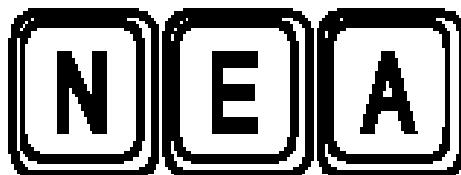


# Reaction Mechanisms For Entrained-Flow Coal Gasification

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NETL 2010 Multiphase Flow Science Workshop  
May 5, 2010 Pittsburgh, PA



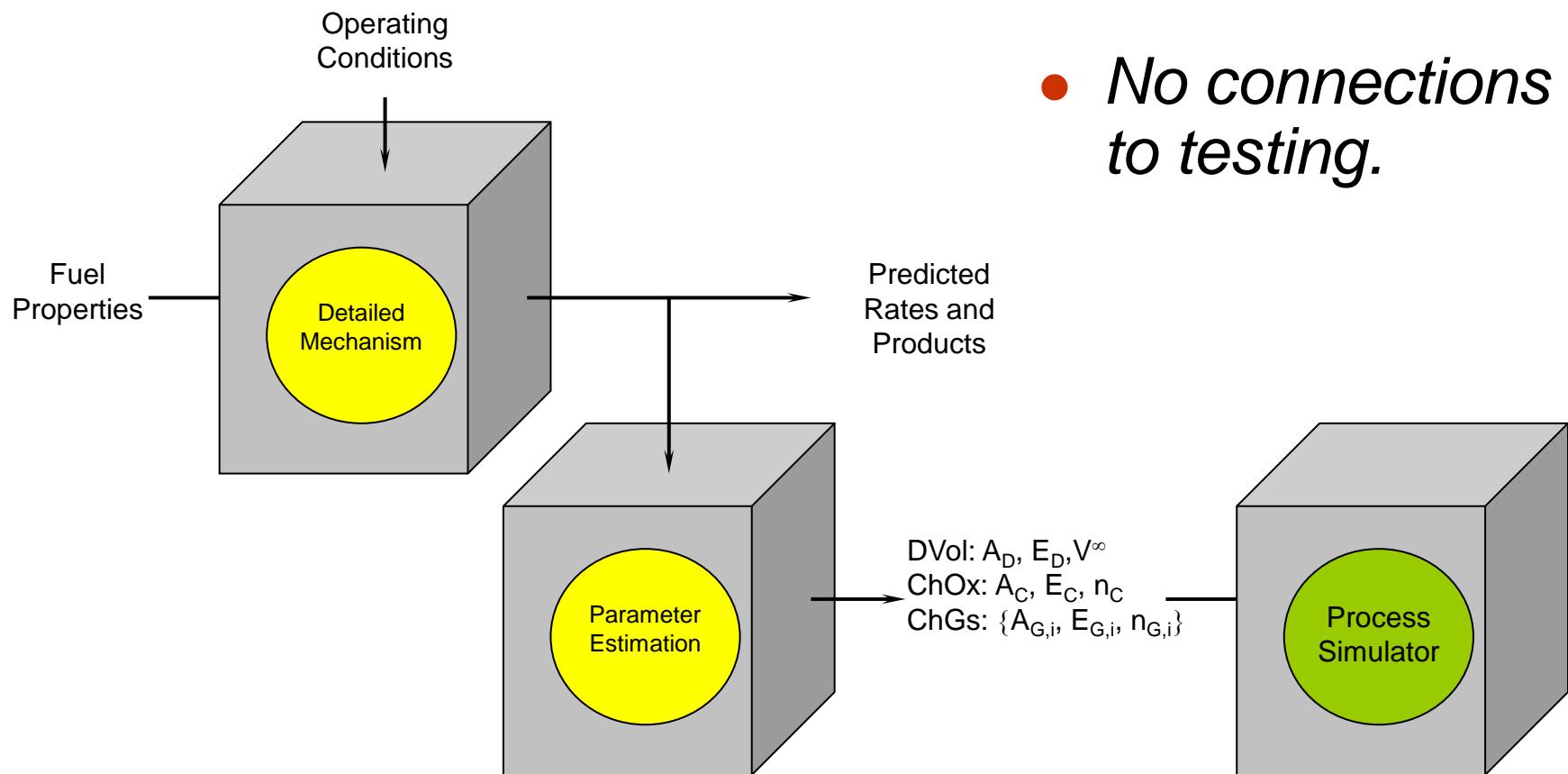
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# All Rate Parameters Should Be Assigned From Readily Available Fuel Properties



200 ms, S.R.=0.38

# There are Six Distinct Stages of Fuel Conversion Chemistry

## ***Devolatilization***

- Source of all gaseous fuels and soot.
- Determines char yield, size, structure, and initial reactivity.

## ***Secondary Volatiles Pyrolysis***

- Release of noncondensibles at moderate temperatures.
- Conversion of tars into soot at high temperatures.

## ***Homogeneous Conversion***

- Restricted to the gas phase.
- Major heat source.
- Partial combustion of primary volatiles.
- Major source of CO, H<sub>2</sub>, CO<sub>2</sub>, and H<sub>2</sub>O.
- Shifting/reforming chemistry throughout.

## ***Heterogeneous Secondary Chemistry***

- Deposition of coke from gaseous volatiles.
- Basis for NO reduction on soot.
- Char catalyzed water/gas shifting.

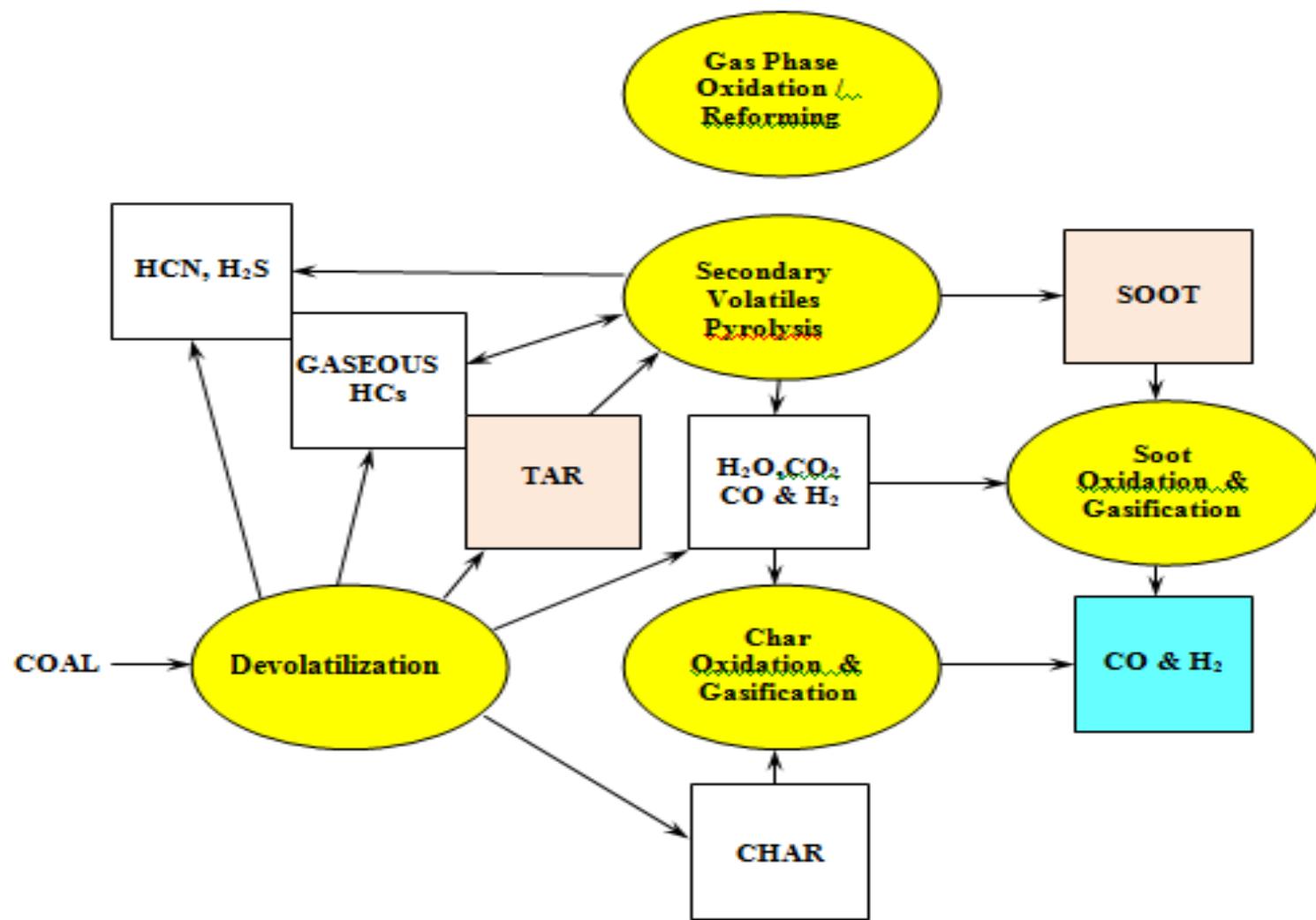
## ***Char/Soot Oxidation***

- Major heat source.
- Determines residual char yield for gasification.
- Some flyash production.

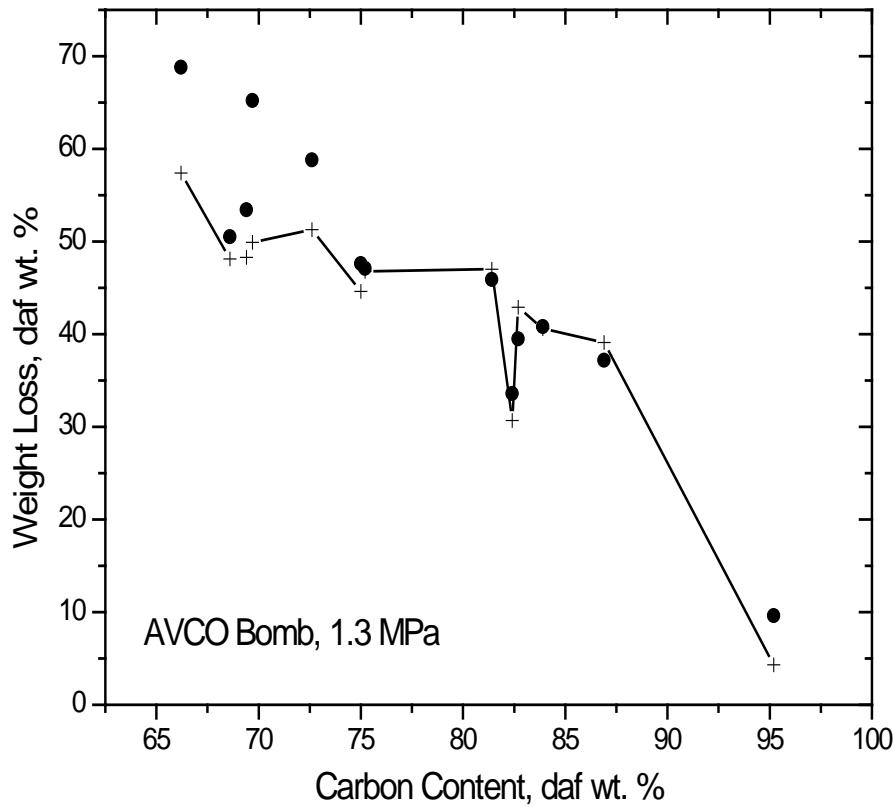
## ***Char/Soot Gasification***

- Determines overall conversion.
- Flyash production, via char particle fragmentation + ash agglomeration.

# Gasification Chemistry

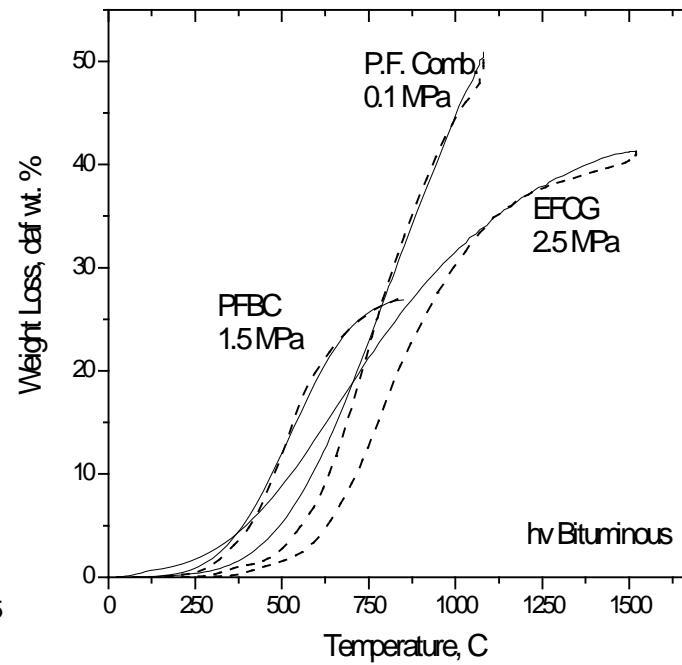
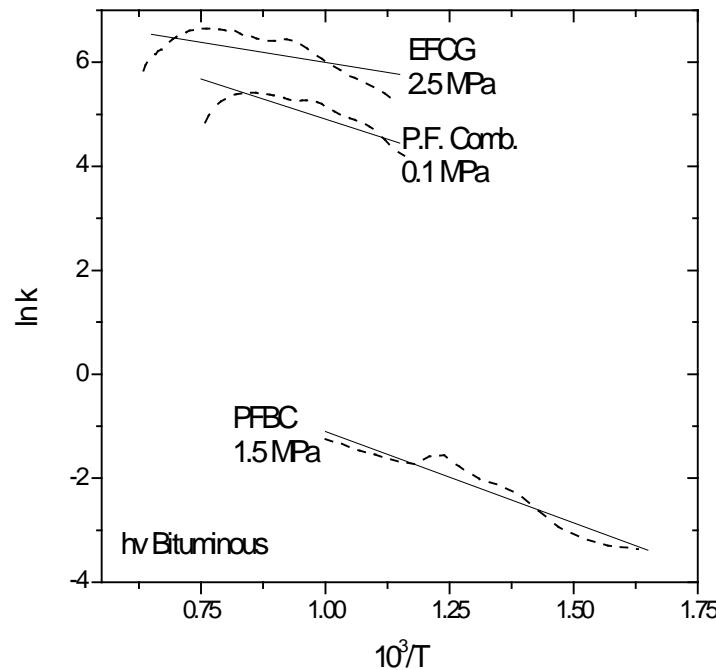


# Accurate Predictions for Devolatilization of Any Coal Type



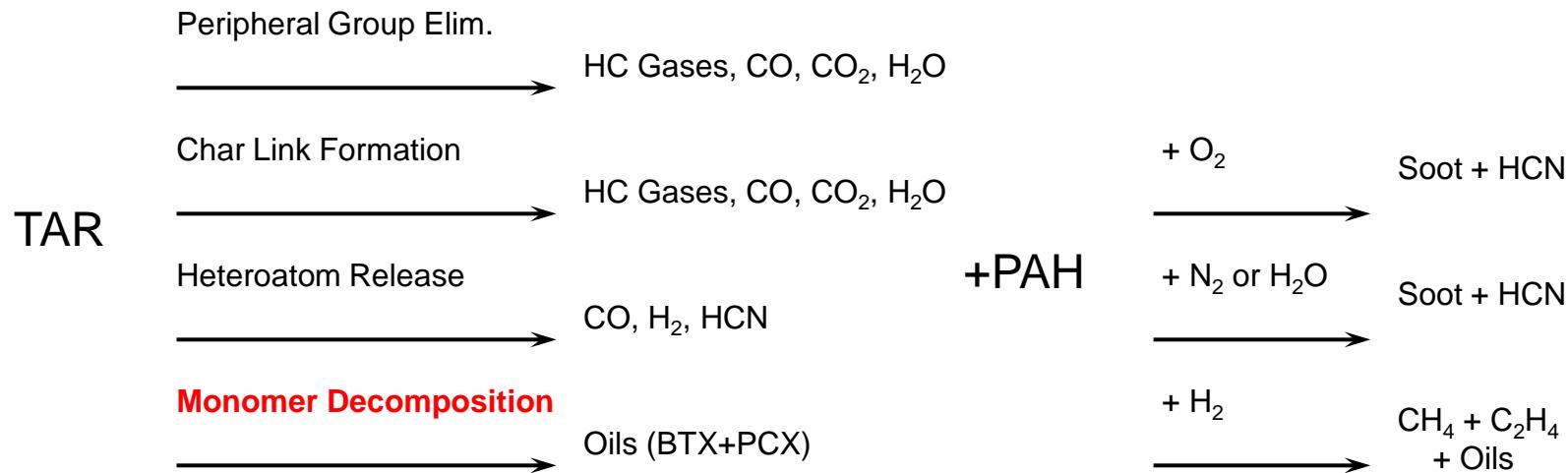
- *Depicts the distinctive yields of individual samples of even the same coal rank.*
- *Based on only the proximate and ultimate analyses.*

# Automatically Assign All Parameters In Simple Devolatilization Rate Laws



- Even the SFOR matches the FC predictions.
- Assigned  $E_{ACT}$  are constant over a broad range of heating rate.
- Rate laws can be specified for any product, including volatile-N.

# Tar Conversion Mechanism Is Well-Characterized



FC Reaction Sequence + *PAH Conversion*  
+ *Oils Production* (?) *Into Soot*

OPERATING CONDITIONS:

90.0 micron particles at 25. C are entrained in N<sub>2</sub>  
 with 15.0% CO<sub>2</sub>, 30.0% H<sub>2</sub>O, 5.0% CO and 5.0% H<sub>2</sub>  
 at 1600. C in a furnace at 1600. C for .100E+02 s.  
 The ambient pressure is 2.00 MPa.

Primary Pyrolysis Products, daf wt.%	Secondary Pyrolysis Products, daf wt.%				
	Soot Fr.= 0.2	0.4	0.6	0.8	1.0

Tar	22.5	18.0	13.5	9.0	4.5	0.0
Soot	0.0	4.1	8.3	12.4	16.5	20.6
H <sub>2</sub>	1.89	2.17	2.44	2.77	3.16	3.54
CH <sub>4</sub>	1.6	1.64	1.72	1.45	0.82	0.20
C <sub>2</sub> H <sub>2</sub>	0.0	0.00	0.00	0.00	0.00	0.00
C <sub>2</sub> H <sub>4</sub>	0.66	0.5	0.4	0.3	0.1	0.0
C <sub>2</sub> H <sub>6</sub>	0.16	0.1	0.0	0.0	0.0	0.0
C <sub>3</sub> H <sub>6</sub>	0.53	0.3	0.1	0.0	0.0	0.0
C <sub>3</sub> H <sub>8</sub>	0.00	0.0	0.0	0.0	0.0	0.0
CO	2.2	2.5	2.9	3.4	4.0	4.7
CO <sub>2</sub>	3.2	3.2	3.2	3.2	3.2	3.2
H <sub>2</sub> O	6.1	6.1	6.1	6.1	6.1	6.1
HCN	1.23	1.28	1.34	1.39	1.45	1.50
H <sub>2</sub> S	0.54	0.56	0.58	0.60	0.62	0.64
Char	59.5					

Condensed Product Composition, daf wt.%					
	% C	% H	% O	% N	% S

Tar	85.6	5.8	7.3	0.94	0.41
Soot	98.7	1.0	0.0	0.34	0.00
Char	99.4	0.5	0.0	0.09	0.00

- *Secondary pyrolysis products are accurately predicted from primary products.*
- *Assume instantaneous conversion for EF conditions.*

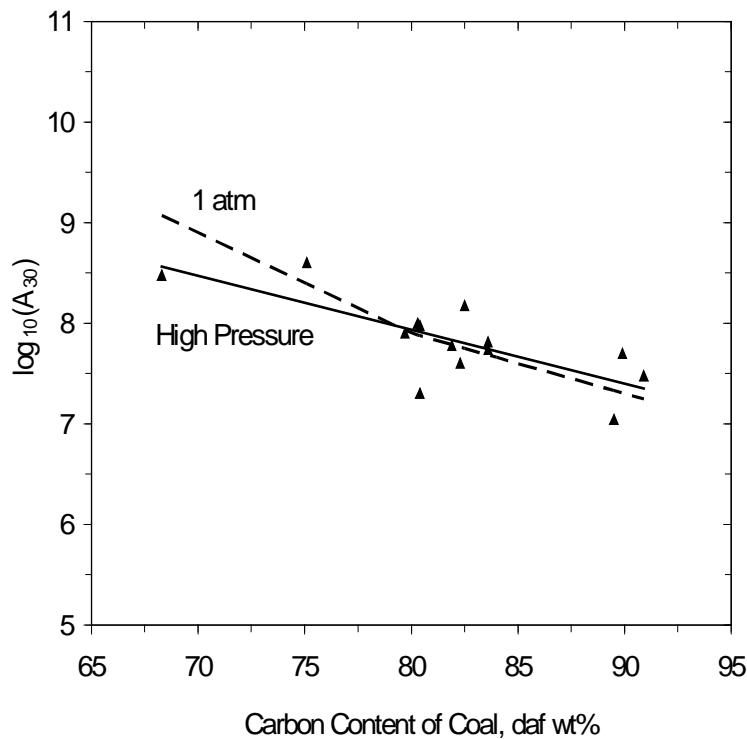
Coal	Soot Yield, daf wt. %	% of Wt. Loss
Pit. #8	22.9 - 29.1	43 - 57
Ill. #6	21.0	40
PRB	9.1	19

# Carbon Burnout Kinetics Model for Char Oxidation & Char Gasification

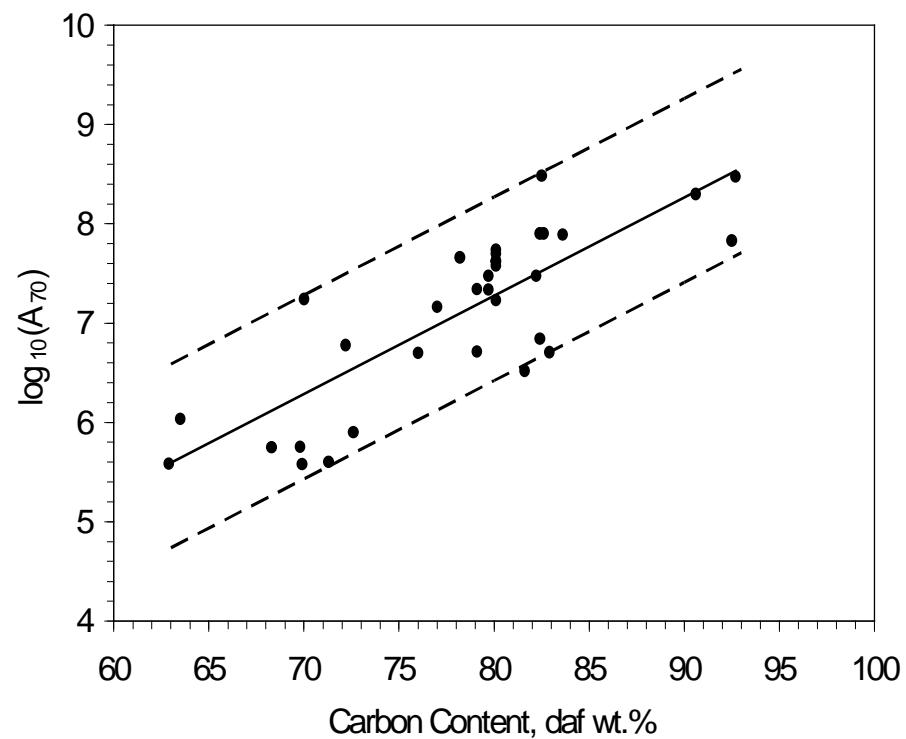
- CBK includes single-film char combustion, intraparticle reaction/diffusion, thermal annealing, and ash inhibition.
  - Combustion  $2C + O_2 \rightarrow C(O) + CO$   
 $C + C(O) + O_2 \rightarrow C(O) + CO_2$   
 $C(O) \rightarrow CO$
  - Gasification  
 $C + CO_2 \leftrightarrow C(O) + CO$   
 $C(O) \rightarrow CO$   
 $C + H_2O \leftrightarrow C(O) + H_2$   
 $C + 2H_2 \rightarrow CH_4$  (slow)
  - CBK/E was validated against a database of 235 independent tests that characterized 11 coals, 2 coal chars, and a graphite, heating rates approaching  $10^6$  °C/s, furnace temperatures to 1527 °C, pressures to 2.0 MPa, and O<sub>2</sub> levels to 100 %.
  - CBK/G was validated against a database of 452 independent tests that characterized 26 coals, heating rates approaching  $10^5$  °C/s, furnace temperatures to 1500 °C, pressures to 3.0 MPa, and broad ranges of CO<sub>2</sub>, H<sub>2</sub>O, CO, and H<sub>2</sub> levels.

# A One-Point Calibration is Needed for Every Fuel Sample

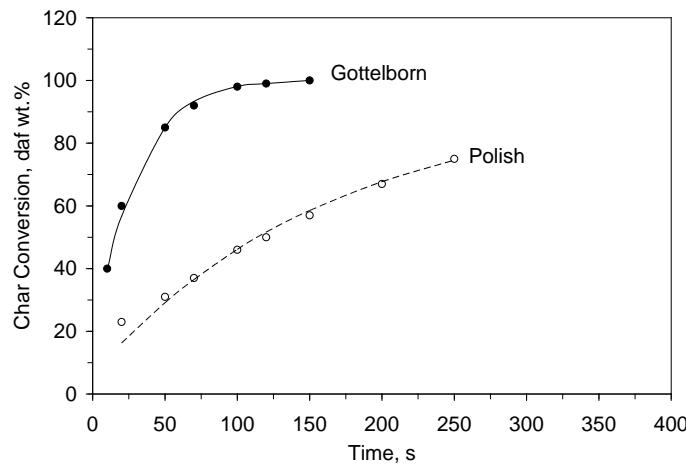
*Oxidation*



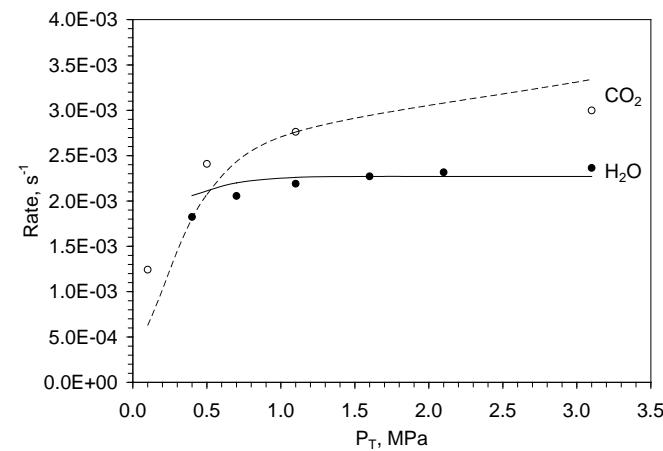
*Gasification*



# CBK/G Performs Well Over A Broad Domain of Gasification Conditions



Predicted (curves) and measured (data points) char conversion histories for (● and solid line) Polish and (○ and dashed line) Gottelborn chars at 1500°C and 0.1 MPa pure CO<sub>2</sub> in a WMR (Moors, 1998).

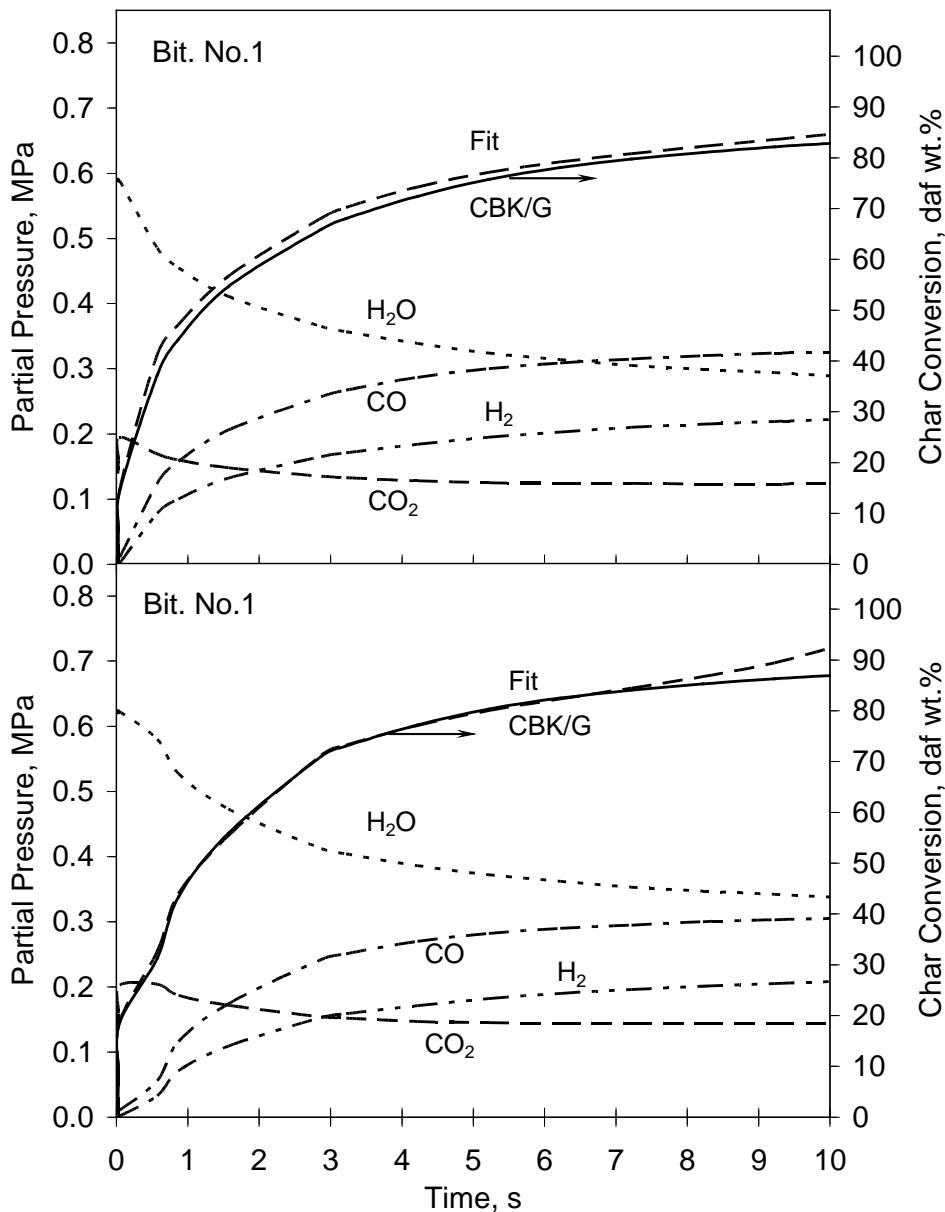


Predicted (curves) and measured (data points) rates of Xiao Long Tan lignite char gasification at (● and solid line) 850°C in 80 % H<sub>2</sub>O, 10 % H<sub>2</sub>, and 10 % CO, and at (○ and dashed line) 900°C in 90 % CO<sub>2</sub> and 10 CO % (Sha et al., 1990).

# Char Conversion In Whole Syngas

Gas Mixture	Char Conversion, %
25 % H <sub>2</sub> O	49.4
+25 % H <sub>2</sub>	11.2
+25 % H <sub>2</sub> , 10 % CO <sub>2</sub> , 40 % CO	12.7

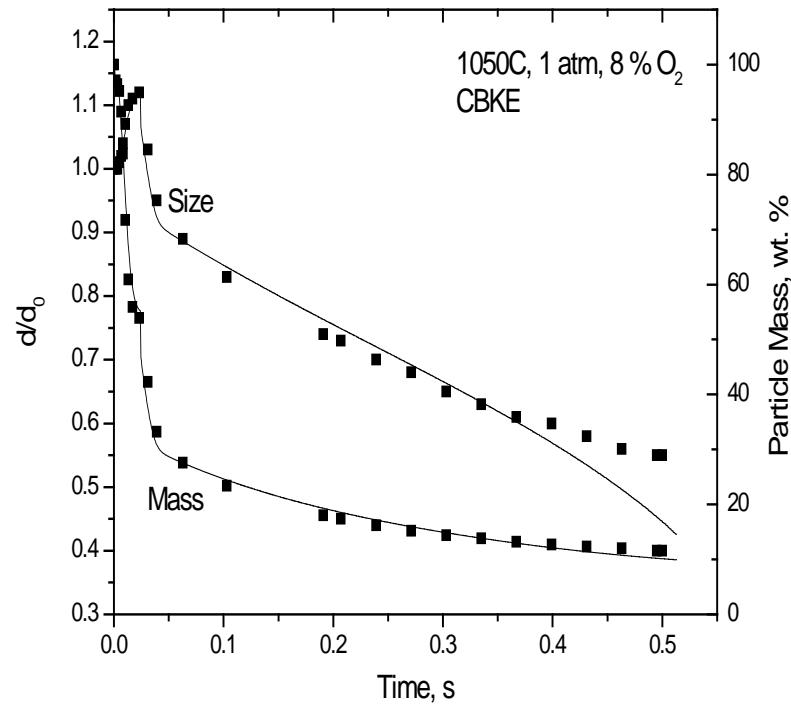
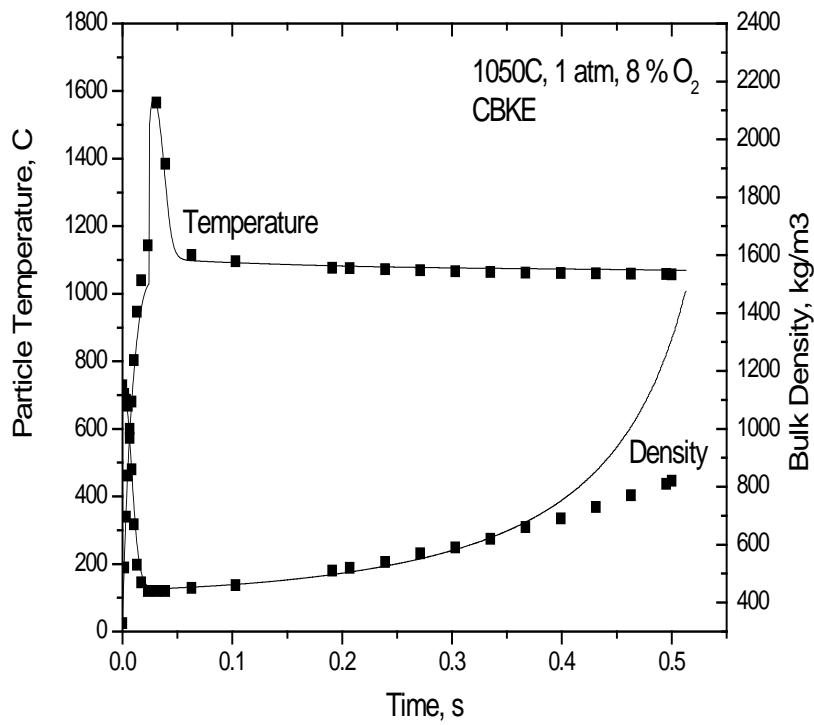
- Little literature data on whole syngas; mostly pure CO<sub>2</sub> or pure H<sub>2</sub>O.
- SRI can run any H<sub>2</sub>O/CO<sub>2</sub>/CO/H<sub>2</sub> mixture to 4.0 MPa.
- Severe inhibition of steam gasification by H<sub>2</sub>.
- Negligible contribution from CO<sub>2</sub> gasification.



# Automatically Assign All Gasification Rate Parameters

- The global rate matches the CBK/G predictions for complex mixtures.
- The global rate also performs well in modest extrapolations.

# NEA's Global Rates In Fluent Reproduce the PC Coal Lab® Results

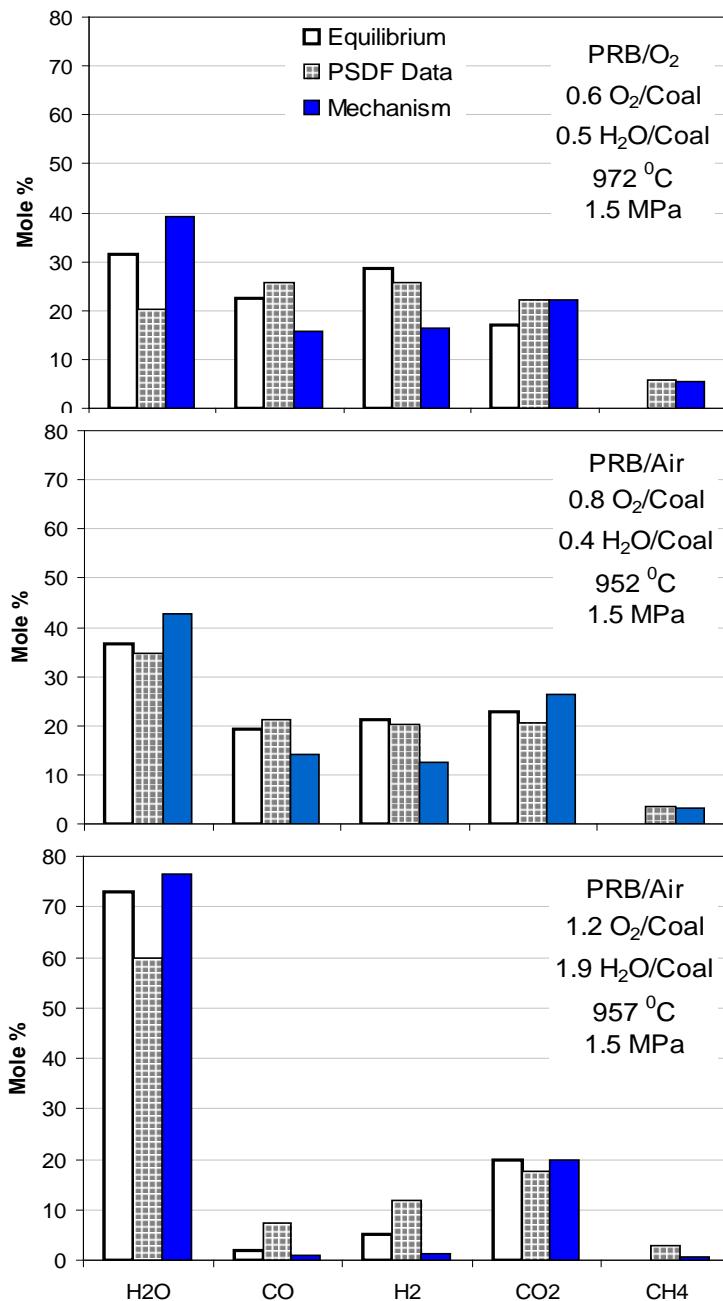


# Homogeneous Reaction Mechanism

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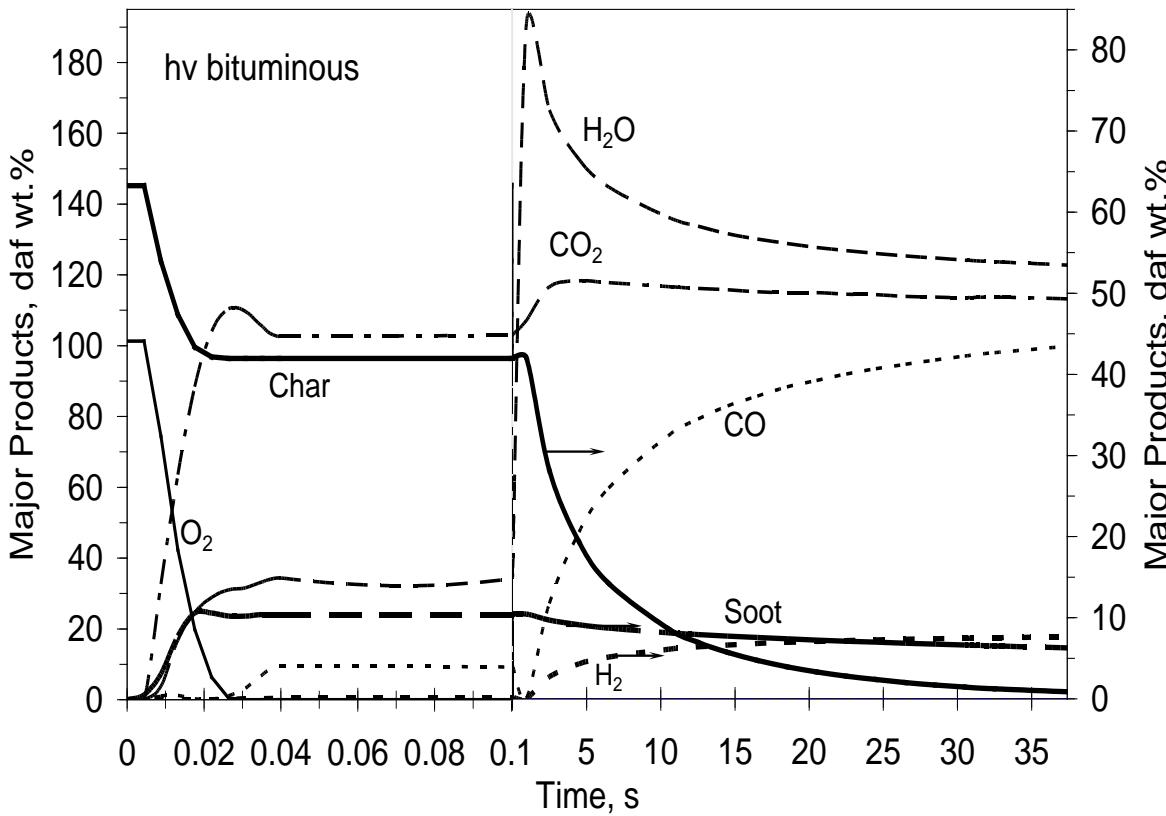
- 555 reactions, 154 species.
- Includes C<sub>1</sub>-C<sub>3</sub> GHCs, benzene, toluene, and phenol.
- Includes all major IOGs (H<sub>2</sub>, H<sub>2</sub>O, CO, CO<sub>2</sub>, etc.)
- S- & N-species omitted at this stage.
- Validated for 275≤T,C≤1425;  
1≤P,atm≤42; and 0.65≤S.R.≤3.30

# PSDF Consistency Check



- Data on PRB subbituminous & HWA bituminous
  - Impose the actual S.R., T, P, H<sub>2</sub>O/Coal, & O<sub>2</sub>/Coal
- Abundant CH<sub>4</sub> in the product gas
- Predicted CO & H<sub>2</sub> too low; H<sub>2</sub>O too high but closer to equilibrium
- Correct tendencies among these cases with variation in O<sub>2</sub>/Coal & H<sub>2</sub>O/Coal

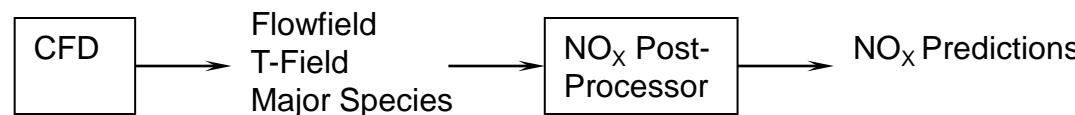
# 1D Gasifier Simulation With Detailed Ignition Chemistry & Equilibrated Syngas Composition



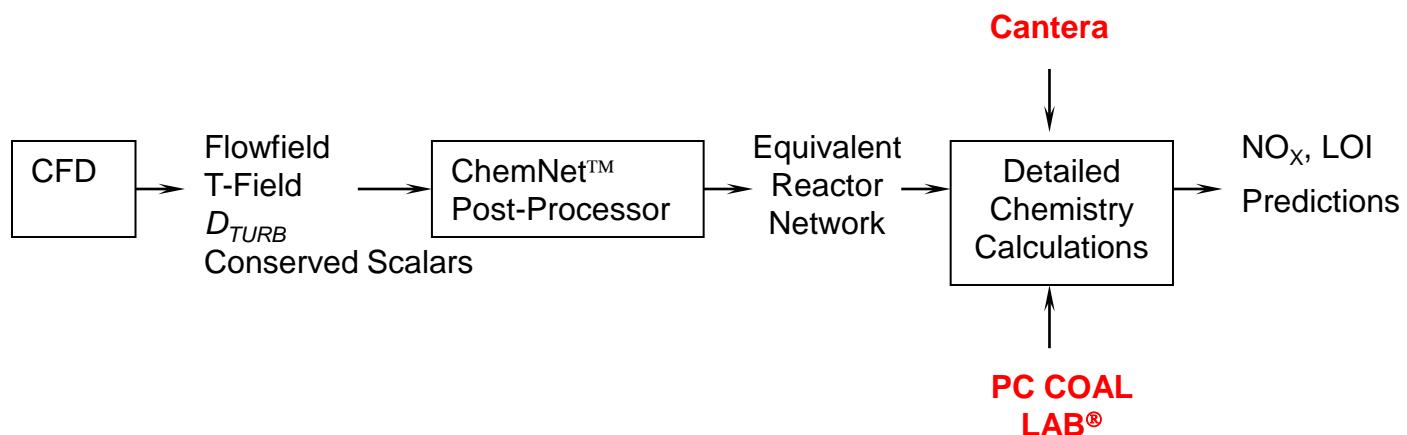
- First-stage calculation based on full kinetics to determine  $X_{char}$  and  $X_{soot}$ .
- Steam injection into a reducing second stage.
- Equilibrium gas compositions shift throughout the second stage.
- Steam gasification with strong CO inhibition.
- Soot persists.

# NEA's ChemNet™ Post-Processing (CNPP)

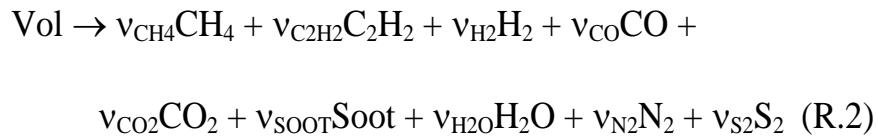
## Conventional Post-Processing



## ChemNet™ Post-Processing



# Severe Implementation Obstacles for CFD



- *Solvers do not handle irreversible chemistry with radiation & particle dynamics.*
- *Only a handful of species can be included.*
- *Fluent v.5.5 could not converge a 2D axisymmetric coal-flow with this chemistry.*

# Summary

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- *Accurately predict devolatilization behavior based on prox/ult analyses without lab support.*
- *After a 1-point calibration, CBK accurately predicts oxidation and gasification of char & soot for diverse conditions.*
- *Comprehensive mechanisms automatically specify all parameters in global rate laws.*
- *Difficult to implement even a skeletal gasification mechanism in CFD.*

# Forget “Understanding” and Focus On *Accuracy* in Applications

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- *Fuel Science* **SHOULD** specify all the rate parameters used in process simulations (CFD, AspenPlus, HySys, etc.)
- *Simulation practitioners* should **NOT** have to comb literature or resort to default values.

# Multifuels Capability Requires Detailed Volatiles Compositions

	SD	SG	JR	GL	PR	JW
Volatile, daf wt. %						
Wt. Loss	<b>86.1</b>	<b>86.0</b>	65.2	56.5	59.8	39.7
Soot	<b>4.3</b>	<b>13.4</b>	30.1	33.7	37.9	26.8
CH <sub>4</sub>	<b>7.1</b>	<b>7.4</b>	0.7	0.4	0.5	0.3
C <sub>2</sub> H <sub>2</sub>	<b>2.2</b>	<b>1.3</b>	1.5	1.0	1.3	2.3
C <sub>2</sub> H <sub>4</sub>	1.4	1.5	0.0	0.0	0.0	0.0
H <sub>2</sub>	2.1	1.7	<b>3.4</b>	<b>3.6</b>	<b>4.0</b>	<b>3.5</b>
CO	<b>48.4</b>	<b>41.5</b>	12.9	7.2	6.1	1.7
CO <sub>2</sub>	<b>8.2</b>	<b>8.0</b>	6.4	2.2	1.7	1.0
H <sub>2</sub> O	<b>12.1</b>	<b>7.7</b>	<b>7.6</b>	4.9	4.3	1.8
HCN	0.0	0.0	1.26	2.47	2.24	1.52
NH <sub>3</sub>	<b>0.24</b>	<b>2.90</b>	0.0	0.0	0.0	0.0
H <sub>2</sub> S	0.0	0.44	0.42	1.17	1.91	0.96
Char Comp., daf wt. %						
C	94.7	97.1	98.9	98.4	98.5	98.2
H	3.4	2.5	0.5	0.5	0.4	0.5
O	1.9	0.4	0.0	0.0	0.0	0.0
N	0.0	0.0	0.4	1.1	1.0	1.26
S	0.0	0.0	0.1	0.1	0.1	0.0
Char ash, wt. %	2.5	<b>75.7</b>	15.9	14.2	<b>30.9</b>	21.8
Char size, $\mu\text{m}$	<b>97.6</b>	<b>103.6</b>	29.9	59.1	54.1	41.7

*Biomass has:*

- *Higher volatile yields.*
- *Less soot and H<sub>2</sub>.*
- *More HCs and CO.*
- *No char-N.*
- *Larger char sizes.*
- *SG also produces abundant NH<sub>3</sub> and a very high char ash content.*