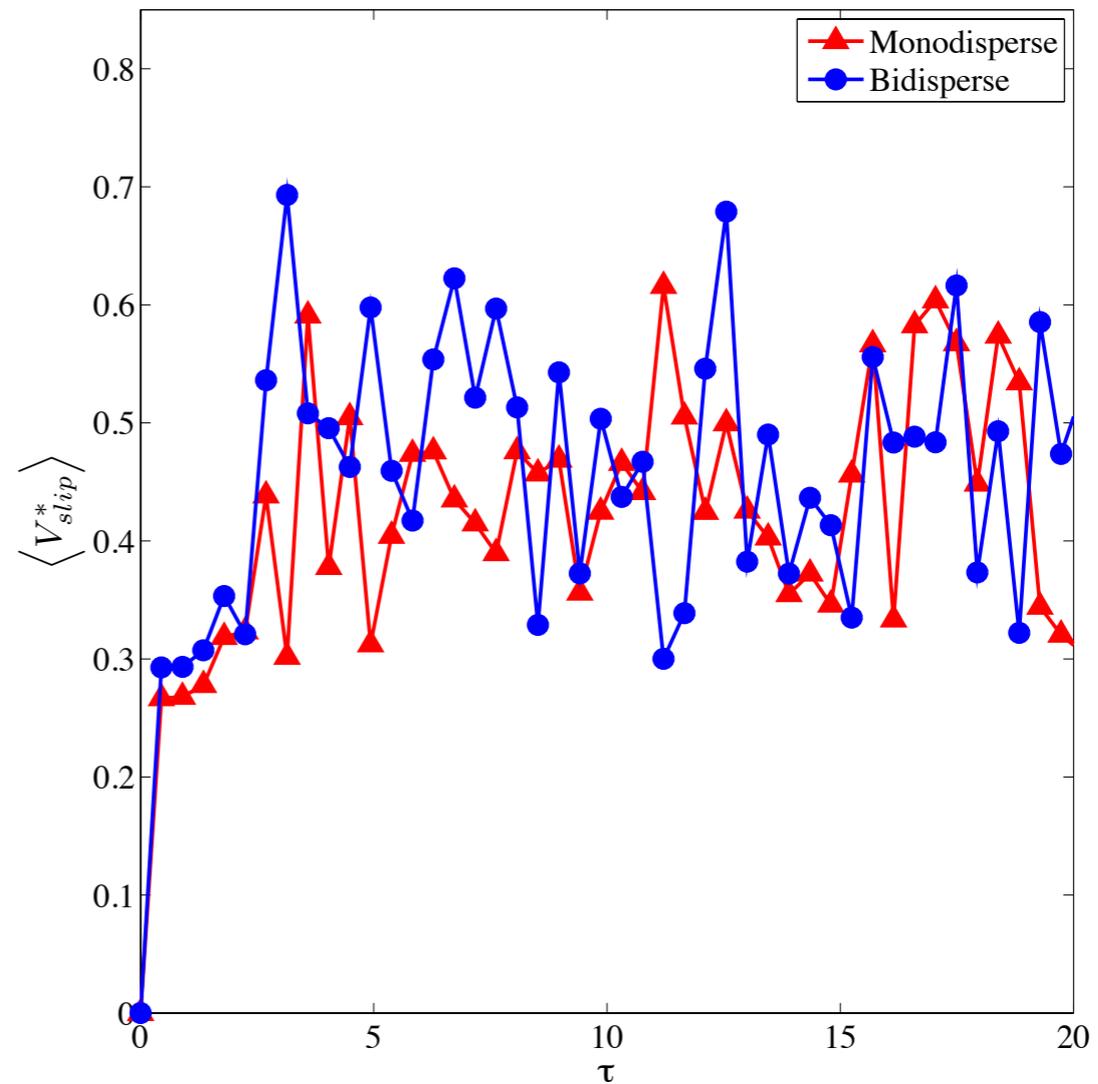
Broad PSD ($e = 0.99$)

Bidisperse

Monodisperse



$$\langle V_{slip} \rangle = \frac{\langle (1 - \phi) V_g \rangle}{\langle 1 - \phi \rangle} - \frac{\langle \phi V_{s_{mix}} \rangle}{\langle \phi \rangle}$$



MFIX simulations:

- $d_1 = 212.5 \mu m, d_2 = 127.5 \mu m$
- $\langle \phi_1 \rangle = 0.125, \langle \phi_2 \rangle = 0.025$
- Doubly periodic
- 16 cm x 64 cm
- 0.25 cm grids

$$\langle V_{slip}^* \rangle = \frac{\langle V_{slip} \rangle}{V_t}$$

$$\tau = t \frac{g}{V_t}$$

Model prediction: Volume fraction ratios

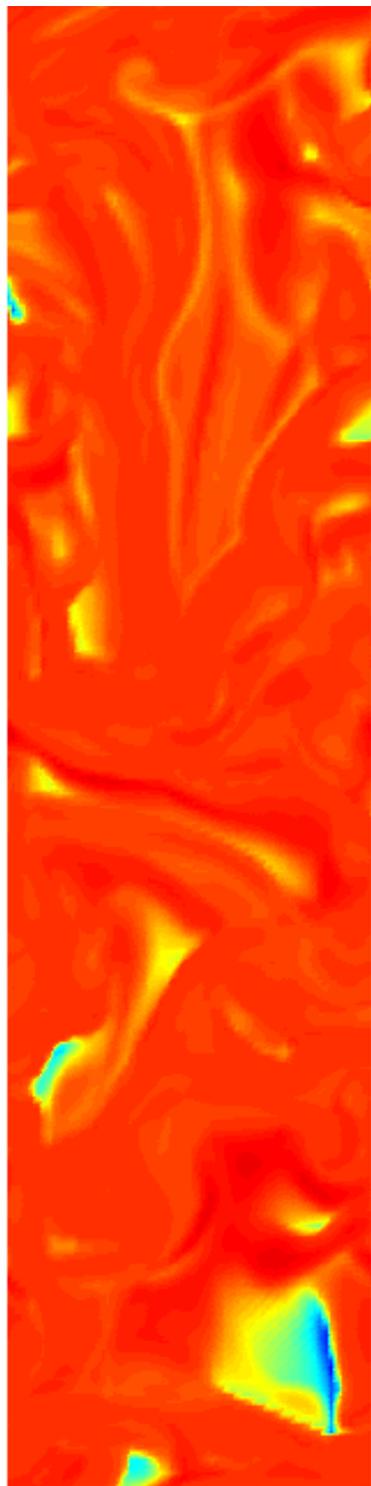


Broad PSD

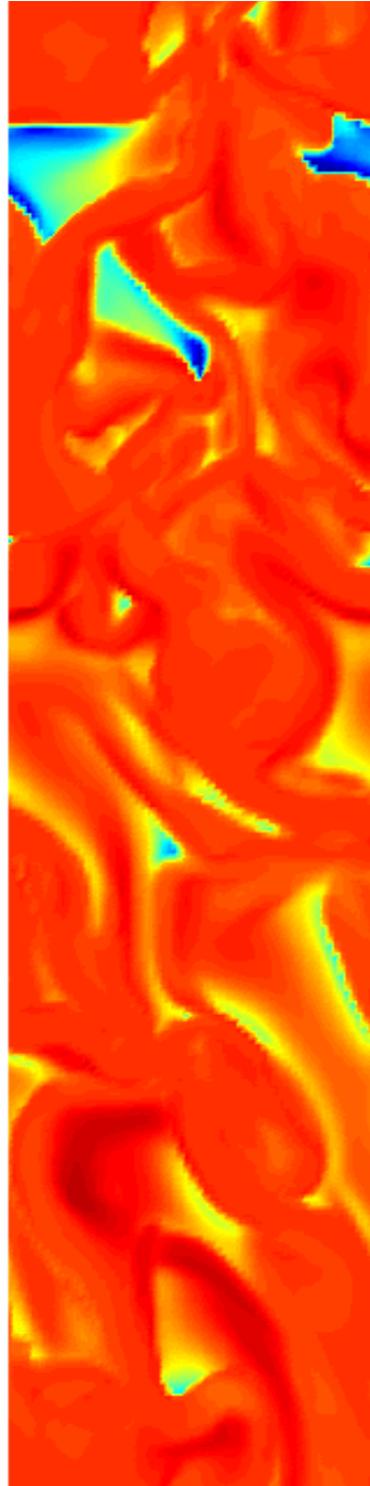
Model prediction: Volume fraction ratios

Broad PSD

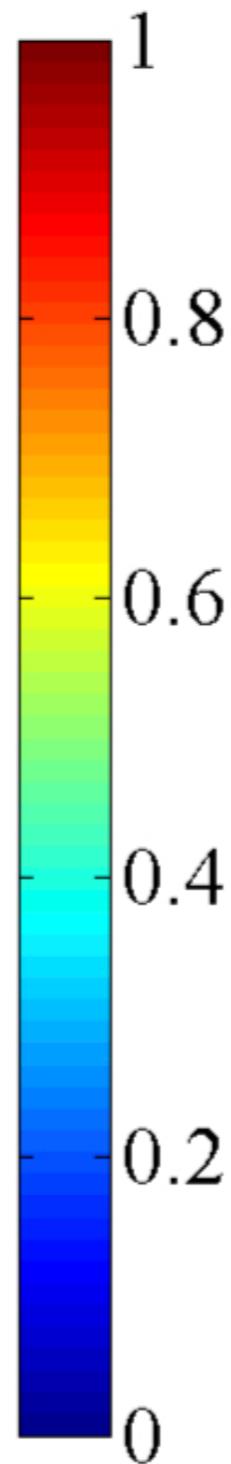
$e = 0.99$



$e = 0.95$



ϕ_1/ϕ



MFIX simulations:

- GHD theory
- HYS drag model
- $d_1=212.5 \mu m, d_2=127.5 \mu m$
- $\langle \phi_1 \rangle = 0.125, \langle \phi_2 \rangle = 0.025$
- Doubly periodic
- 16 cm x 64 cm

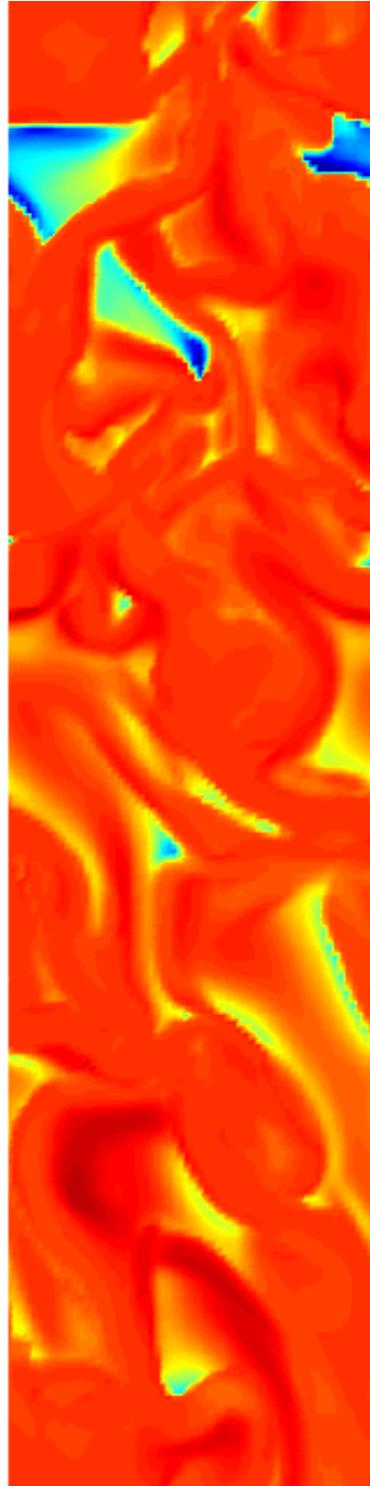
Model prediction: Volume fraction ratios

Broad PSD

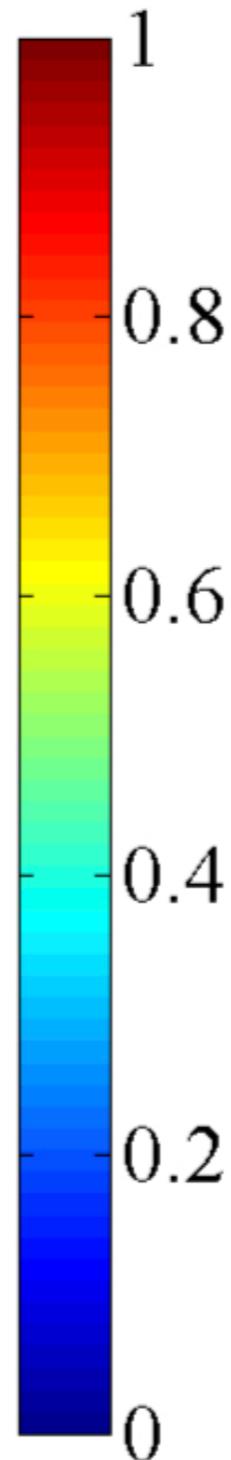
$e = 0.99$



$e = 0.95$



ϕ_1/ϕ



MFIX simulations:

- GHD theory
- HYS drag model
- $d_1=212.5 \mu\text{m}$, $d_2=127.5 \mu\text{m}$
- $\langle\phi_1\rangle=0.125$, $\langle\phi_2\rangle=0.025$
- Doubly periodic
- 16 cm x 64 cm

Broad PSD maintains a very tight distribution of volume fraction ratio throughout the flow domain for both coefficients of restitution.

Model predictions



Bimodal PSD ($e = 0.95$)

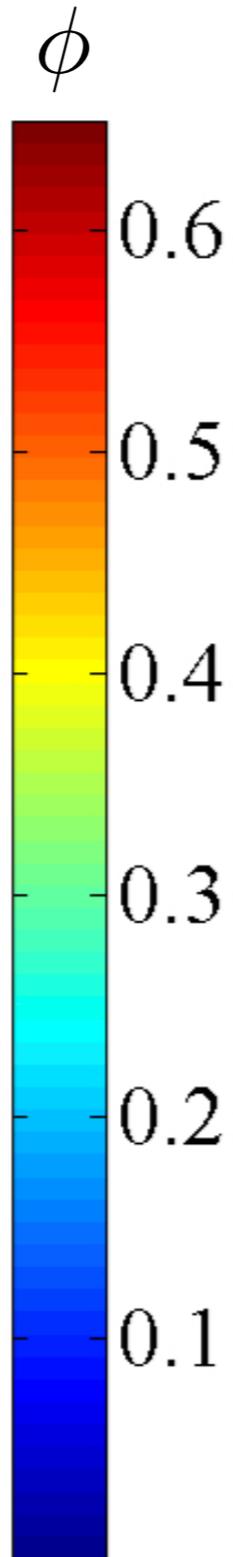
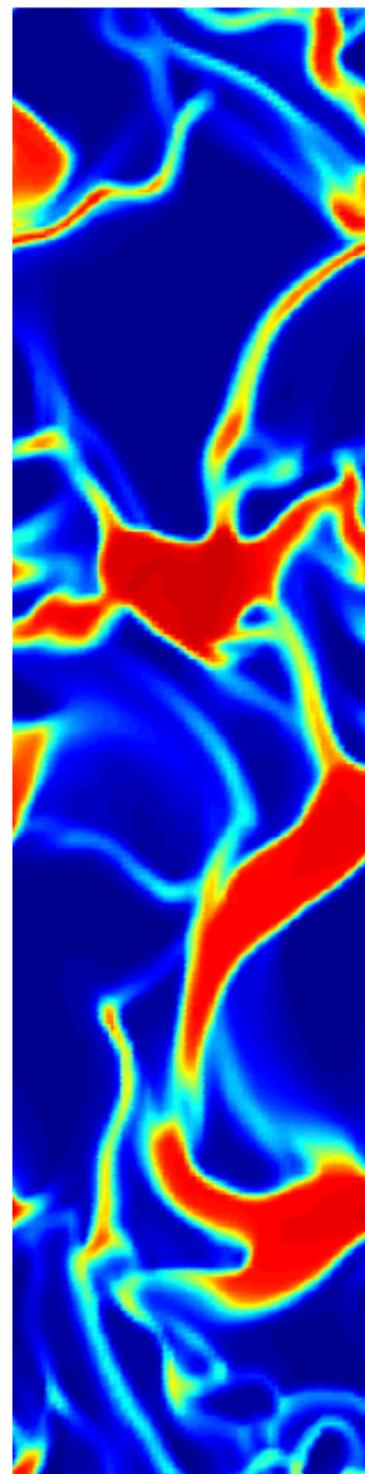
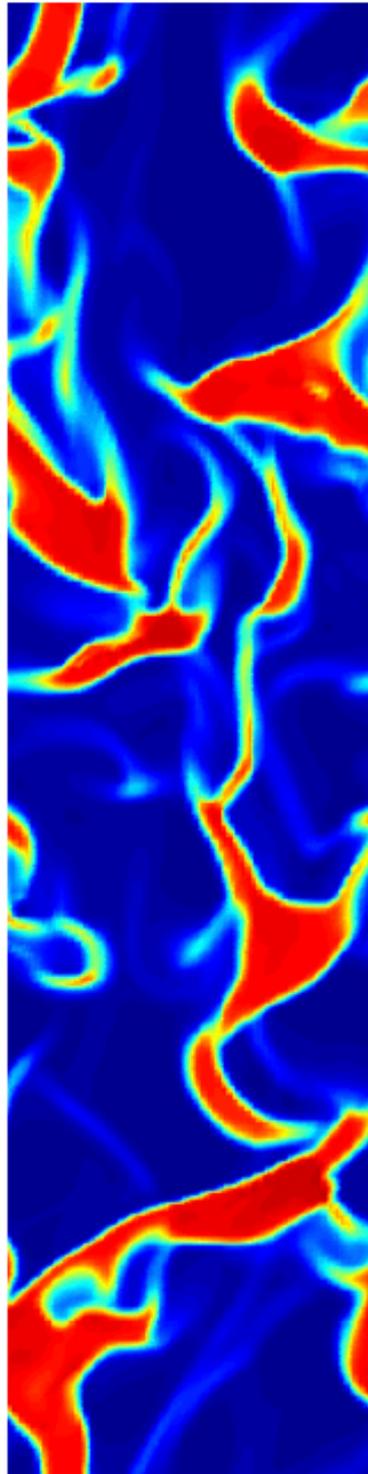
Model predictions



Bimodal PSD ($e = 0.95$)

Bidisperse

Monodisperse



MFIX simulations:

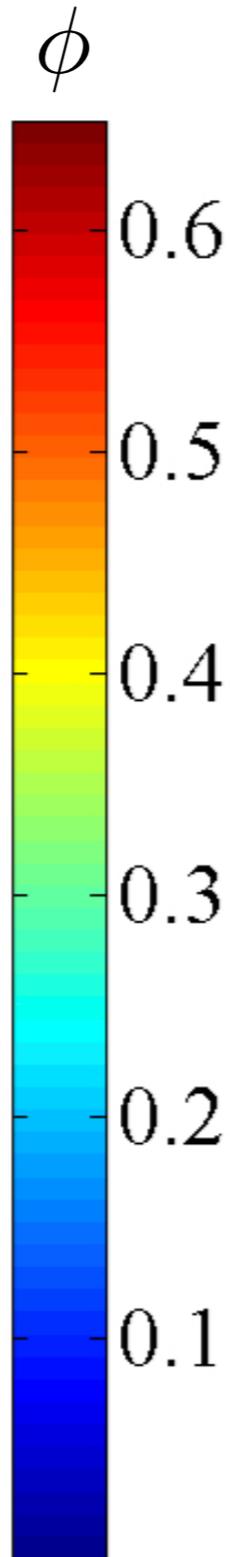
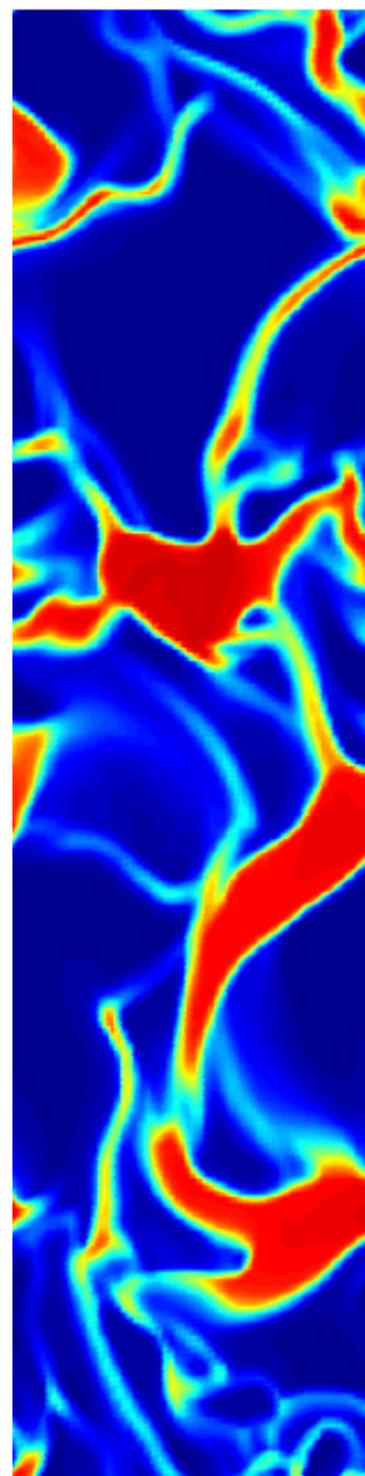
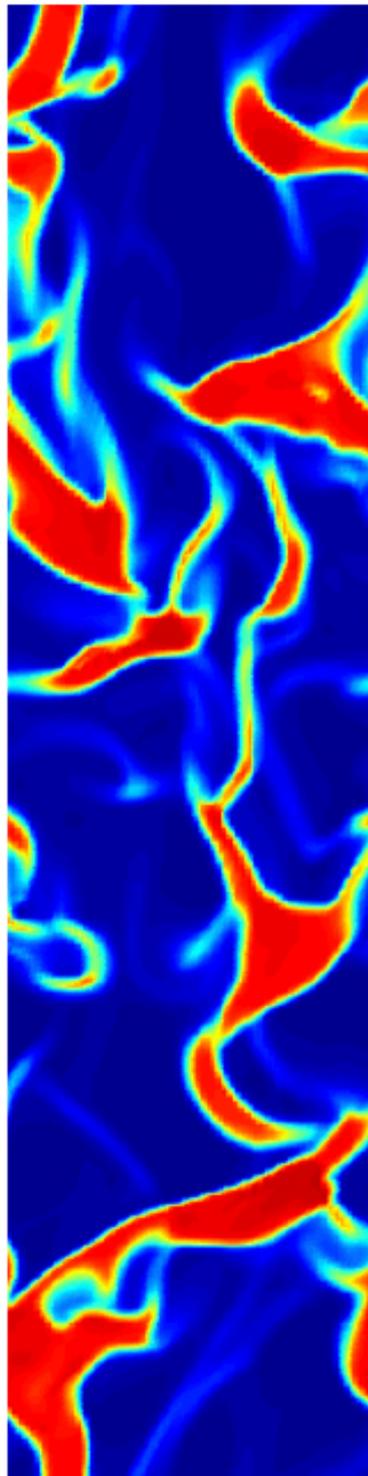
- $d_1=650 \mu m, d_2=170 \mu m$
- $\langle \phi_1 \rangle = \langle \phi_2 \rangle = 0.075$
- Doubly periodic
- 16 cm x 64 cm
- 0.25 cm grids

Model predictions

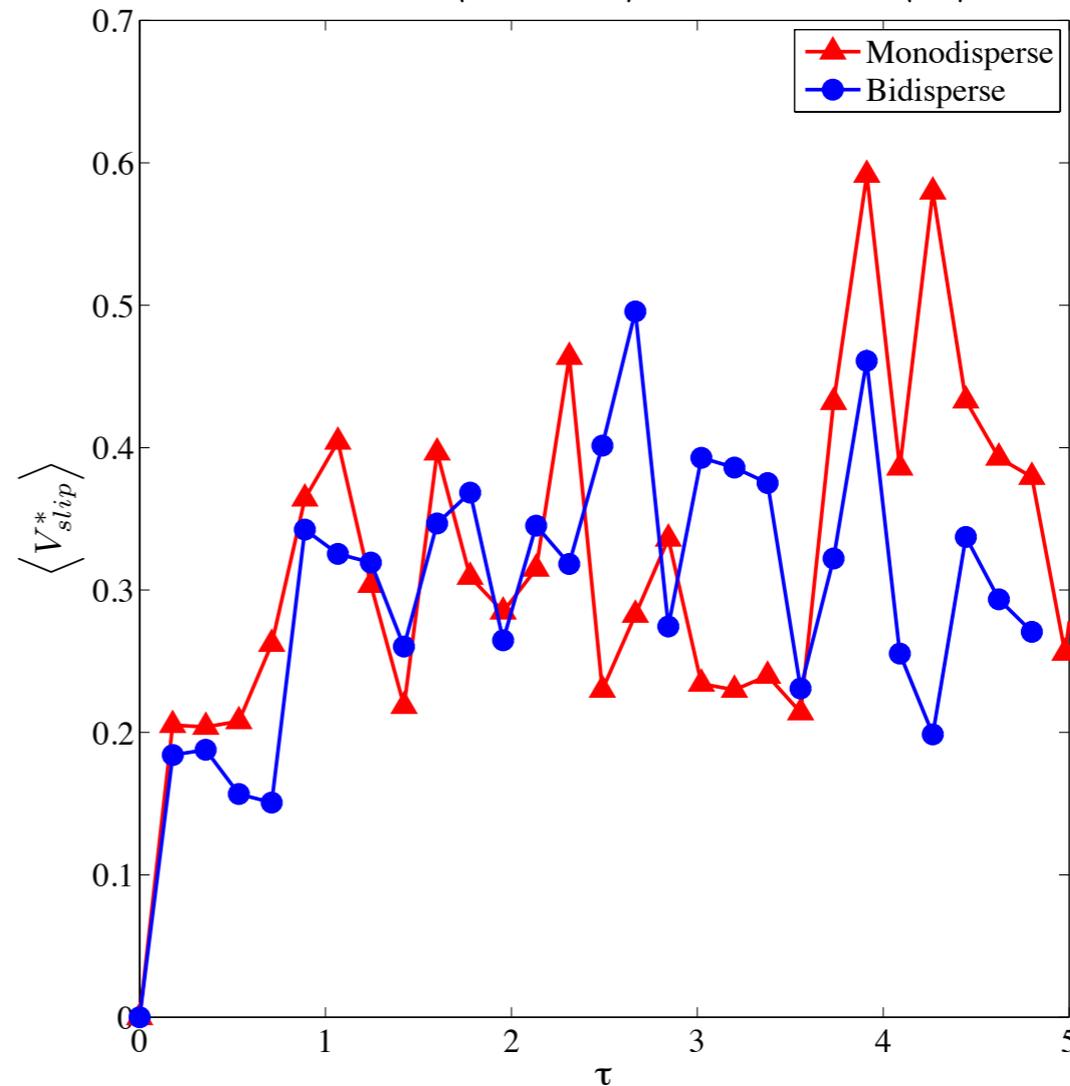
Bimodal PSD ($e = 0.95$)

Bidisperse

Monodisperse



$$\langle V_{slip} \rangle = \frac{\langle (1 - \phi) V_g \rangle}{\langle 1 - \phi \rangle} - \frac{\langle \phi V_{s_{mix}} \rangle}{\langle \phi \rangle}$$



MFIX simulations:

- $d_1 = 650 \mu m, d_2 = 170 \mu m$
- $\langle \phi_1 \rangle = \langle \phi_2 \rangle = 0.075$
- Doubly periodic
- 16 cm x 64 cm
- 0.25 cm grids

$$\langle V_{slip}^* \rangle = \frac{\langle V_{slip} \rangle}{V_t}$$

$$\tau = t \frac{g}{V_t}$$

Model predictions



Bimodal PSD ($e = 0.99$)

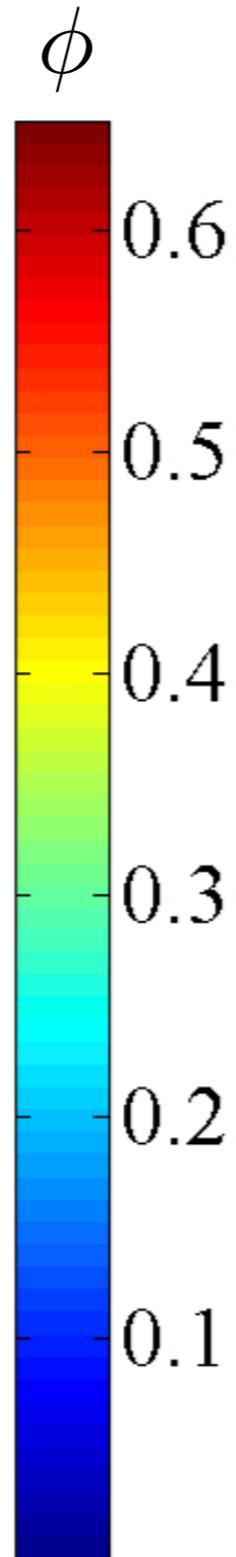
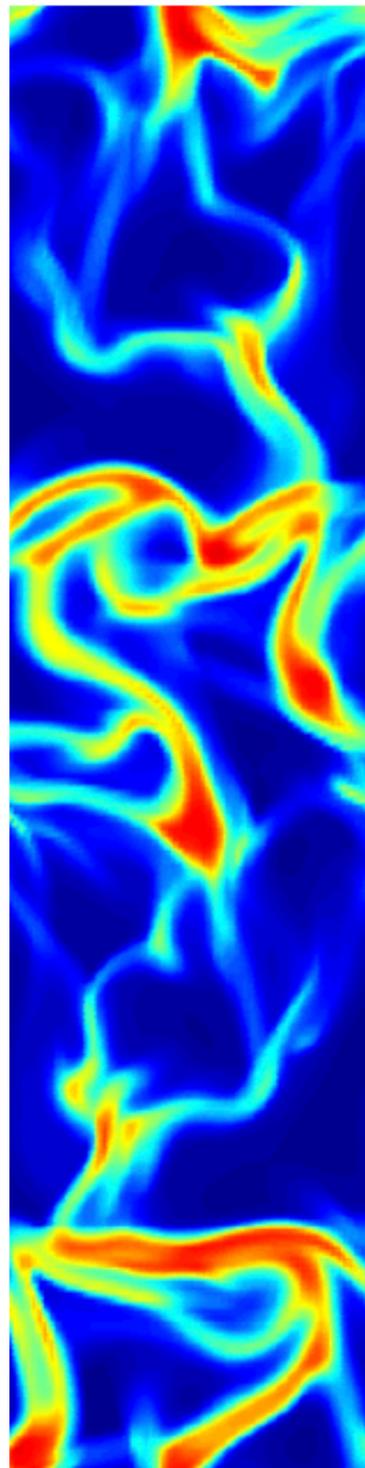
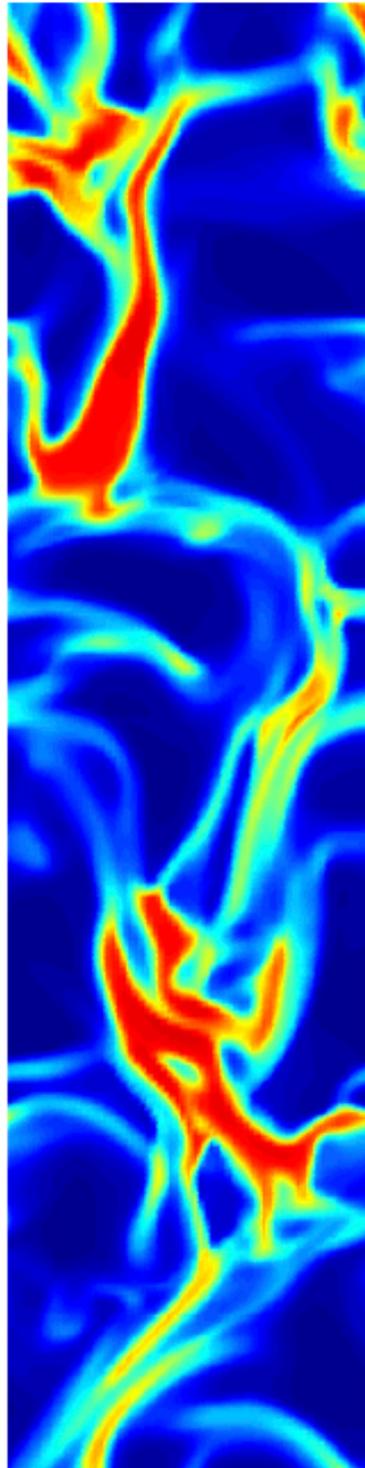
Model predictions



Bimodal PSD ($e = 0.99$)

Bidisperse

Monodisperse



MFIX simulations:

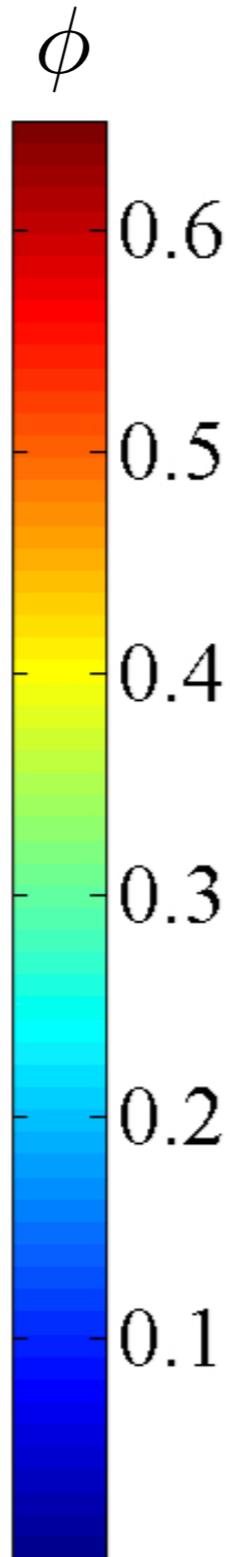
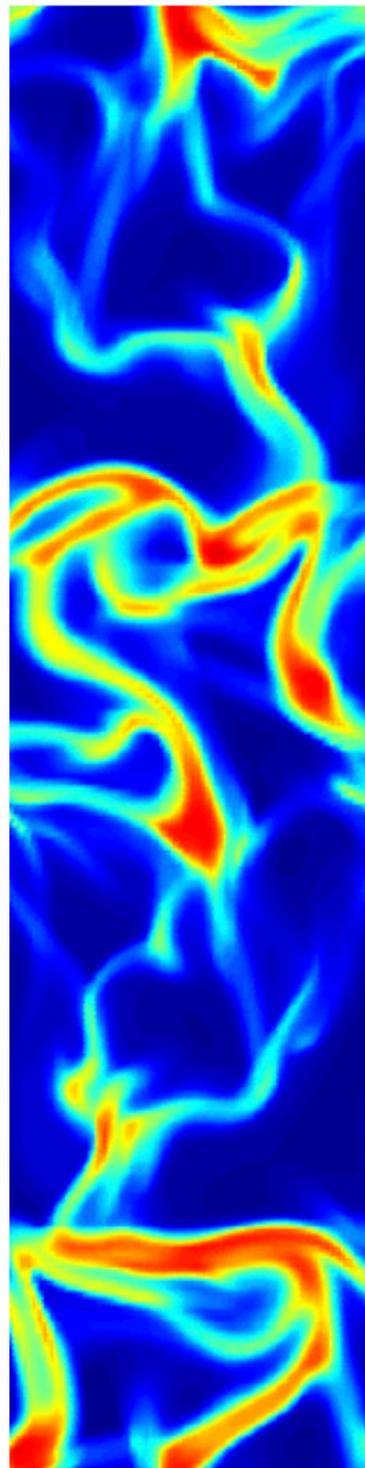
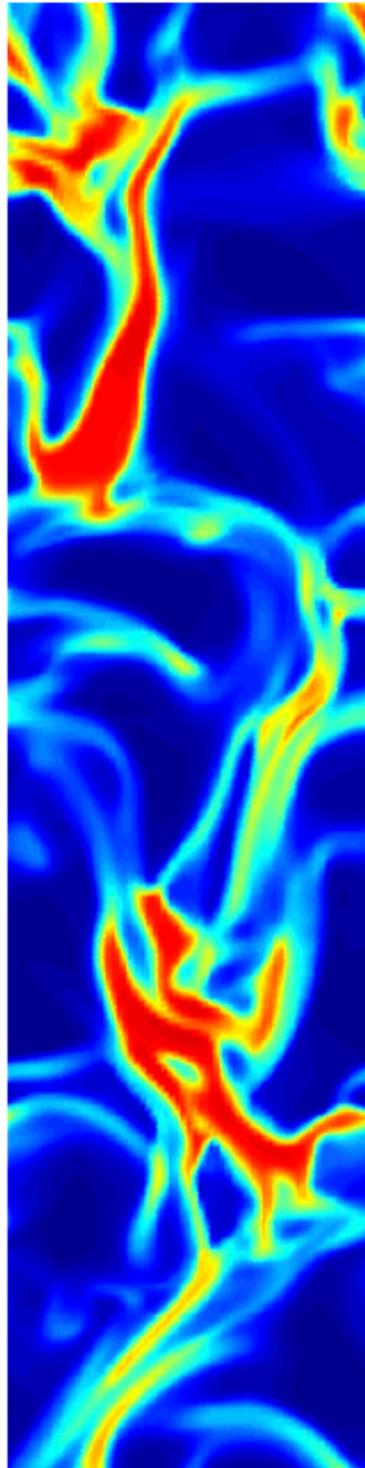
- $d_1 = 650 \mu m$, $d_2 = 170 \mu m$
- $\langle \phi_1 \rangle = \langle \phi_2 \rangle = 0.075$
- Doubly periodic
- 16 cm x 64 cm
- 0.25 cm grids

Model predictions

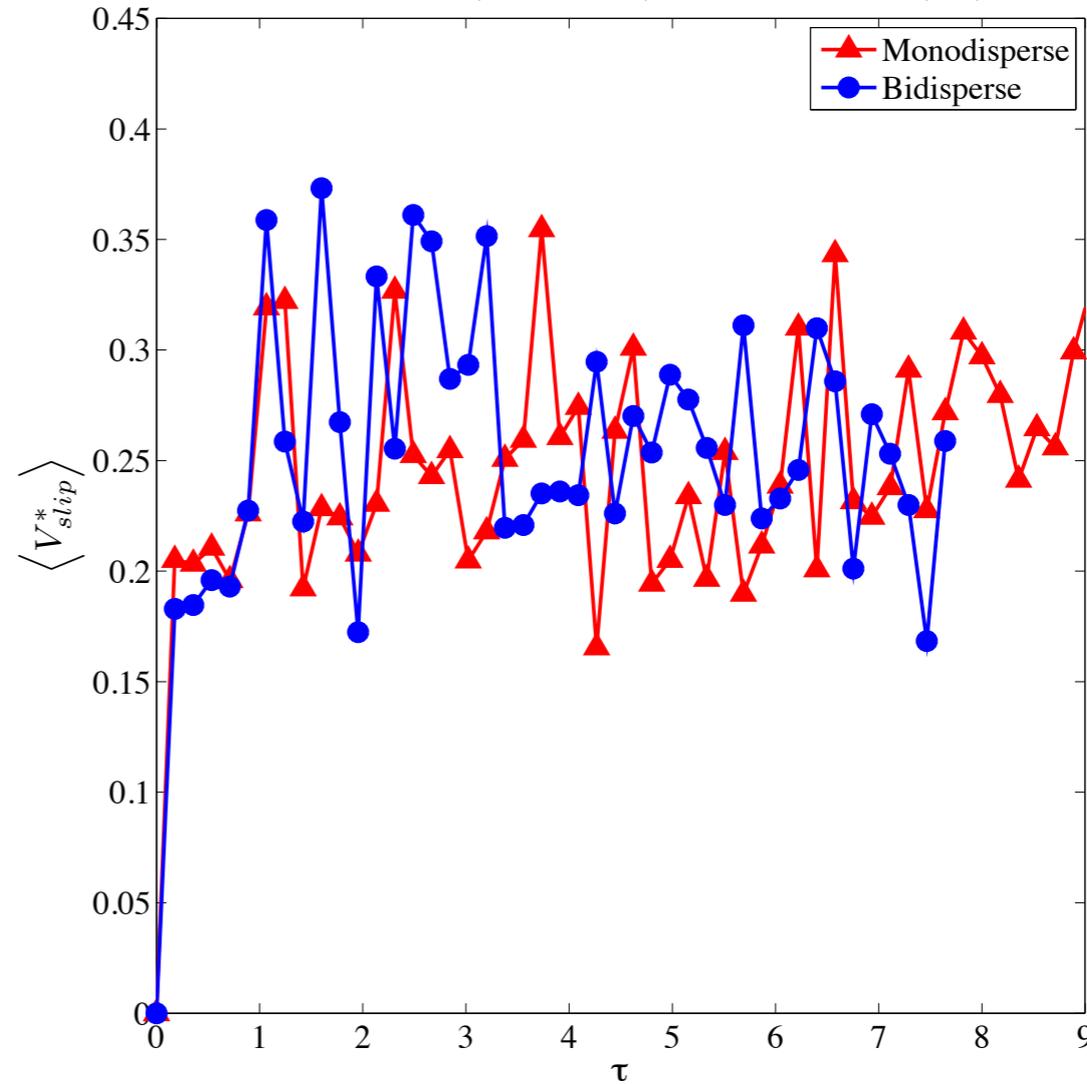
Bimodal PSD ($e = 0.99$)

Bidisperse

Monodisperse



$$\langle V_{slip} \rangle = \frac{\langle (1 - \phi) V_g \rangle}{\langle 1 - \phi \rangle} - \frac{\langle \phi V_{s_{mix}} \rangle}{\langle \phi \rangle}$$



MFIX simulations:

- $d_1 = 650 \mu m, d_2 = 170 \mu m$
- $\langle \phi_1 \rangle = \langle \phi_2 \rangle = 0.075$
- Doubly periodic
- 16 cm x 64 cm
- 0.25 cm grids

$$\langle V_{slip}^* \rangle = \frac{\langle V_{slip} \rangle}{V_t}$$

$$\tau = t \frac{g}{V_t}$$

Model prediction: Volume fraction ratios

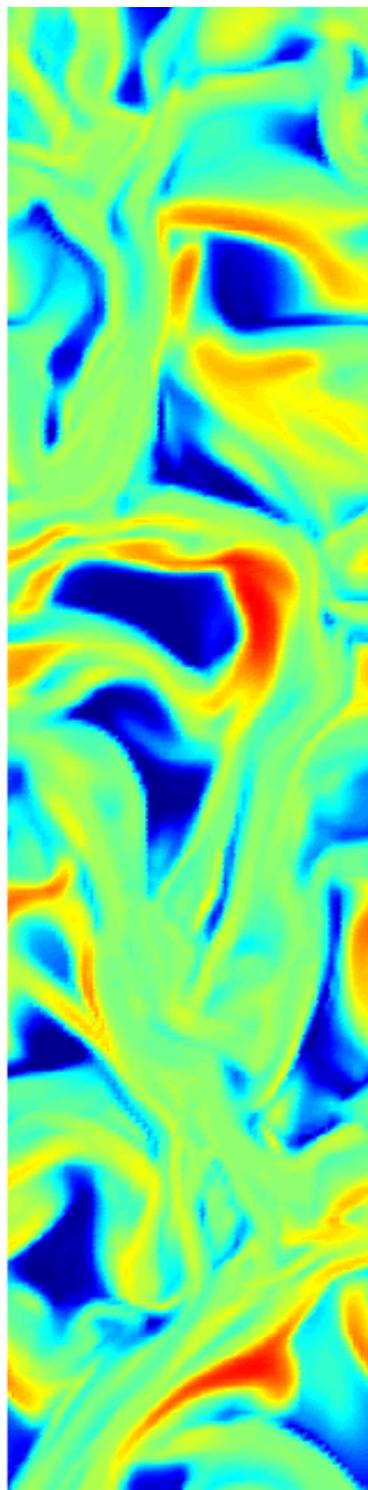


Bimodal PSD

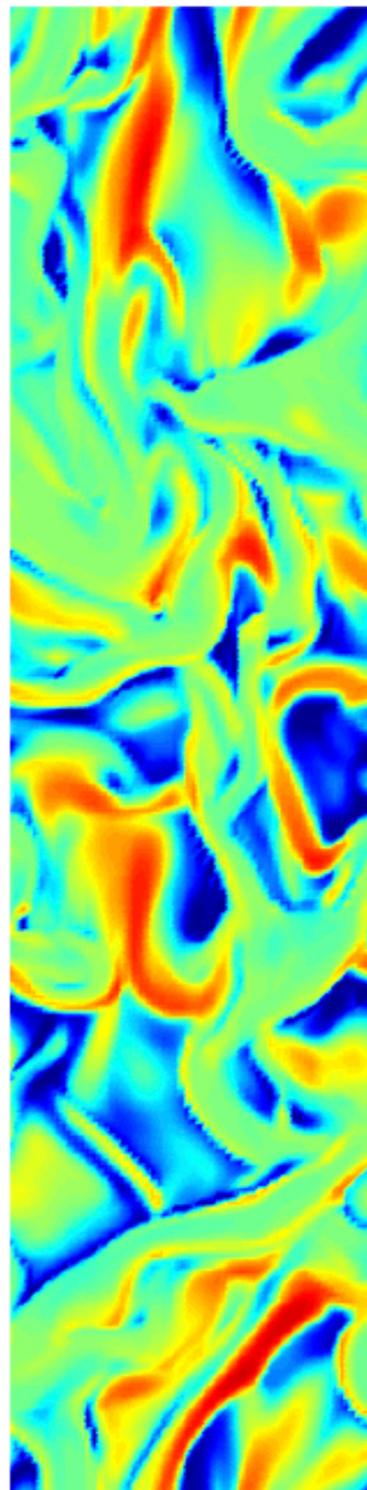
Model prediction: Volume fraction ratios

Bimodal PSD

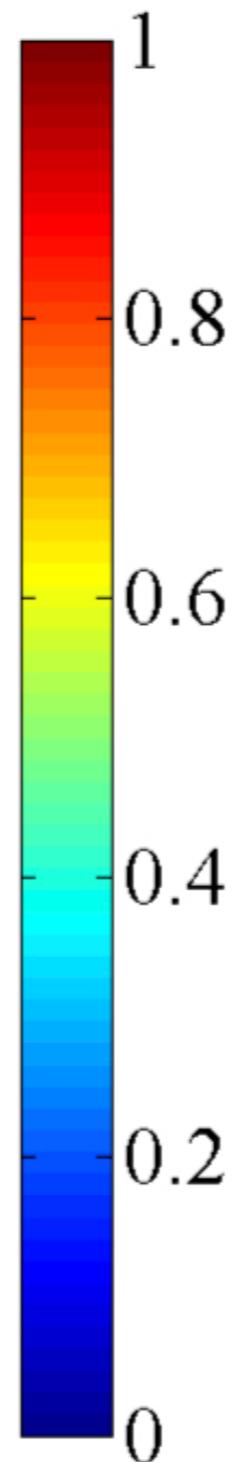
$e = 0.99$



$e = 0.95$



ϕ_1 / ϕ



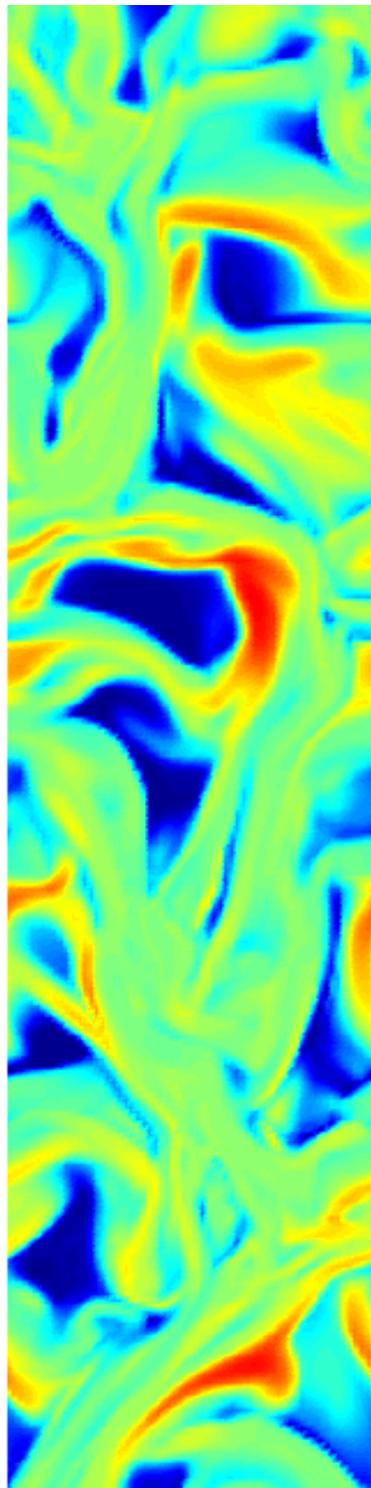
MFIX simulations:

- GHD theory
- HYS drag model
- $d_1 = 650 \mu m$, $d_2 = 170 \mu m$
- $\langle \phi_1 \rangle = 0.075$, $\langle \phi_2 \rangle = 0.075$
- Doubly periodic
- 16 cm x 64 cm

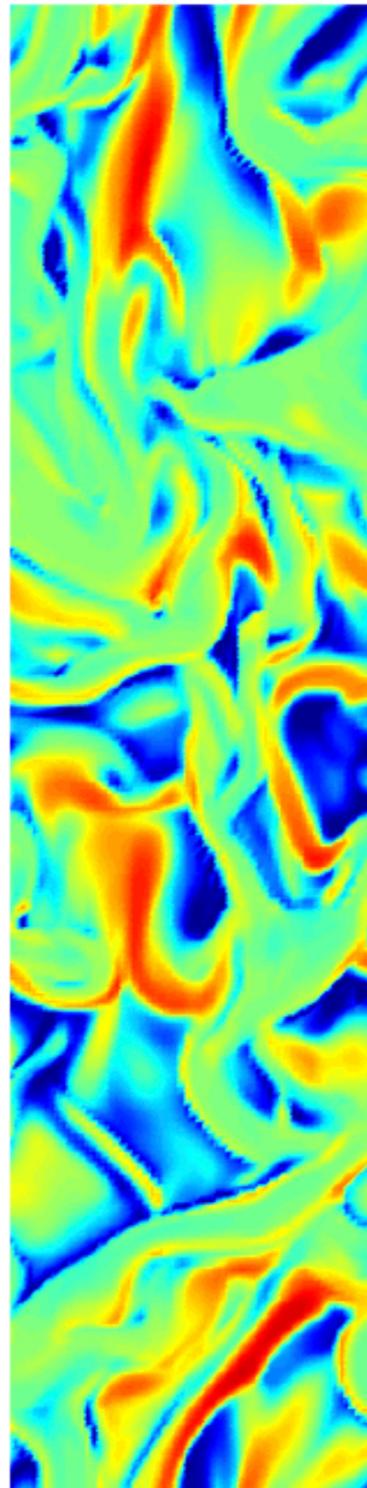
Model prediction: Volume fraction ratios

Bimodal PSD

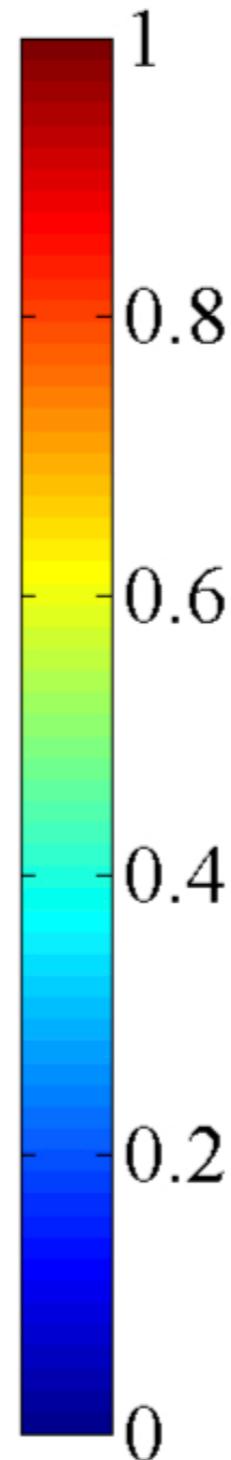
$e = 0.99$



$e = 0.95$



ϕ_1/ϕ



MFIX simulations:

- GHD theory
- HYS drag model
- $d_1=650 \mu m, d_2=170 \mu m$
- $\langle \phi_1 \rangle = 0.075, \langle \phi_2 \rangle = 0.075$
- Doubly periodic
- 16 cm x 64 cm

Bimodal PSD has a much broader distribution of particle volume fraction ratio than the Broad PSD case.

Grid resolution effects

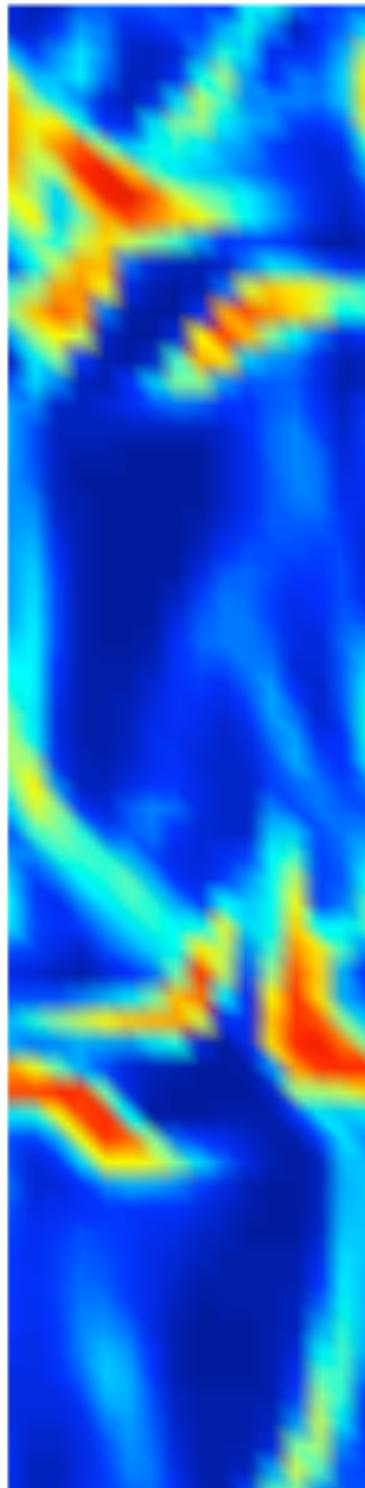


Broad PSD ($e = 0.99$)

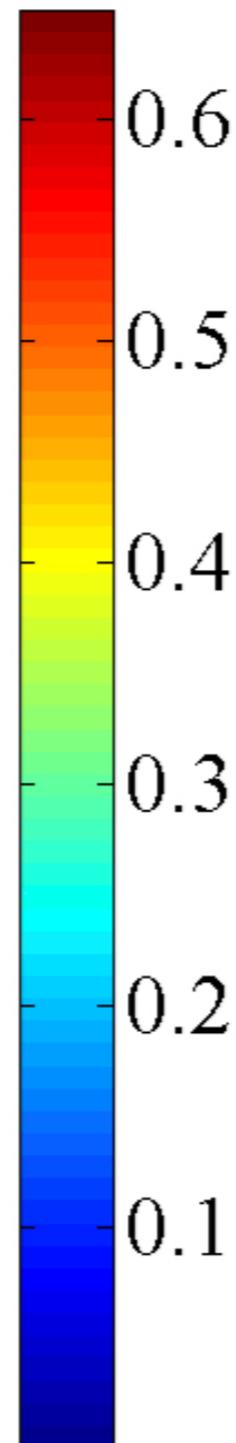
Grid resolution effects

Broad PSD ($e = 0.99$)

1 cm grids



ϕ



MFIX simulations:

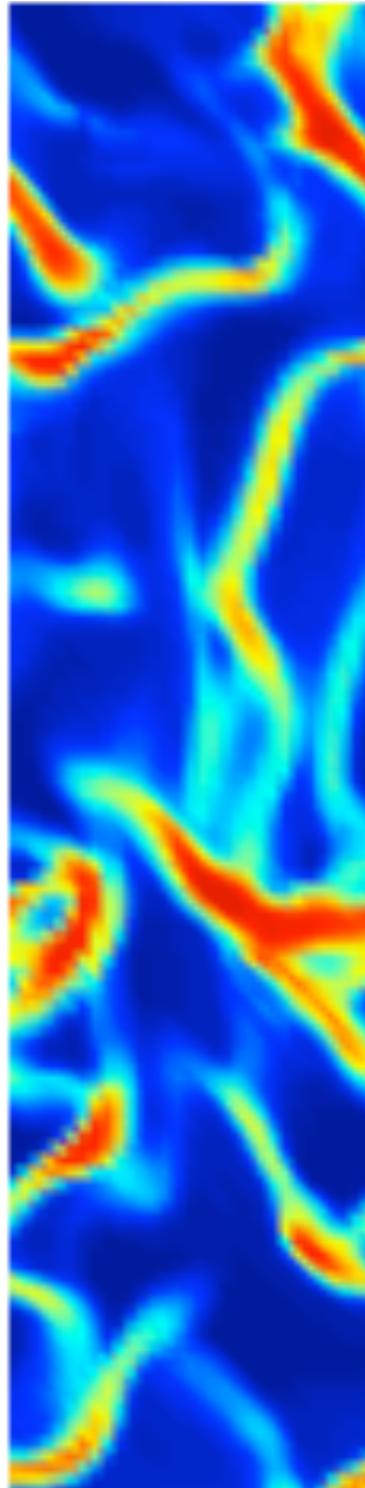
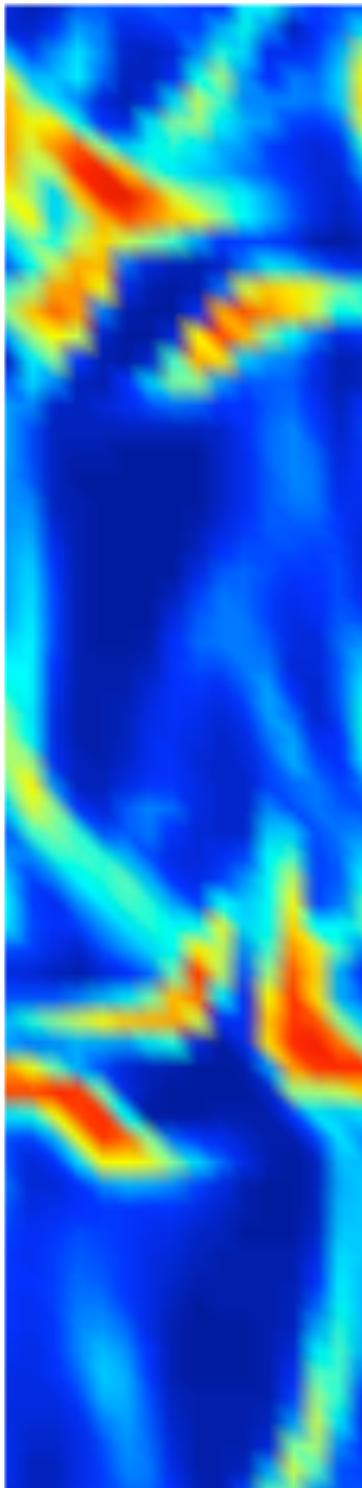
- GHD theory
- HYS drag model
- $d_1 = 212.5 \mu m$, $d_2 = 127.5 \mu m$
- $\langle \phi_1 \rangle = 0.125$, $\langle \phi_2 \rangle = 0.025$
- Doubly periodic
- 16 cm x 64 cm

Grid resolution effects

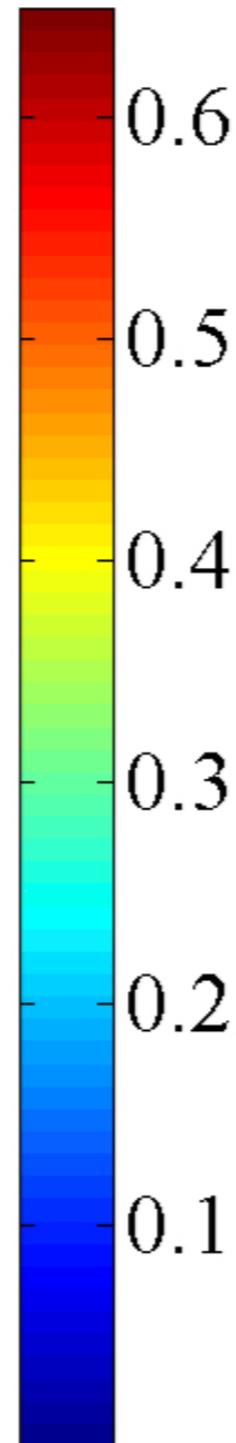
Broad PSD ($e = 0.99$)

1 cm grids

0.5 cm grids



ϕ



MFIX simulations:

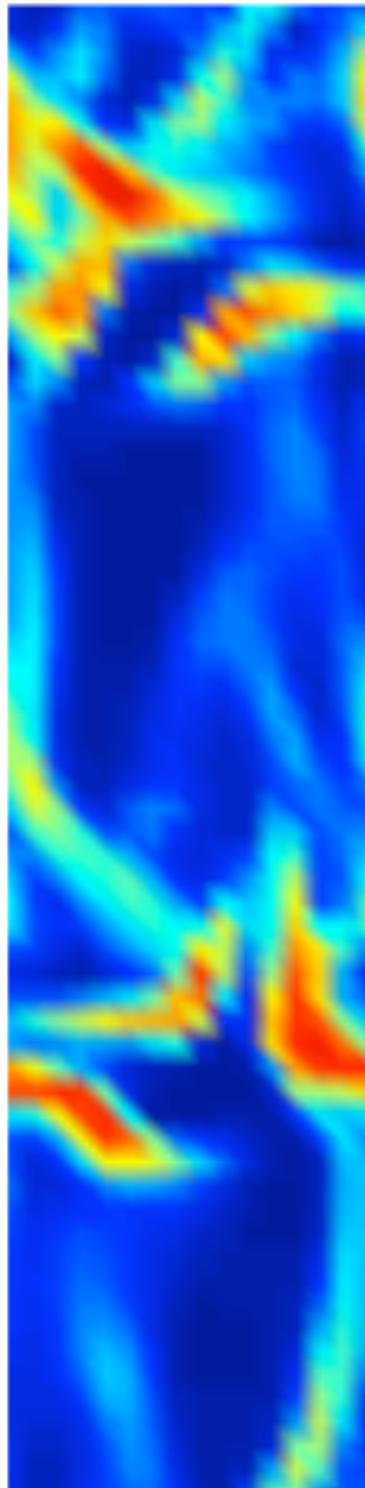
- GHD theory
- HYS drag model
- $d_1=212.5 \mu m$, $d_2=127.5 \mu m$
- $\langle \phi_1 \rangle = 0.125$, $\langle \phi_2 \rangle = 0.025$
- Doubly periodic
- 16 cm x 64 cm

Grid resolution effects

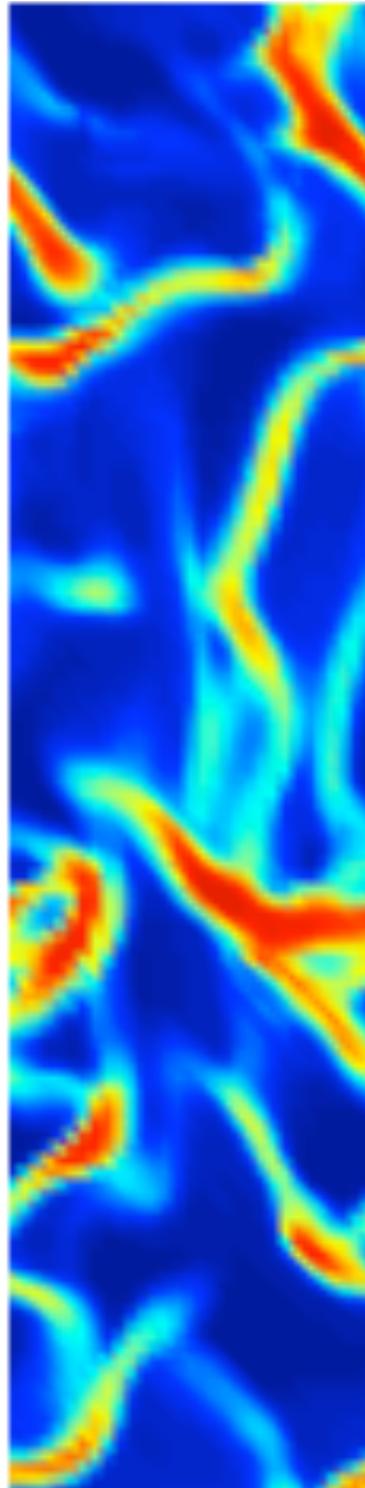


Broad PSD ($e = 0.99$)

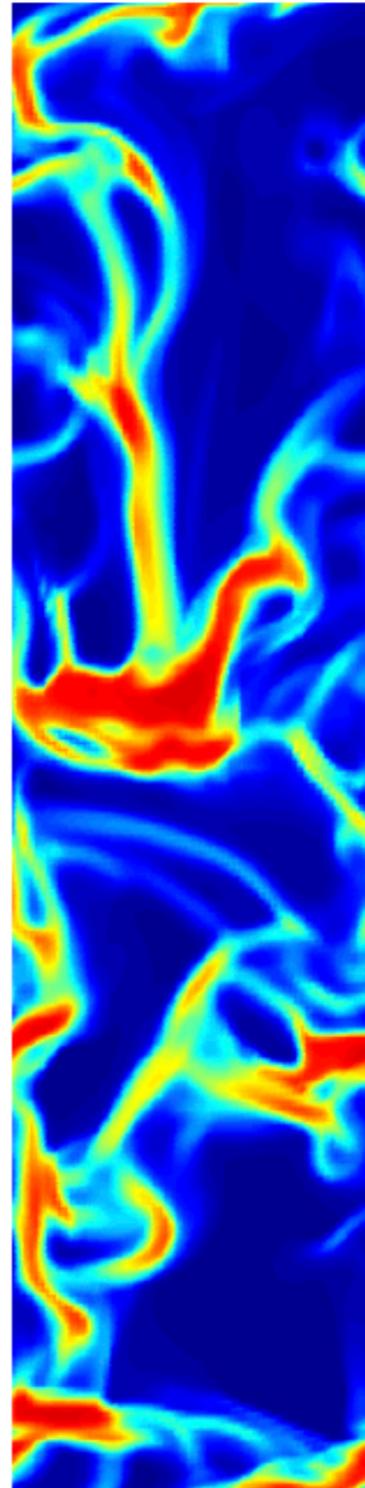
1 cm grids



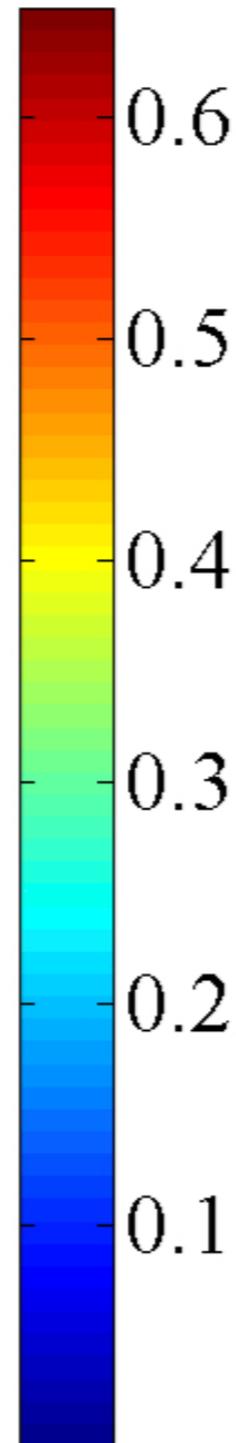
0.5 cm grids



0.25 cm grids



ϕ



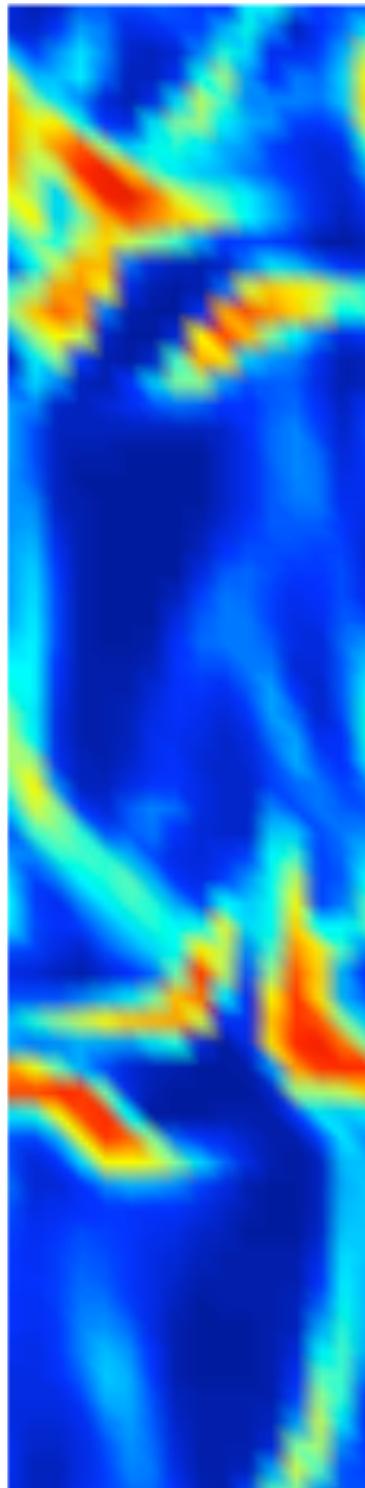
MFIX simulations:

- GHD theory
- HYS drag model
- $d_1=212.5 \mu\text{m}$, $d_2=127.5 \mu\text{m}$
- $\langle\phi_1\rangle=0.125$, $\langle\phi_2\rangle=0.025$
- Doubly periodic
- 16 cm x 64 cm

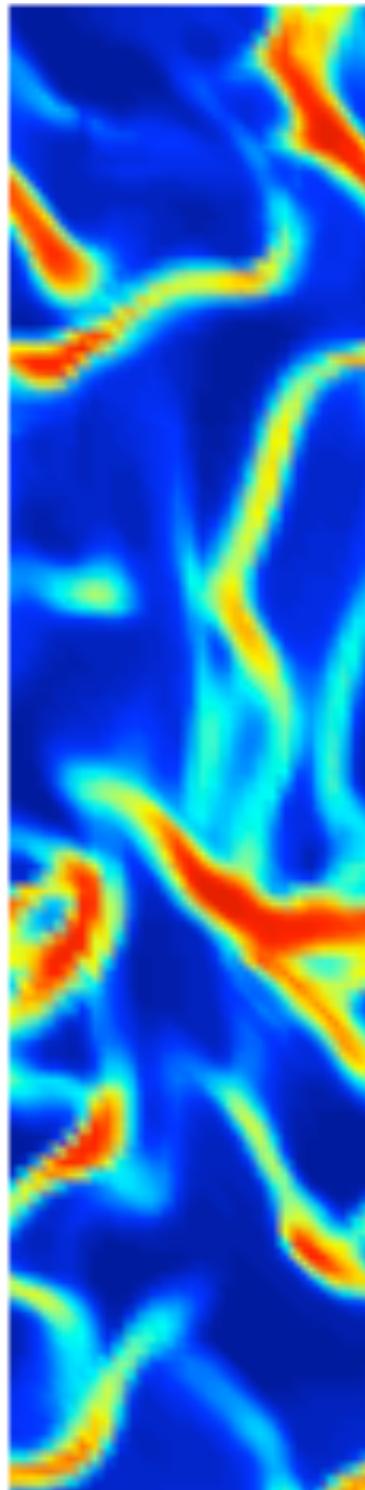
Grid resolution effects

Broad PSD ($e = 0.99$)

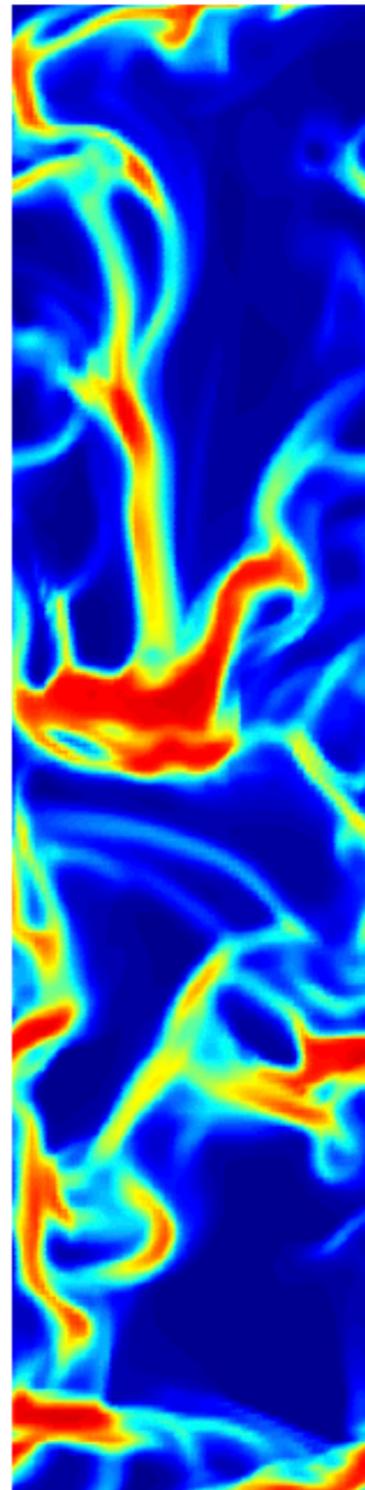
1 cm grids



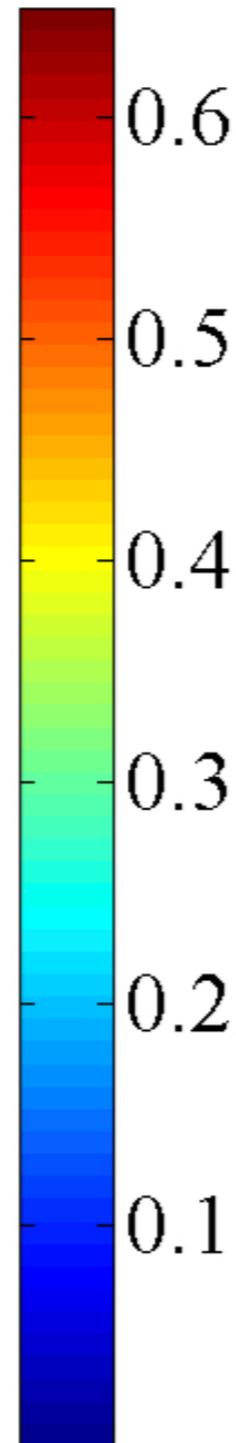
0.5 cm grids



0.25 cm grids



ϕ



MFIX simulations:

- GHD theory
- HYS drag model
- $d_1 = 212.5 \mu m$, $d_2 = 127.5 \mu m$
- $\langle \phi_1 \rangle = 0.125$, $\langle \phi_2 \rangle = 0.025$
- Doubly periodic
- 16 cm x 64 cm

As grid resolution is increased, finer structures begin to appear in the flow domain.

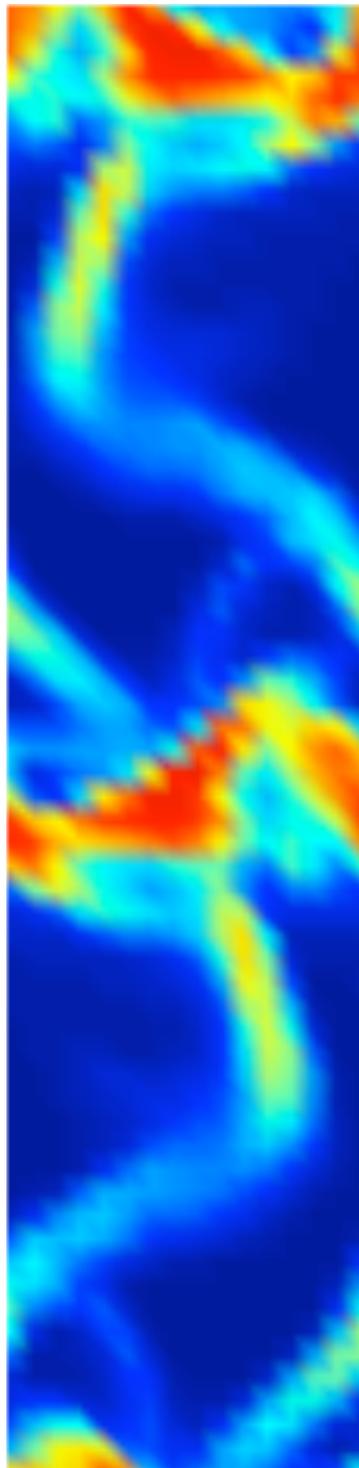
Grid resolution effects



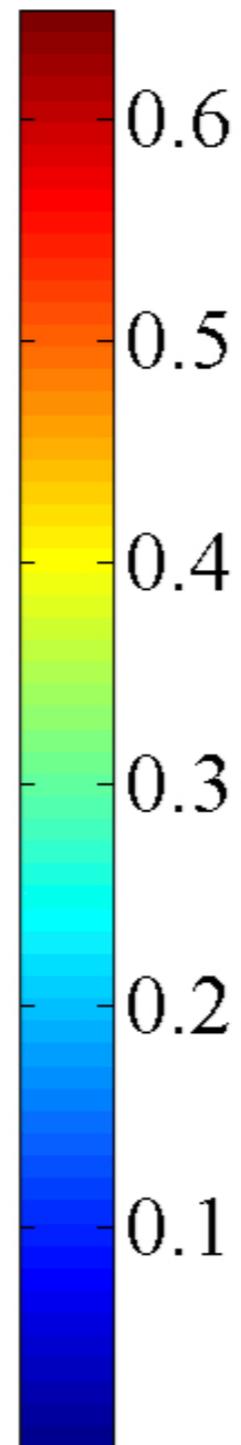
Bimodal PSD ($e = 0.99$)

Bimodal PSD ($e = 0.99$)

1 cm grids



ϕ



MFIX simulations:

- GHD theory
- HYS drag model
- $d_1 = 650 \mu m$, $d_2 = 170 \mu m$
- $\langle \phi_1 \rangle = 0.075$, $\langle \phi_2 \rangle = 0.075$
- Doubly periodic
- 16 cm x 64 cm

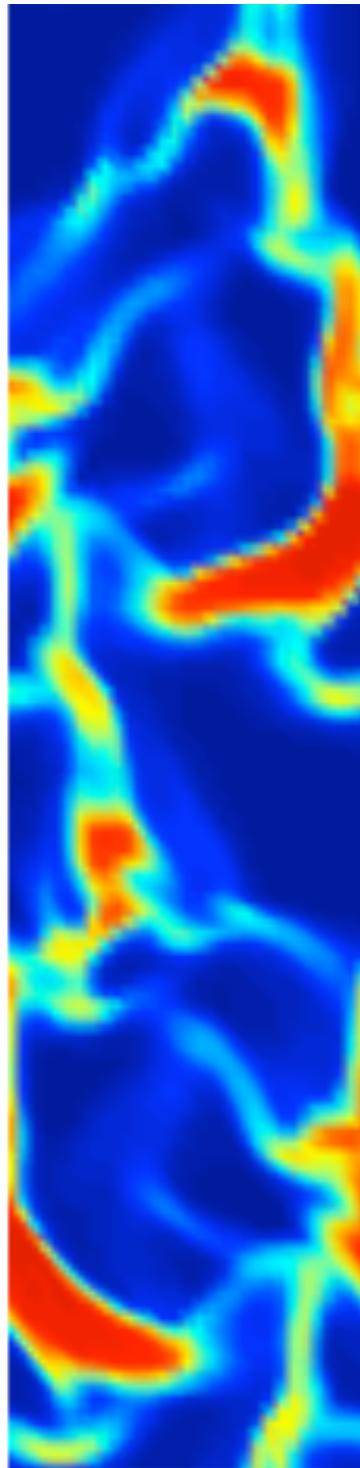
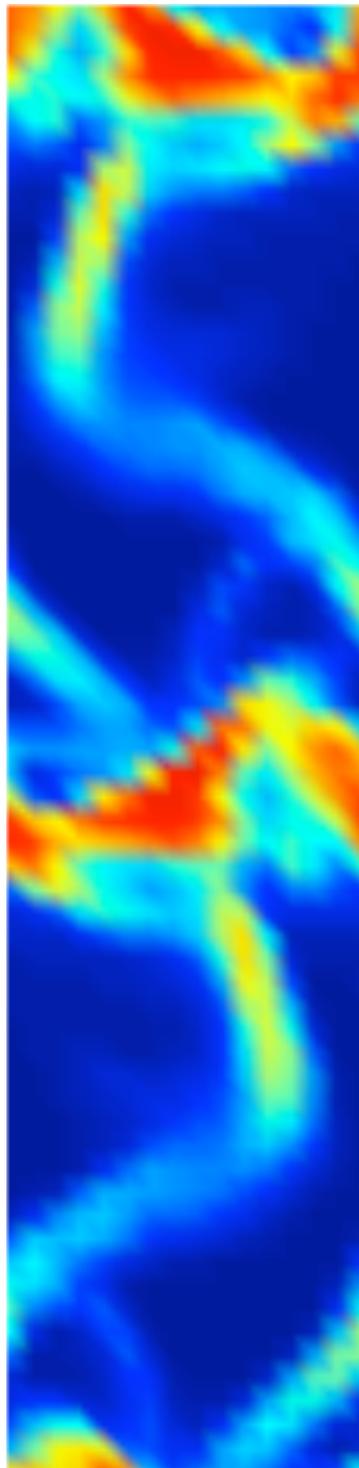
Grid resolution effects



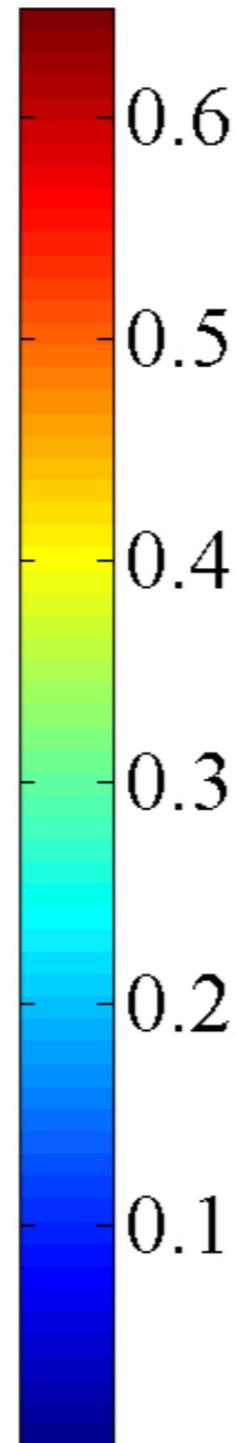
Bimodal PSD ($e = 0.99$)

1 cm grids

0.5 cm grids



ϕ



MFIX simulations:

- GHD theory
- HYS drag model
- $d_1=650 \mu m, d_2=170 \mu m$
- $\langle \phi_1 \rangle = 0.075, \langle \phi_2 \rangle = 0.075$
- Doubly periodic
- 16 cm x 64 cm

Grid resolution effects

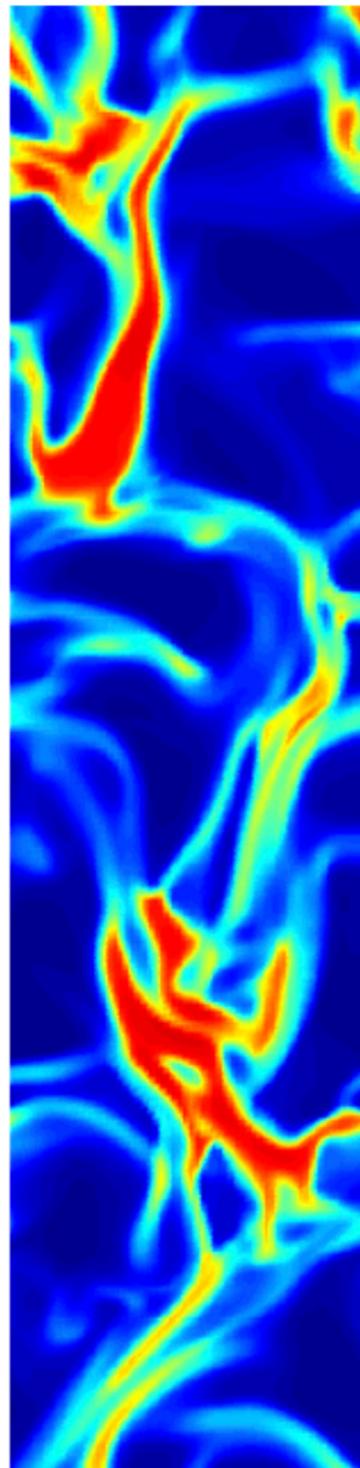
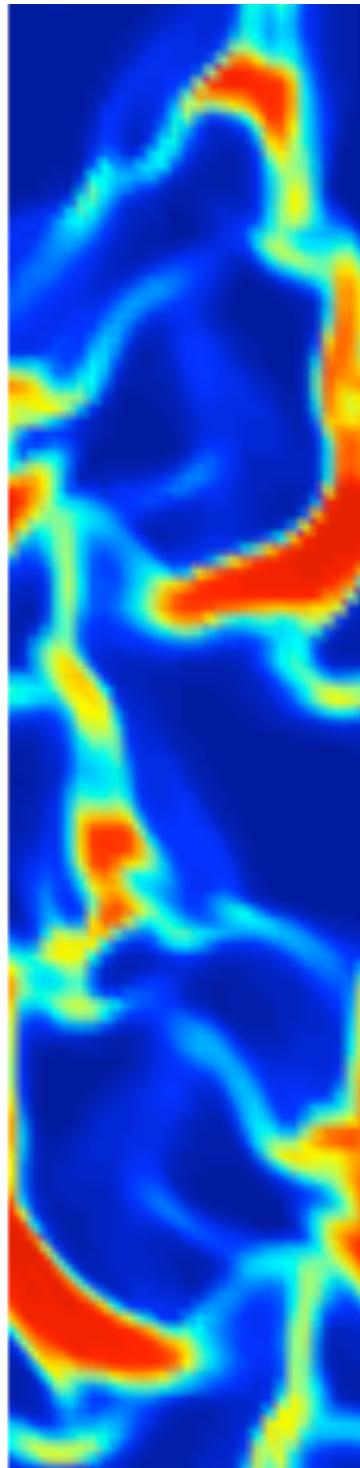
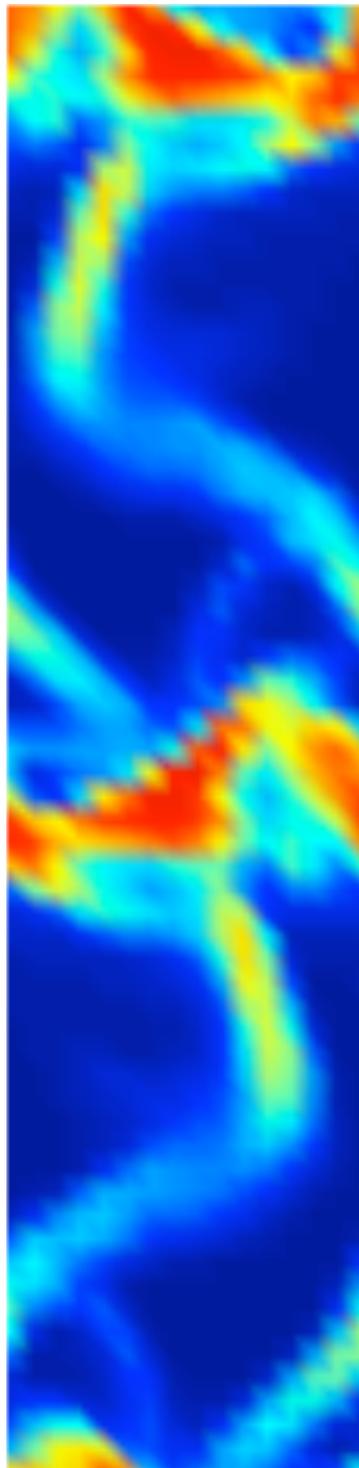


Bimodal PSD ($e = 0.99$)

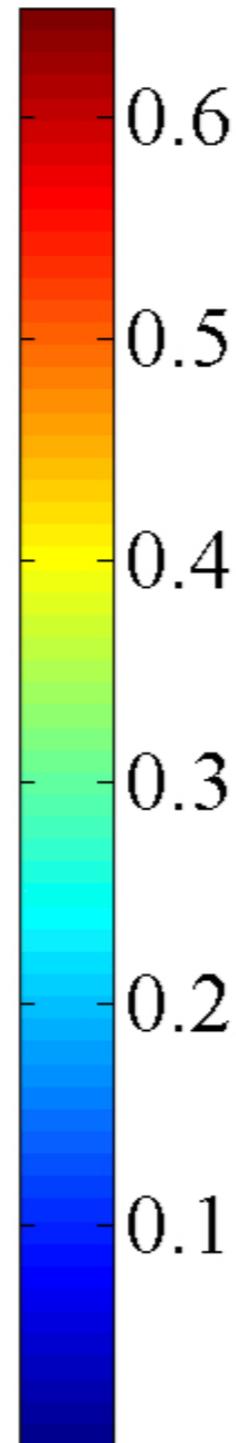
1 cm grids

0.5 cm grids

0.25 cm grids



ϕ



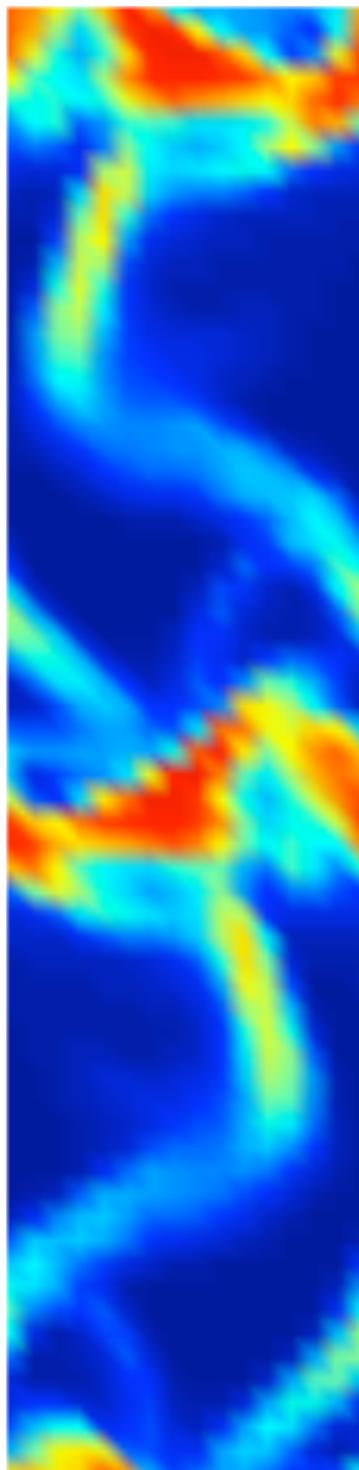
MFIX simulations:

- GHD theory
- HYS drag model
- $d_1=650 \mu m, d_2=170 \mu m$
- $\langle \phi_1 \rangle = 0.075, \langle \phi_2 \rangle = 0.075$
- Doubly periodic
- 16 cm x 64 cm

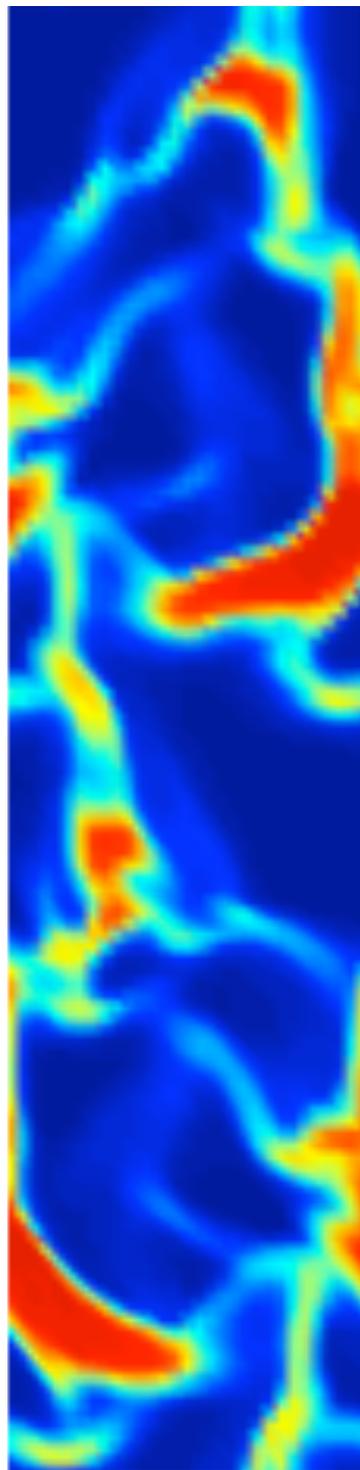
Grid resolution effects

Bimodal PSD ($e = 0.99$)

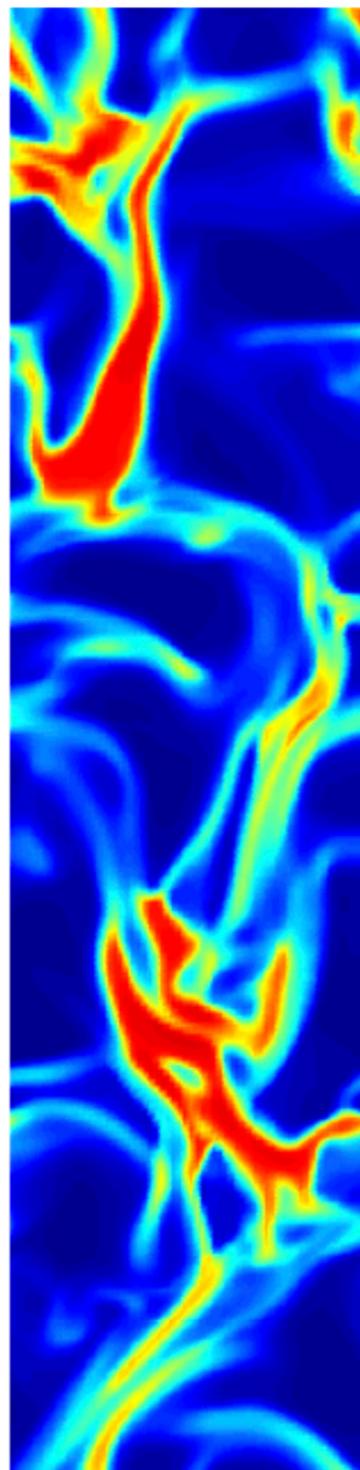
1 cm grids



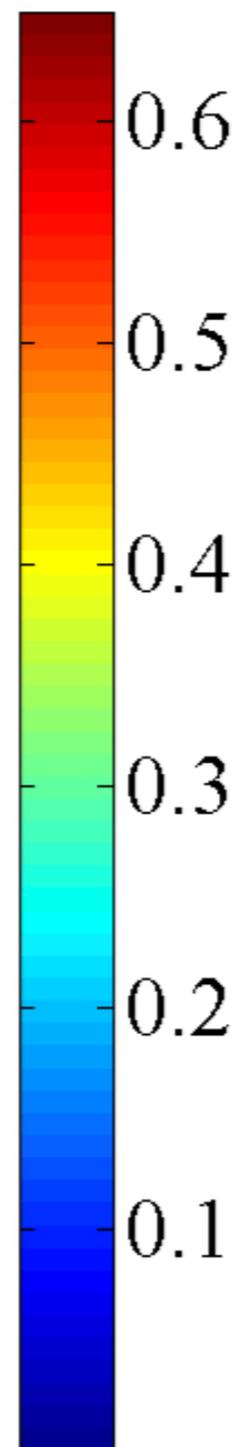
0.5 cm grids



0.25 cm grids



ϕ



MFIX simulations:

- GHD theory
- HYS drag model
- $d_1 = 650 \mu\text{m}$, $d_2 = 170 \mu\text{m}$
- $\langle \phi_1 \rangle = 0.075$, $\langle \phi_2 \rangle = 0.075$
- Doubly periodic
- 16 cm x 64 cm

The emergence of fine structure with grid resolution indicates that equations used to model binary gas-solid flows must be coarse grained.

Bimodal PSD ($e = 0.95$)

Assumption:

$$Kn \ll 1$$

$$Kn = \frac{l_{mf}}{l_{grad}}$$

$$l_{mf} \approx \frac{d}{6\sqrt{2}\phi}$$

$$l_{grad} = \left| \frac{\bar{\chi}}{\nabla\chi} \right|$$

Range of validity of kinetic theory formulation



Bimodal PSD ($e = 0.95$)

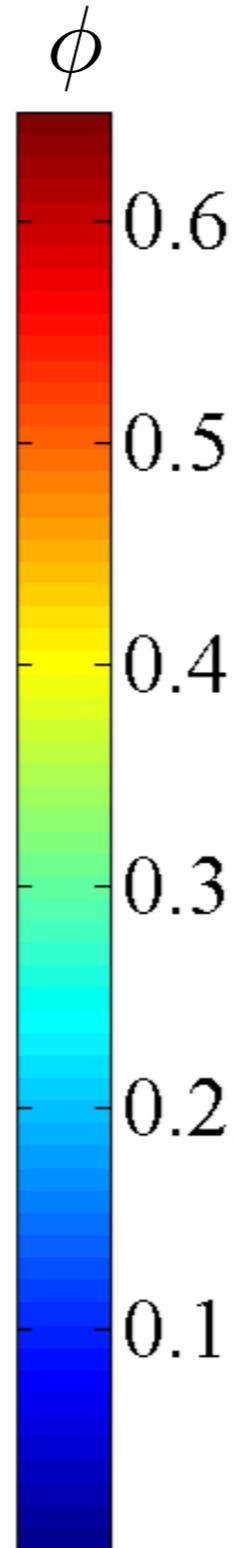
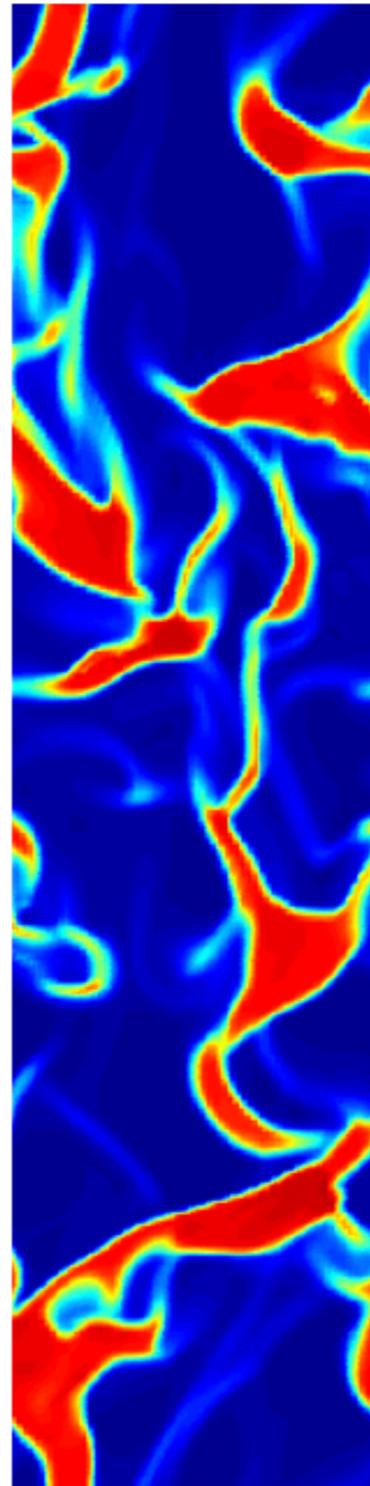
Assumption:

$$Kn \ll 1$$

$$Kn = \frac{l_{mf}}{l_{grad}}$$

$$l_{mf} \approx \frac{d}{6\sqrt{2}\phi}$$

$$l_{grad} = \left| \frac{\bar{\chi}}{\nabla\chi} \right|$$



Range of validity of kinetic theory formulation



Bimodal PSD ($e = 0.95$)

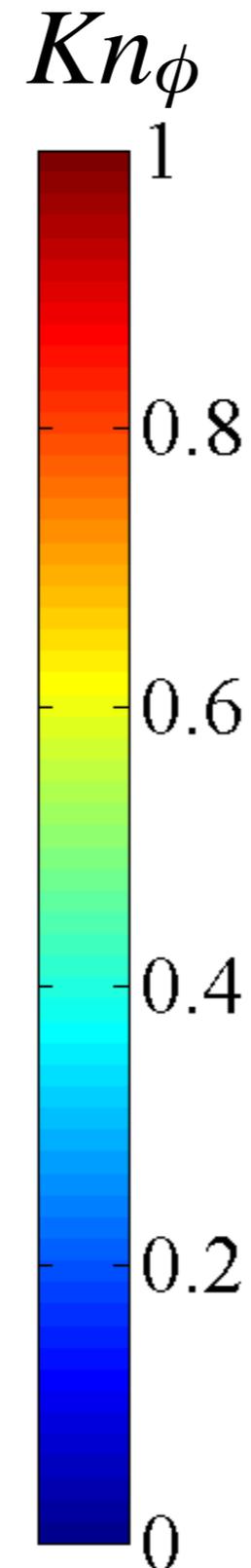
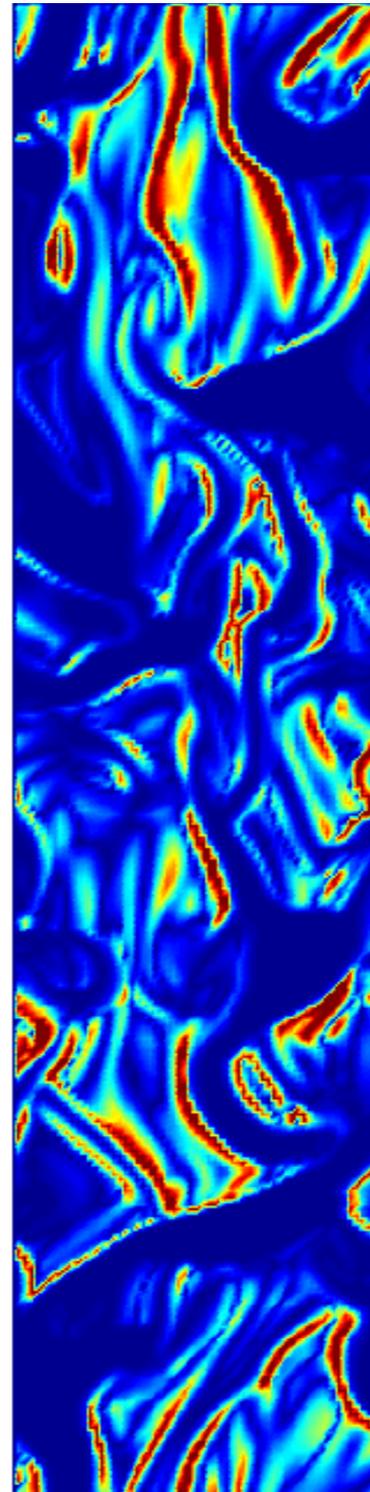
Assumption:

$$Kn \ll 1$$

$$Kn = \frac{l_{mf}}{l_{grad}}$$

$$l_{mf} \approx \frac{d}{6\sqrt{2}\phi}$$

$$l_{grad} = \left| \frac{\bar{\chi}}{\nabla\chi} \right|$$



Range of validity of kinetic theory formulation



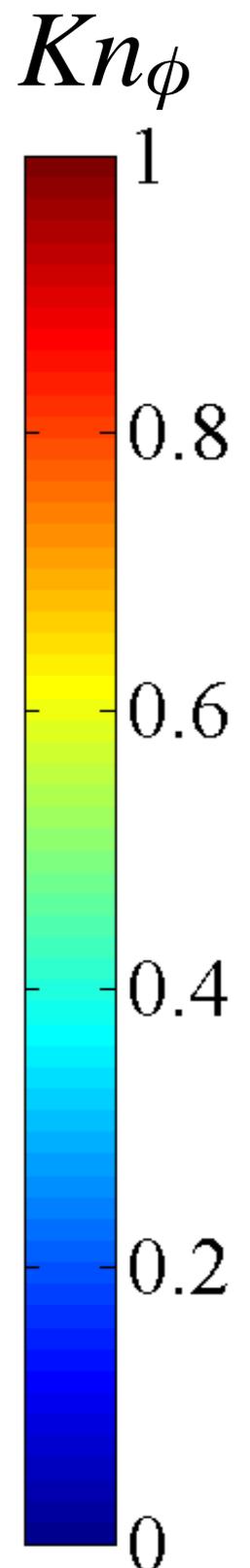
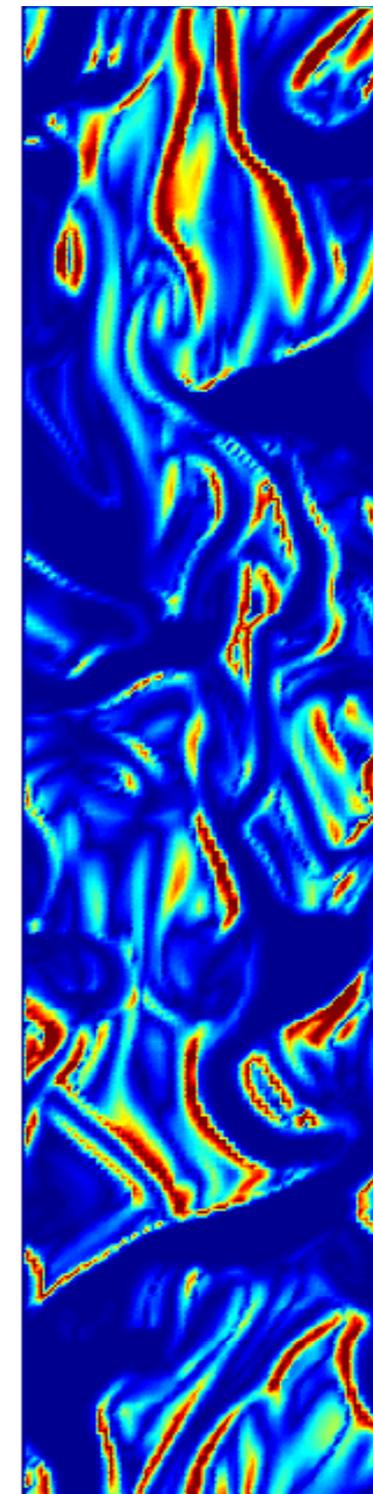
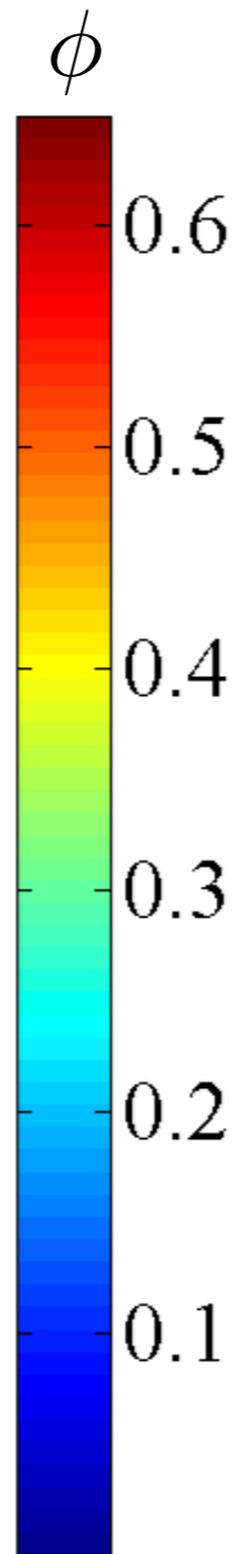
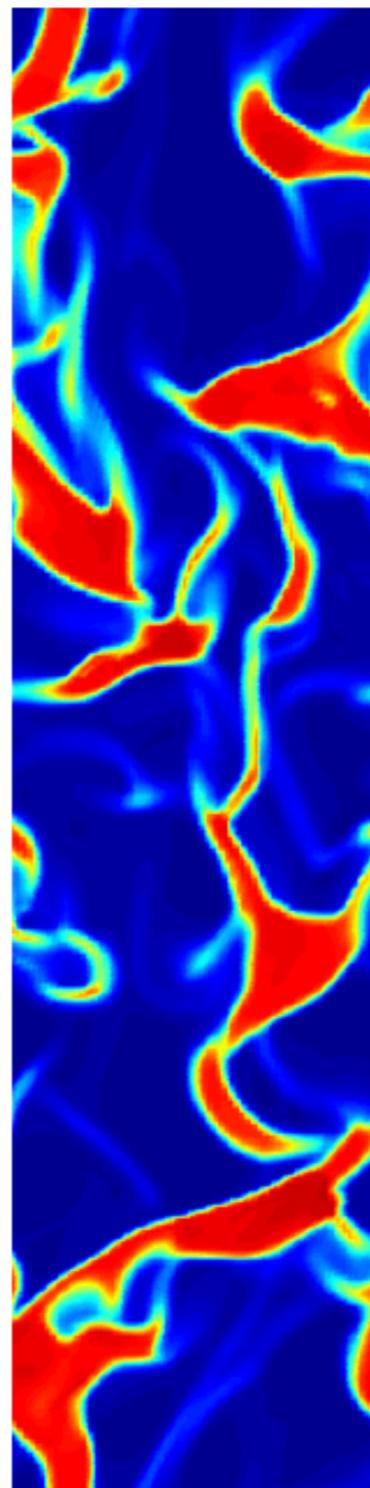
Bimodal PSD ($e = 0.95$)

Assumption:
 $Kn \ll 1$

$$Kn = \frac{l_{mf}}{l_{grad}}$$

$$l_{mf} \approx \frac{d}{6\sqrt{2}\phi}$$

$$l_{grad} = \left| \frac{\bar{\chi}}{\nabla\chi} \right|$$



Bimodal PSD ($e = 0.95$)

Assumption:

$$Kn \ll 1$$

$$Kn = \frac{l_{mf}}{l_{grad}}$$

$$l_{mf} \approx \frac{d}{6\sqrt{2}\phi}$$

$$l_{grad} = \left| \frac{\bar{\chi}}{\nabla\chi} \right|$$

Range of validity of kinetic theory formulation



Bimodal PSD ($e = 0.95$)

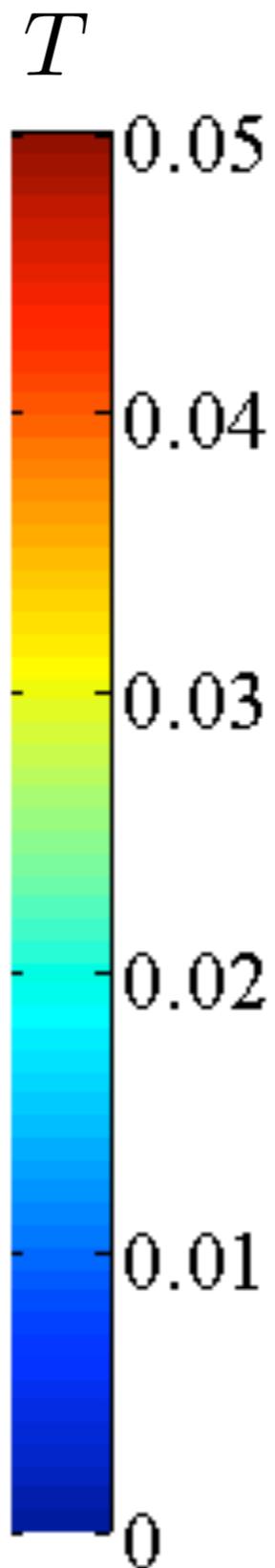
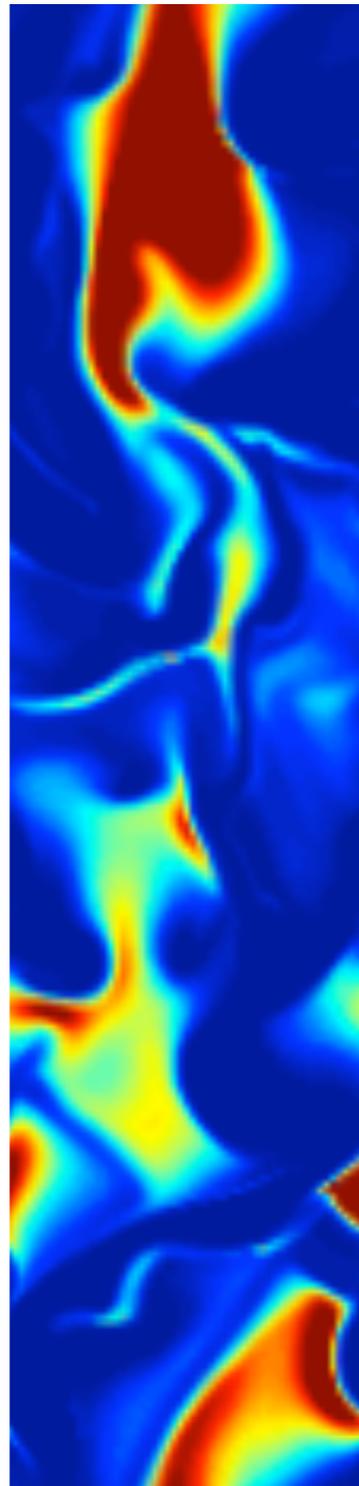
Assumption:

$$Kn \ll 1$$

$$Kn = \frac{l_{mf}}{l_{grad}}$$

$$l_{mf} \approx \frac{d}{6\sqrt{2}\phi}$$

$$l_{grad} = \left| \frac{\bar{\chi}}{\nabla\chi} \right|$$



Range of validity of kinetic theory formulation



Bimodal PSD ($e = 0.95$)

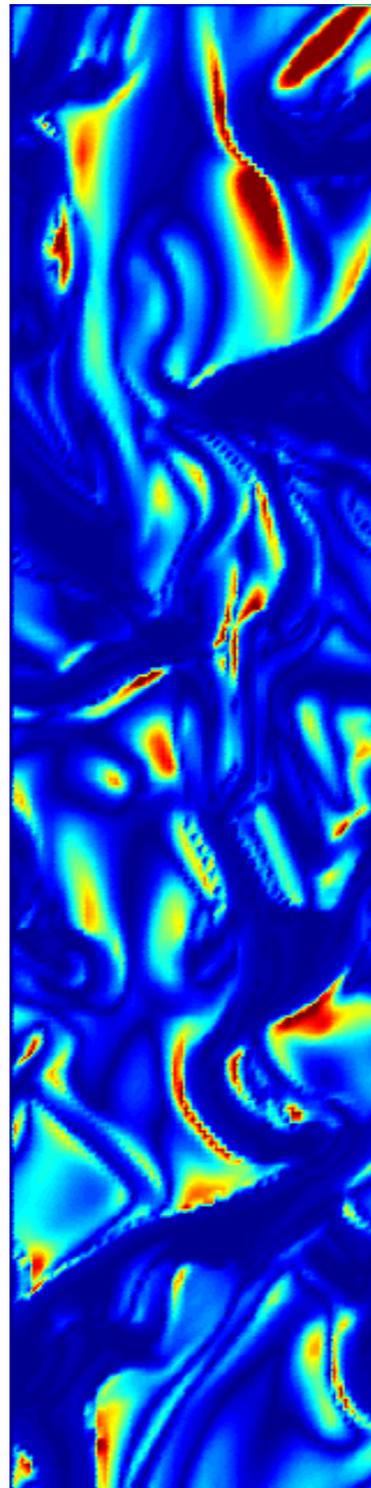
Assumption:

$$Kn \ll 1$$

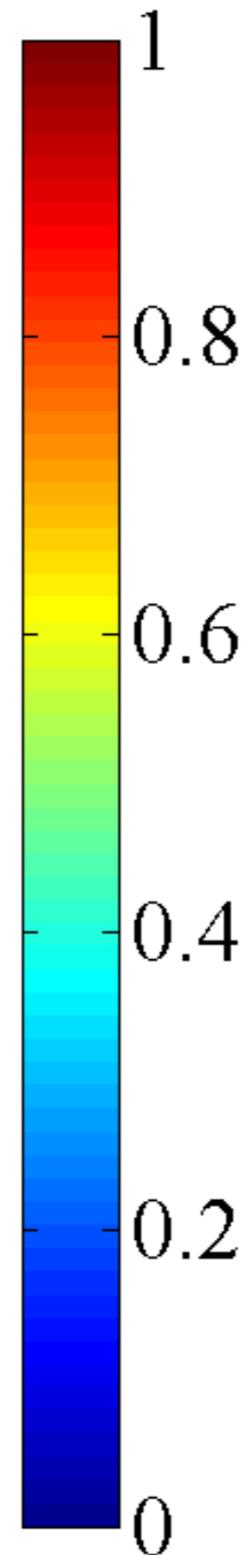
$$Kn = \frac{l_{mf}}{l_{grad}}$$

$$l_{mf} \approx \frac{d}{6\sqrt{2}\phi}$$

$$l_{grad} = \left| \frac{\bar{\chi}}{\nabla\chi} \right|$$



Kn_T



Range of validity of kinetic theory formulation



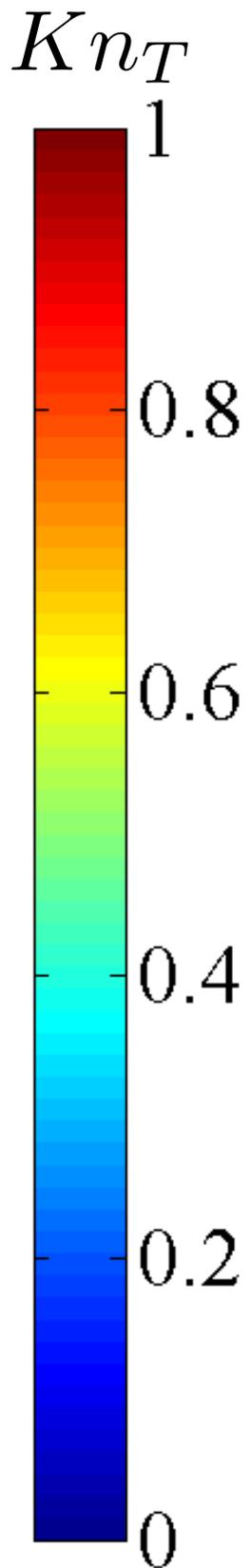
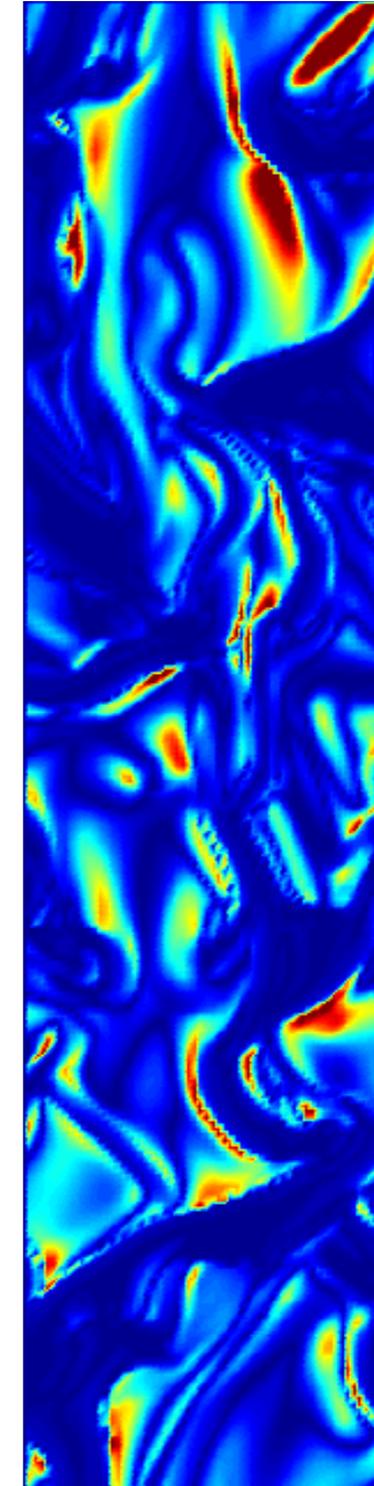
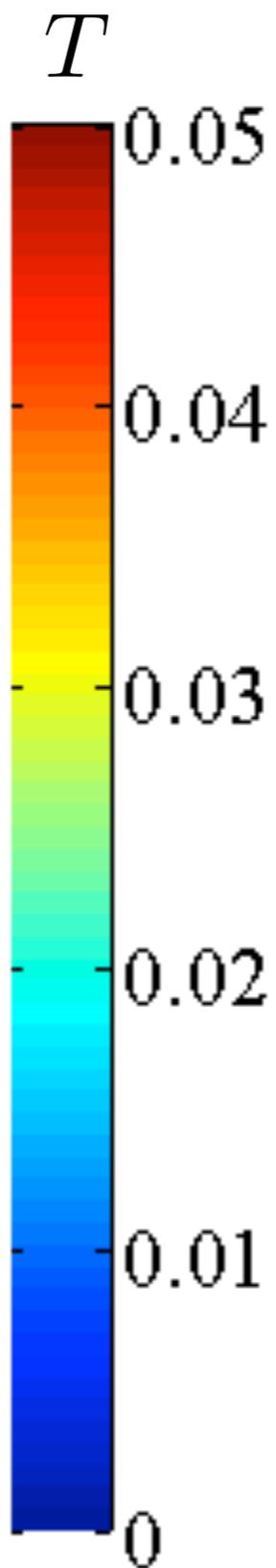
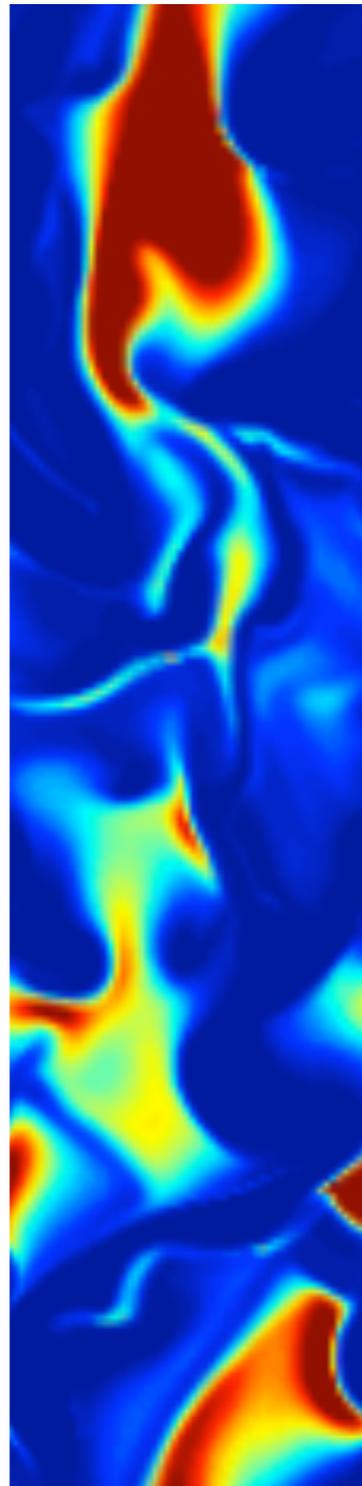
Bimodal PSD ($e = 0.95$)

Assumption:
 $Kn \ll 1$

$$Kn = \frac{l_{mf}}{l_{grad}}$$

$$l_{mf} \approx \frac{d}{6\sqrt{2}\phi}$$

$$l_{grad} = \left| \frac{\bar{\chi}}{\nabla\chi} \right|$$



Summary



Summary



- HYS drag model has been implemented within new CVS version of MFIX.

- HYS drag model has been implemented within new CVS version of MFIX.
- GHD theory has been implemented within MFIX and operates robustly, even in very inhomogeneous gas-solid flows.

- HYS drag model has been implemented within new CVS version of MFIX.
- GHD theory has been implemented within MFIX and operates robustly, even in very inhomogeneous gas-solid flows.
- Binary fluidized gas-solid suspensions manifest inhomogeneous structures similar to monodisperse systems.

- HYS drag model has been implemented within new CVS version of MFIX.
- GHD theory has been implemented within MFIX and operates robustly, even in very inhomogeneous gas-solid flows.
- Binary fluidized gas-solid suspensions manifest inhomogeneous structures similar to monodisperse systems.
- Volume averaged slip velocities in both monodisperse and bidisperse gas-solid flows are qualitatively similar when both PSDs have the same Sauter mean diameter.

- HYS drag model has been implemented within new CVS version of MFIX.
- GHD theory has been implemented within MFIX and operates robustly, even in very inhomogeneous gas-solid flows.
- Binary fluidized gas-solid suspensions manifest inhomogeneous structures similar to monodisperse systems.
- Volume averaged slip velocities in both monodisperse and bidisperse gas-solid flows are qualitatively similar when both PSDs have the same Sauter mean diameter.
- The scale of structures in binary gas-solid flows depends on grid resolution, similar to monodisperse suspensions.

- HYS drag model has been implemented within new CVS version of MFIX.
- GHD theory has been implemented within MFIX and operates robustly, even in very inhomogeneous gas-solid flows.
- Binary fluidized gas-solid suspensions manifest inhomogeneous structures similar to monodisperse systems.
- Volume averaged slip velocities in both monodisperse and bidisperse gas-solid flows are qualitatively similar when both PSDs have the same Sauter mean diameter.
- The scale of structures in binary gas-solid flows depends on grid resolution, similar to monodisperse suspensions.
- Knudsen number was found to be $O(1)$ or less throughout simulation domain.

Acknowledgements



People:

- Jin Sun
- Sebastian Chialvo
- Yesim Igci
- Jia Chew

Funding:

- US Department of Energy
- ExxonMobil Corporation
- ACS Petroleum Research Fund