

Development of a Two-Fluid Drag Law for Clustered Particles using Direct Numerical Simulation

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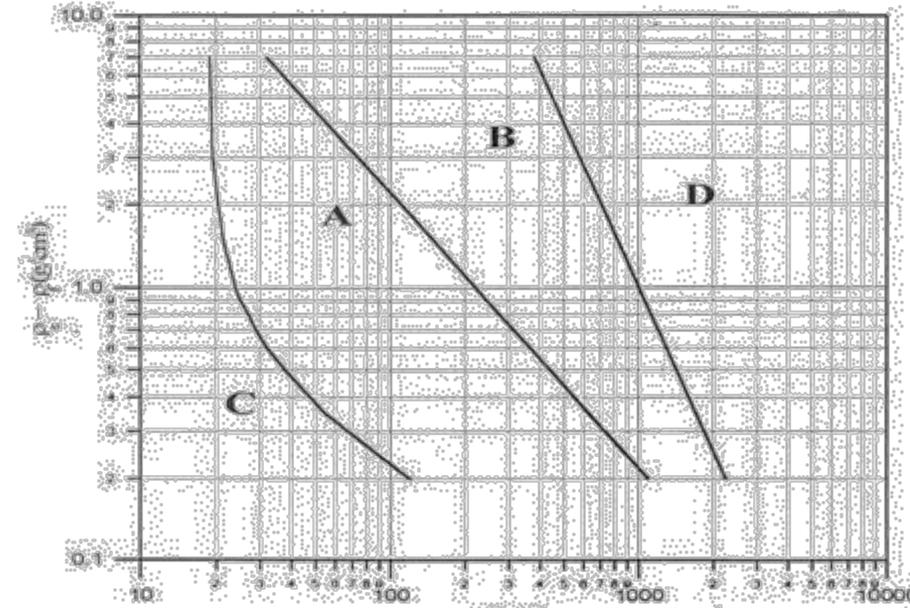


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Introduction

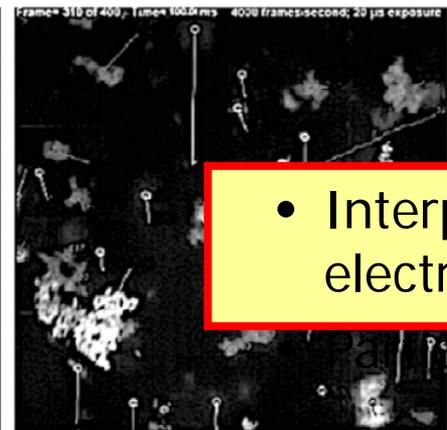
- Geldart classification
 - Geldart B particles
 - Higher Re_m and St
 - Uniform particle configuration
 - Geldart A Particles
 - Lower Re_m and St
 - Formation of particle clusters



Plascoat™ 571 polyethylene

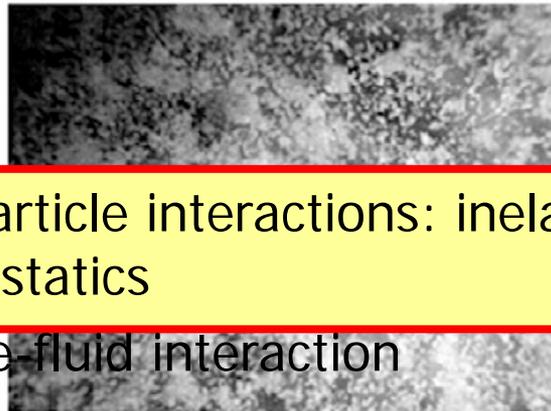
FCC catalyst in the bed

- Interparticle interactions: inelasticity, cohesion, electrostatics



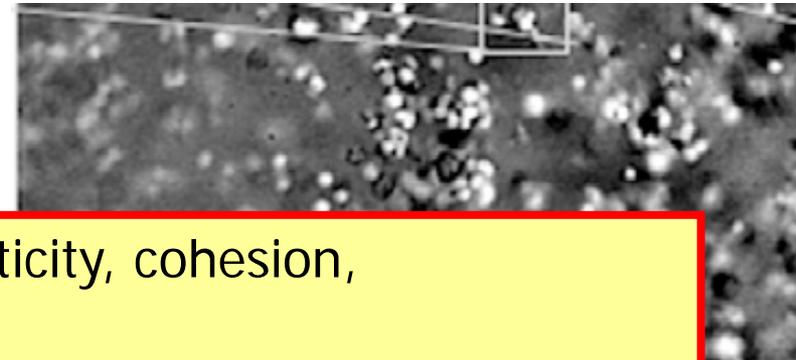
○ ← 100 μm Diameter

In the free board



○ ← 100 μm Diameter

In the fluidized bed



○ ← 100 μm Diameter

Cocco et al., Particle clusters in and above fluidized beds, *Powder Technology*, 2010

Collaboration with Experiments at FIU

❑ Florida International University

Circulating Fluidized Bed

➤ Dr. Seckin Gokaltun

Bubbling Bed

Filter bag

Acrylic riser
2' X 5"

High speed camera

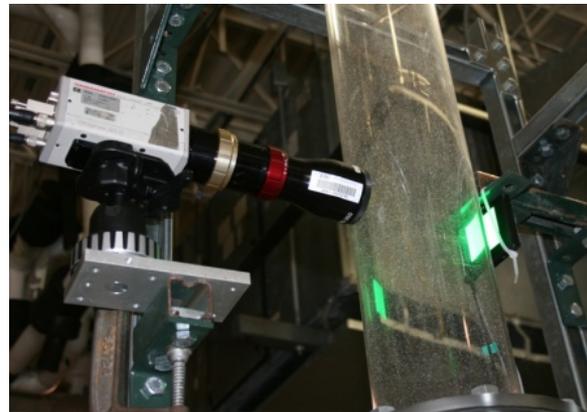
Distributor plate

Rotameter

Pressure regulator



Pressure sensors



Cyclonic separator

Stand pipe

Down comer

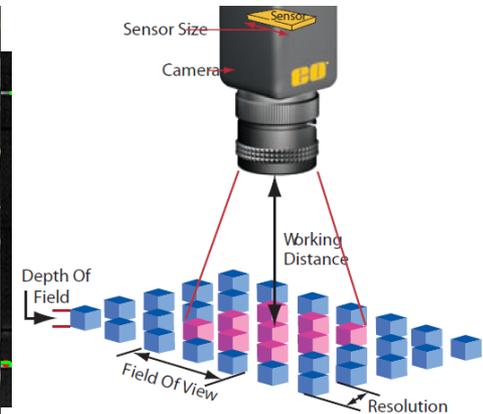
Gate valve



Acrylic Riser
6" X 10'

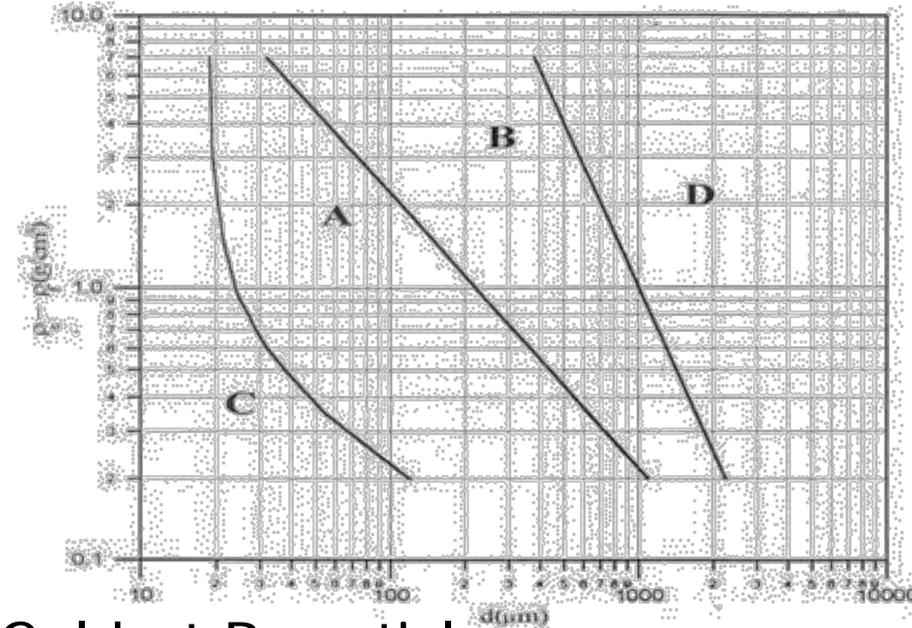
Distributor plate

Inlet Plenum



Abbasi Baharanchi, A., Gokaltun, S., Munroe, N., Dulikravich, G., *An Experimental Study Using High Speed Imaging of Clustered Particles for a More Accurate Drag Law in MFI*, NETL Workshop, 2013.

- Geldart classification
 - Geldart B particles
 - Higher Re_m and St
 - Uniform particle configuration
 - Geldart A Particles
 - Lower Re_m and St
 - Formation of particle clusters
- Several drag laws available for Geldart B particles
 - Ergun(1952), Wen-Yu (1966), DNS: Hill et al (2001), van der Hoef et al (2005, 2007), Tenneti et al (2011)
- Comparison of CFD results for Geldart A systems forming particle clusters (using uniform configuration drag laws) with experimental results
 - Inaccurate pressure drop/bed expansion



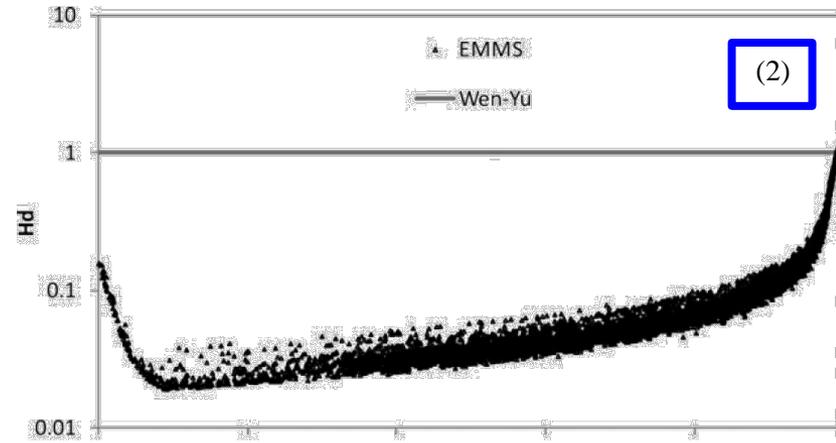
Current Cluster Drag Models

- Current state-of-the-art clustered drag model used in CFD
 - Energy minimization multi scale model⁽¹⁾ (EMMS)
 - Based on the minimum energy required for suspending and transporting dense particle regions
 - Accounts for the effect of heterogeneous structures on drag through a *drag index*

$$\beta = \begin{cases} 150 \frac{\varepsilon_s (1 - \varepsilon_g) \mu_g}{\varepsilon_g d_p^2} + 1.75 \frac{\rho_g}{d_p} \varepsilon_s |\mathbf{v}_g - \mathbf{v}_s| & \varepsilon_g < 0.4 \\ \frac{3}{4} C_D \frac{\rho_g \varepsilon_g \varepsilon_s |\mathbf{v}_g - \mathbf{v}_s|}{d_p} \varepsilon_g^{-2.65} H_d & \varepsilon_g \geq 0.4 \end{cases}$$

Wen-Yu
correlation

Drag
index



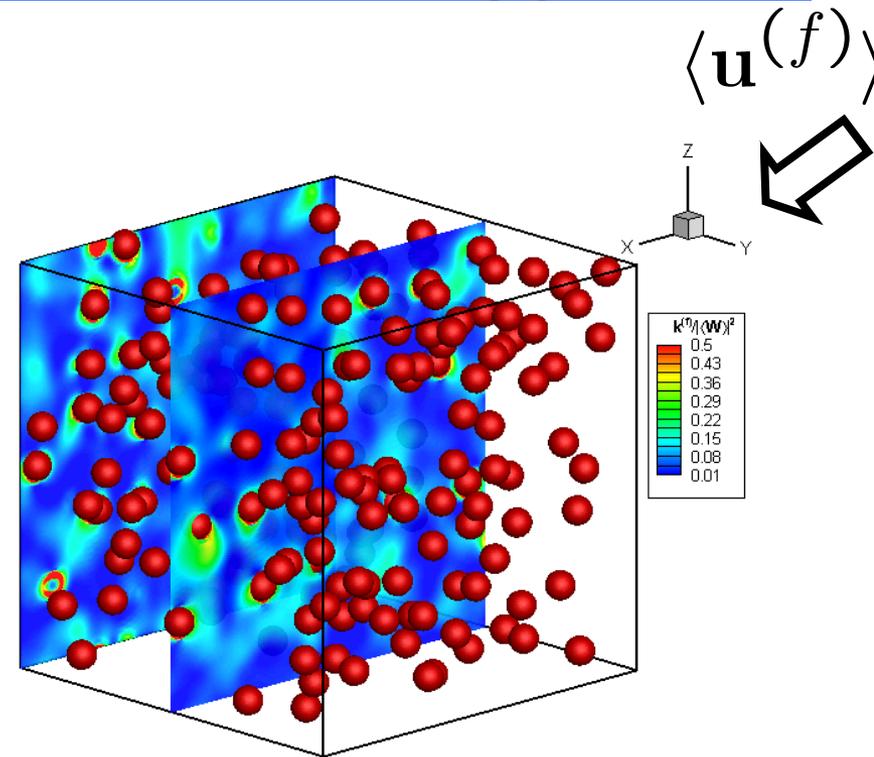
While EMMS is useful, there is scope for an improved clustered drag law

⁽¹⁾ Li, J., Kwauk, M., *Particle-Fluid Two-Phase Flow: the Energy-Minimization Multi-Scale Method; Metallurgy*, Beijing: Industry Press, 1994.

⁽²⁾ Benyahia, S., *Analysis of Model Parameters Affecting the Pressure Profile in a Circulating Fluidized Bed*, AIChE Journal, 2012, 58 (2).

PR-DNS Simulation Approach

- ❑ Particle-resolved direct numerical simulation (PR-DNS) of flow past random configurations of fixed particles
- ❑ periodic domains approximate statistically homogeneous suspensions well¹
- ❑ impose constant mean pressure gradient
- ❑ volume-averaging to estimate ensemble-averaged quantities

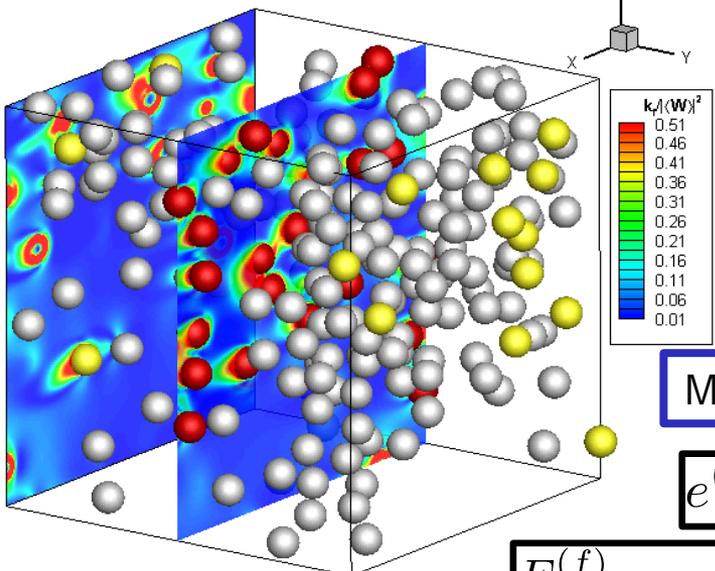


- Demonstrated numerical convergence and accuracy
- Validated in suite of test cases

¹“Drag law for monodisperse gas–solid systems using particle-resolved direct numerical simulation of flow past fixed assemblies of spheres” S. Tenneti, R. Garg, S. Subramaniam *International Journal of Multiphase Flow*, 37(9), p 1072-1092

Freely evolving non-cohesive suspensions

Freely moving particles undergoing collisions



- Rate of work done by constant mean pressure gradient in maintaining flow

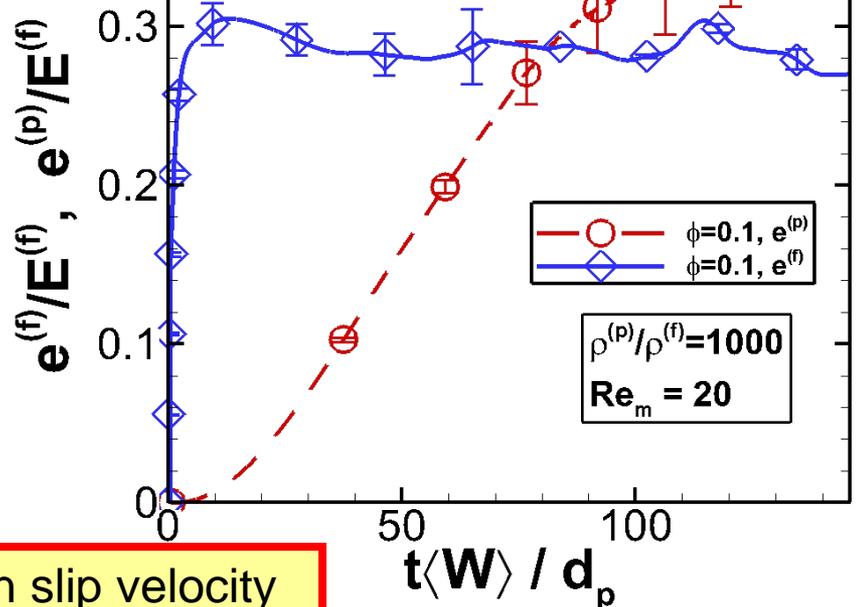
$$\langle \mathbf{W} \rangle \cdot \langle \mathbf{S}_M^{(f)} \rangle = \Pi^{(f)} + \Pi^{(p)}$$

Mean Slip X Mean Drag Production of $k^{(f)}$ Production of $k^{(p)}$

$$e^{(f)} = \rho_f (1 - \phi) k^{(f)}$$

$$e^{(p)} = \rho_p \phi k^{(p)}$$

$$E^{(f)} = \rho_f \langle \mathbf{W} \rangle \cdot \langle \mathbf{W} \rangle / 2$$



~~$$\rho_f (1 - \phi) \frac{dk^{(f)}}{dt} = \Pi^{(f)}$$

unsteady term~~

$$= \underbrace{\Pi^{(f)}}_{\text{viscous dissipation}} - \underbrace{2\mu_f \langle I_f s_{ij} s_{ij} \rangle}_{\text{viscous dissipation}}$$

~~$$\rho_p \phi \frac{dk^{(p)}}{dt} = \Pi^{(p)}$$

unsteady term~~

$$= \underbrace{\Pi^{(p)}}_{\text{collisional dissipation}} - \underbrace{\Gamma_{\text{coll}}^{(p)}}_{\text{collisional dissipation}}$$

Particle velocity fluctuations scale with mean slip velocity

Homogeneous Cooling Cohesive Granular Gas

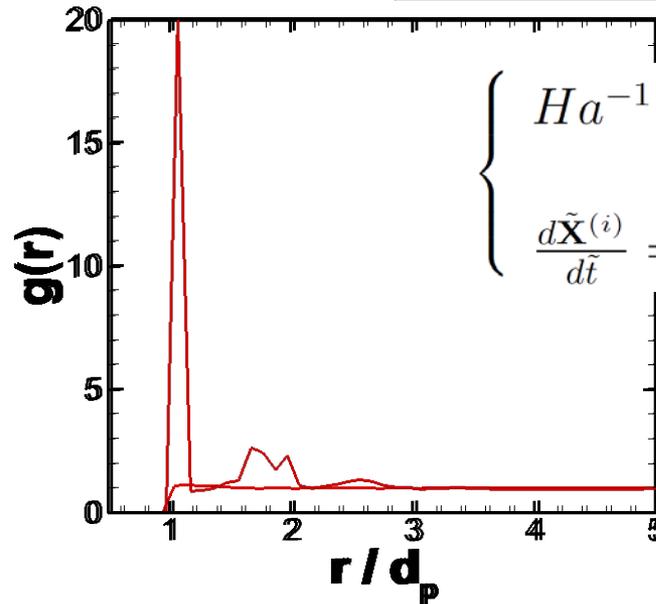
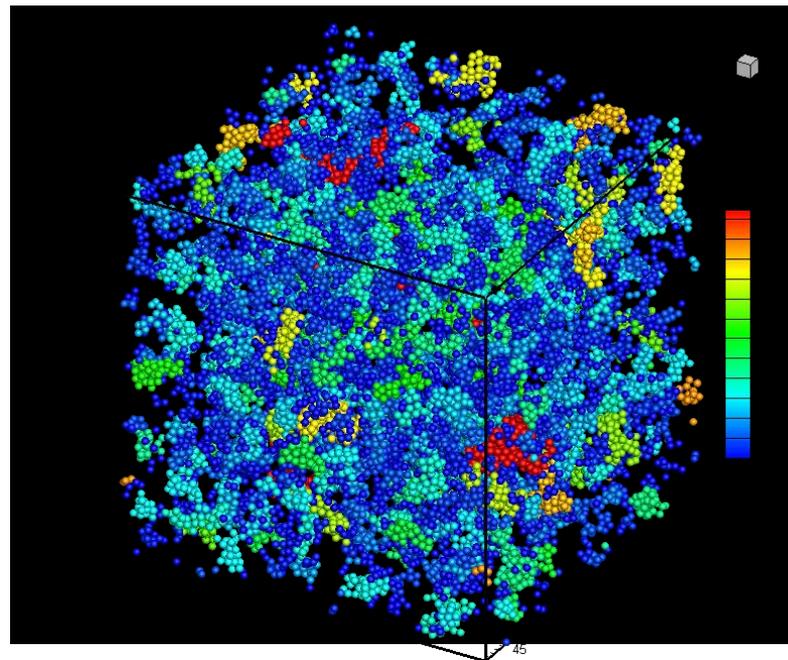
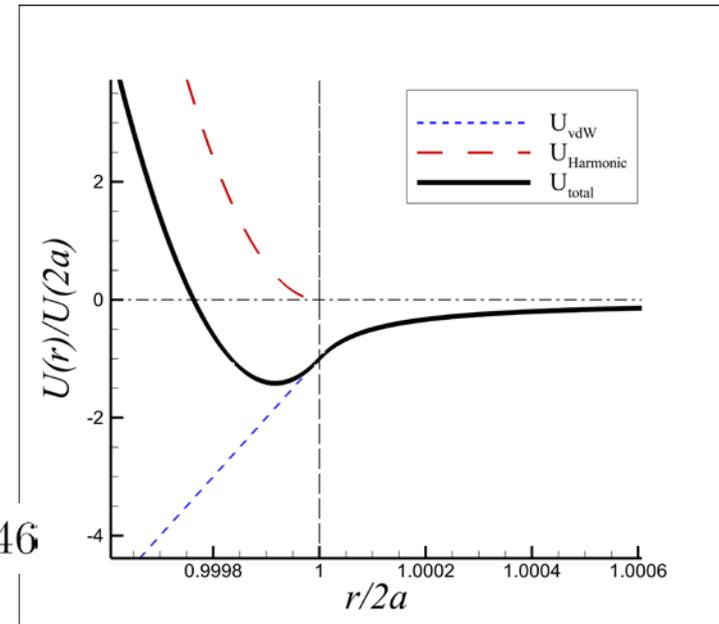
- Soft-sphere DEM of cohesive particles: van der Waals interaction and linear-spring-dashpot on contact

(Eric Murphy)

$$Ha = \frac{A}{\rho \pi d_p^2 d_0 T}$$

Ha is the ratio of adhesion energy to particle kinetic energy (granular temperature)

$$\phi = 0.084, Ha = 2.4, d_0/d_p = 10^{-4}, L/d_p = 50, N = 20146$$

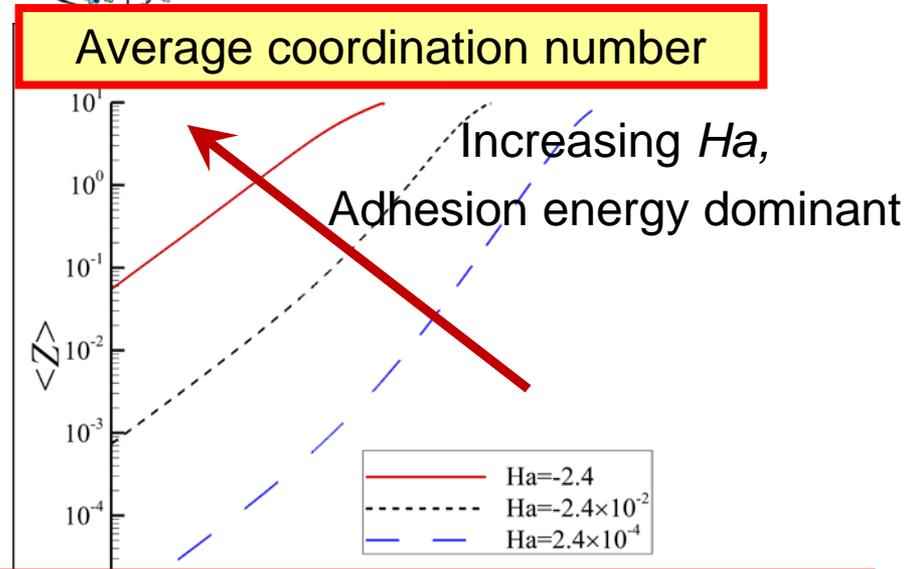
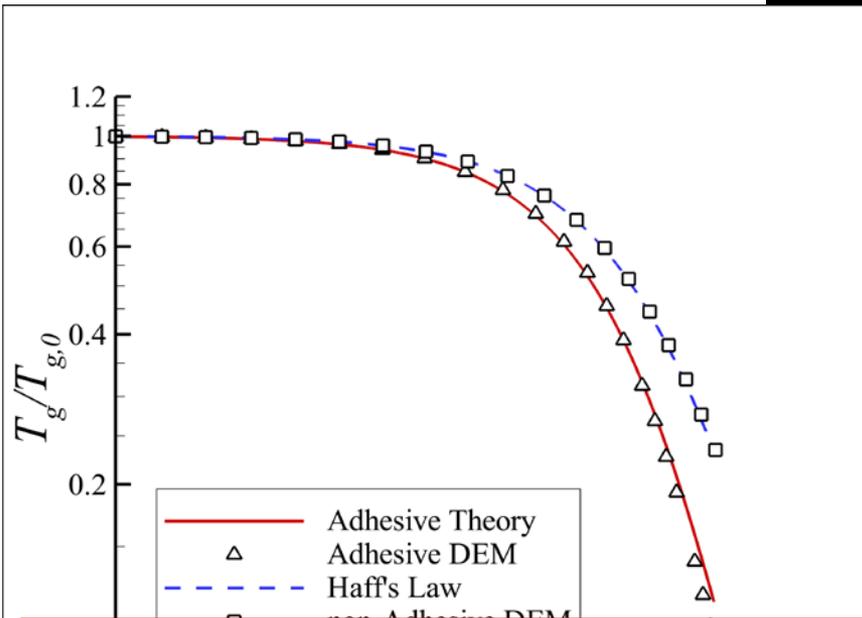
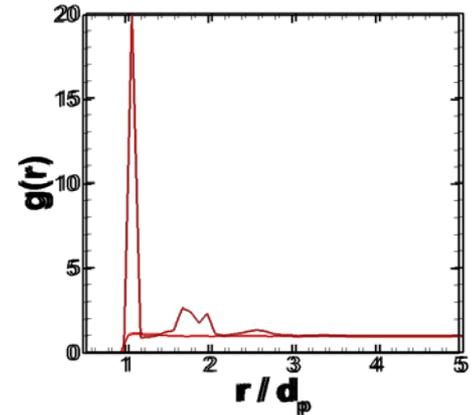
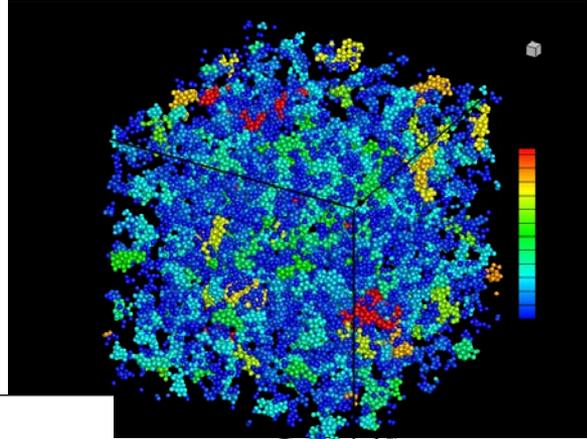


$$\begin{cases} Ha^{-1} \left(\frac{d_0}{d_p} \right)^2 \frac{d\tilde{\mathbf{V}}^{(i)}}{d\tilde{t}} + 1 = 0 \\ \frac{d\tilde{\mathbf{X}}^{(i)}}{d\tilde{t}} = \tilde{\mathbf{V}}^{(i)} \end{cases}$$

$$\begin{cases} \tilde{t} = \frac{t\sqrt{T}}{d_0} \\ \tilde{\mathbf{X}}^{(i)} = \frac{\mathbf{X}^{(i)}}{d_0} \\ \tilde{\mathbf{V}}^{(i)} = \frac{\mathbf{V}^{(i)}}{\sqrt{T}} \\ Ha = \frac{A}{\rho \pi d_p^2 d_0 T} \end{cases}$$

Homogeneous Cooling Cohesive Granular Gas

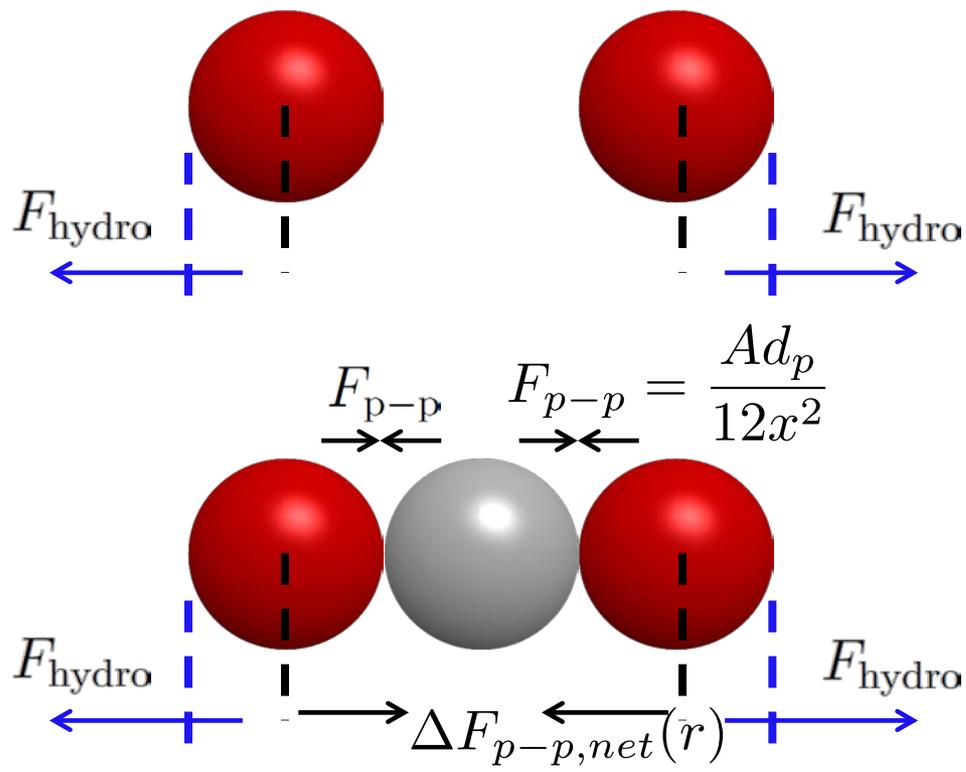
- Pseudo-Liouville Operator Analysis
 - Temperature decay
 - Coordination number
- Soft-sphere DEM of cohesive particles



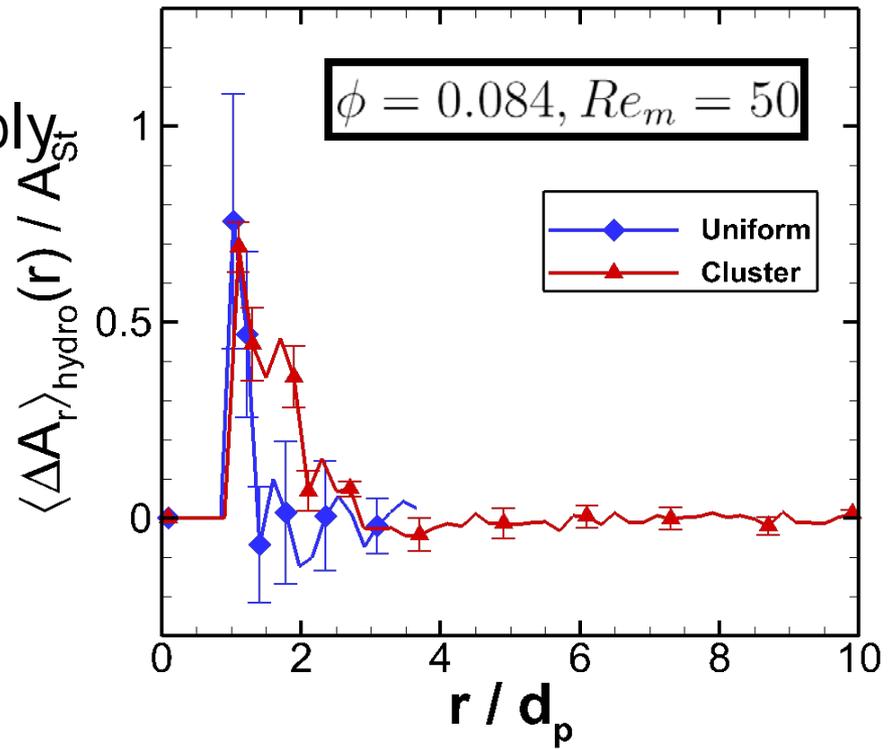
Structure of clusters depends on Ha : the ratio of adhesion energy to particle kinetic energy (granular temperature)

Cohesive Suspensions: Flow Physics

- Compare hydrodynamic forces between a pair of particles in uniform and clustered arrangements in a fixed assembly



Relative radial acceleration



Particles remain as aggregates if the net cohesive forces overcome the hydrodynamic forces at separation r

Difference between uniform and clustered hydrodynamic relative acceleration (force) must be overcome by net cohesive force

Cohesive Suspensions: Flow Physics

Mean flow can modify and re-orient structure

Mean flow hydrodynamics

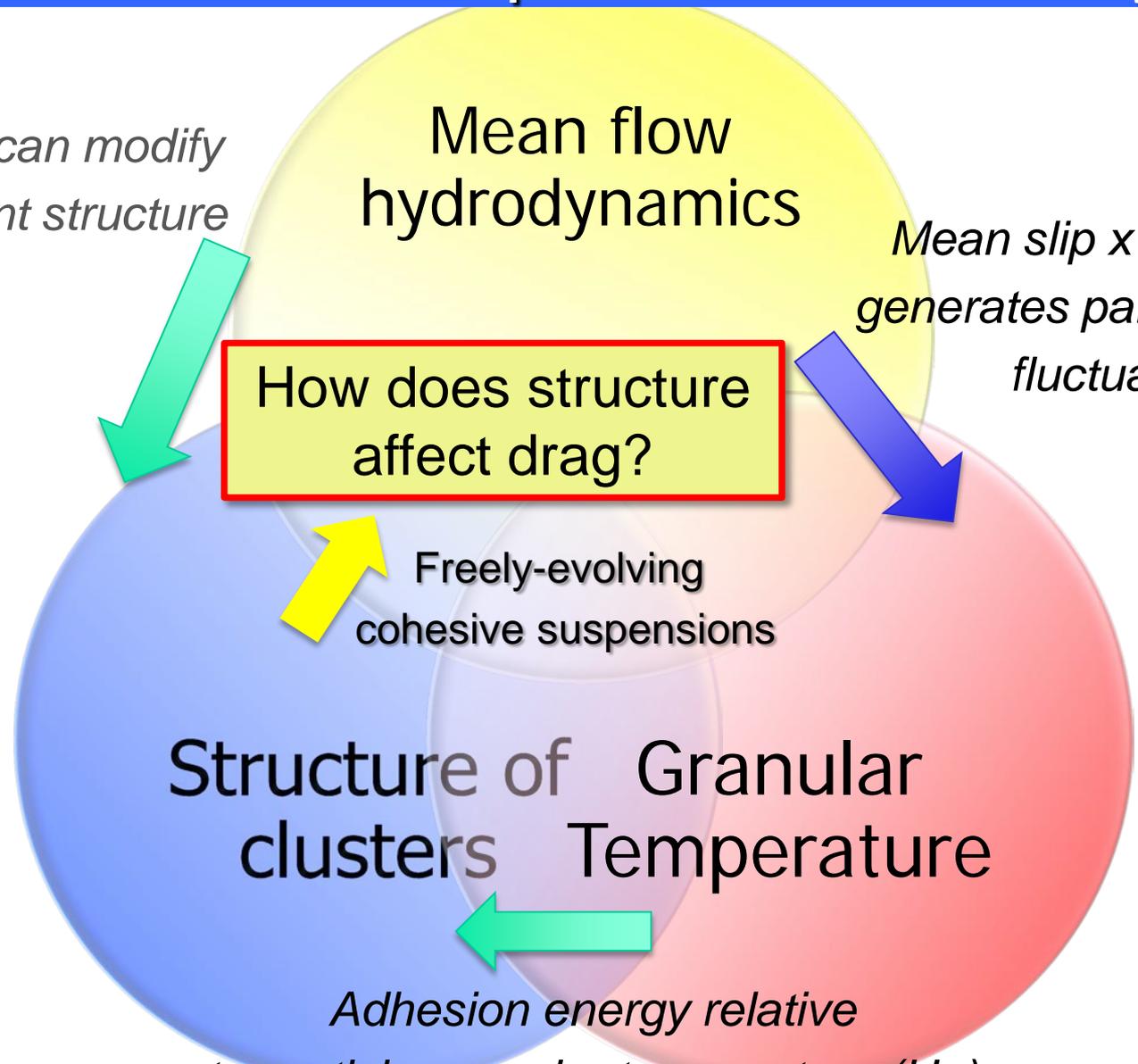
Mean slip x mean drag generates particle velocity fluctuations

How does structure affect drag?

Freely-evolving cohesive suspensions

Structure of Granular clusters Temperature

Adhesion energy relative to particle granular temperature (Ha) determines structure



PR-DNS of Clustered Gas-Solid Systems

- *Type I*: PR-DNS of homogeneous freely evolving gas-solid suspensions of cohesive particles
 - Computationally very expensive owing to range of time and length scales
- *Type II*: PR-DNS of homogeneous freely evolving clustered gas-solid flow (eliminates cluster formation time)
 - A. With cohesive forces allowing rearrangement: study restructuring of clusters in flow
 - B. Rigid clusters: study re-orientation of clusters in flow
- *Type III*: PR-DNS of homogeneous fixed assemblies of clustered particles

Generation of Particle Clusters

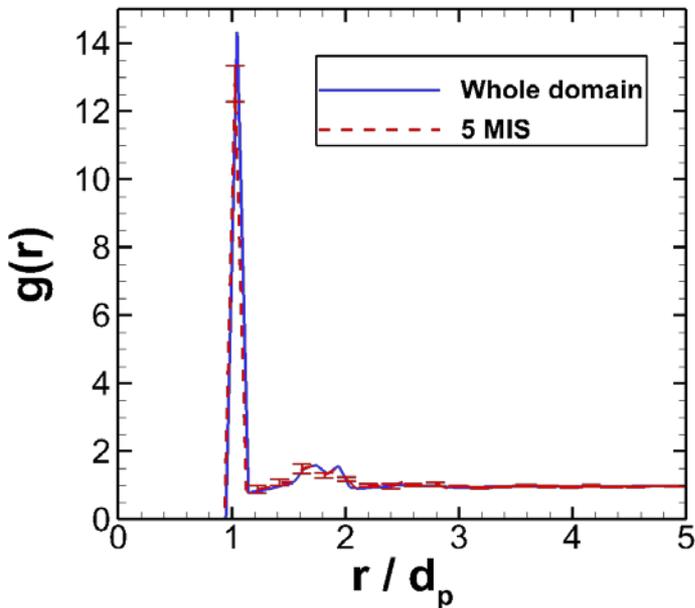
❑ Selection of particle sub-ensembles

➤ Cocco et al. (2010) *Powder Tech.*

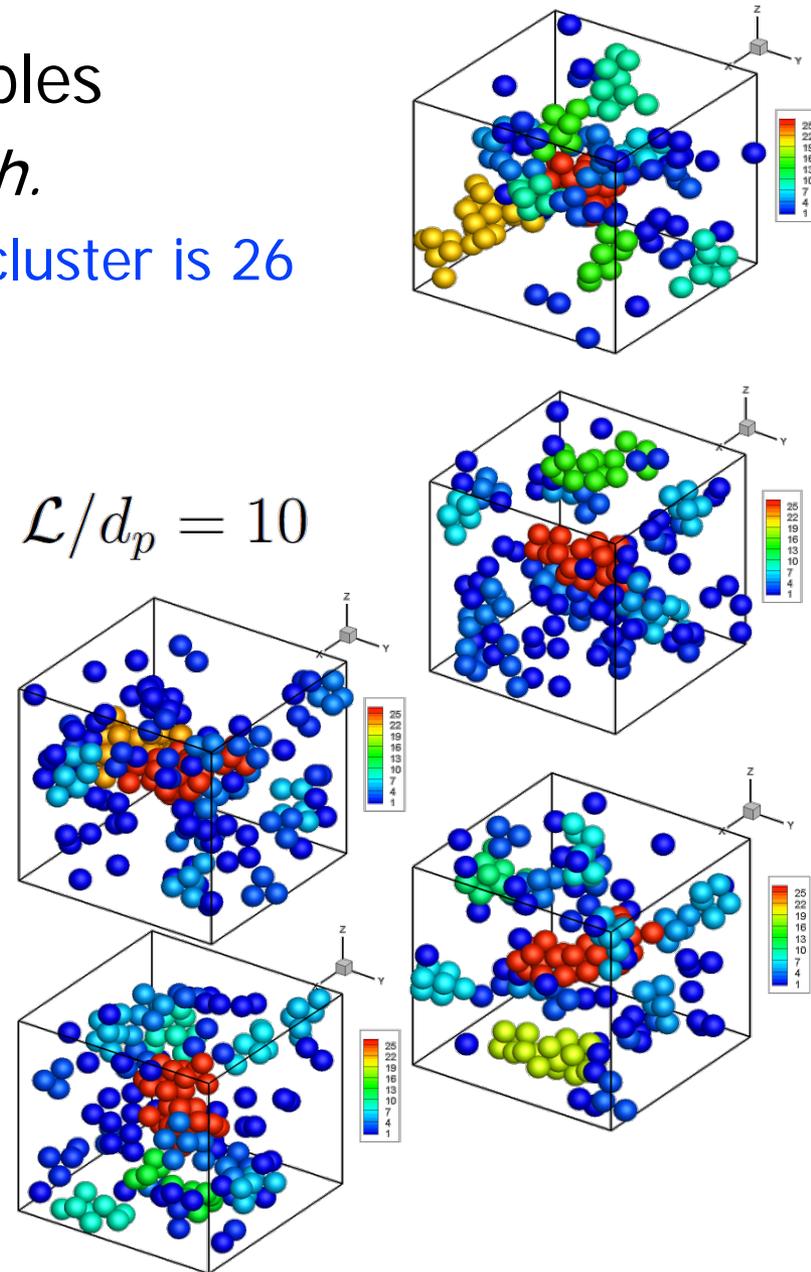
- ✓ Mean number of particles in a cluster is 26
- ✓ 75% of particles in clusters
- ✓ 25% of particles as single

❑ Choosing 5 sub-ensembles with $\mathcal{L}/d_p = 10$

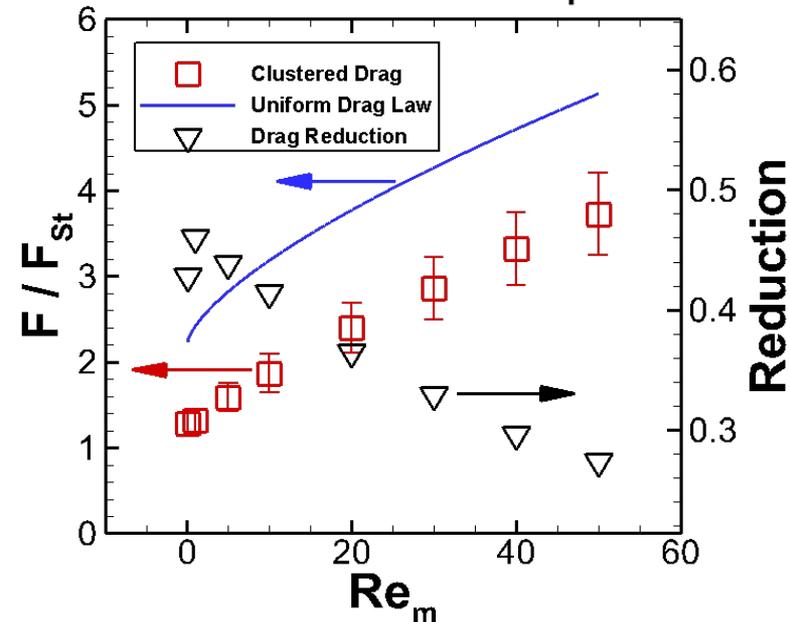
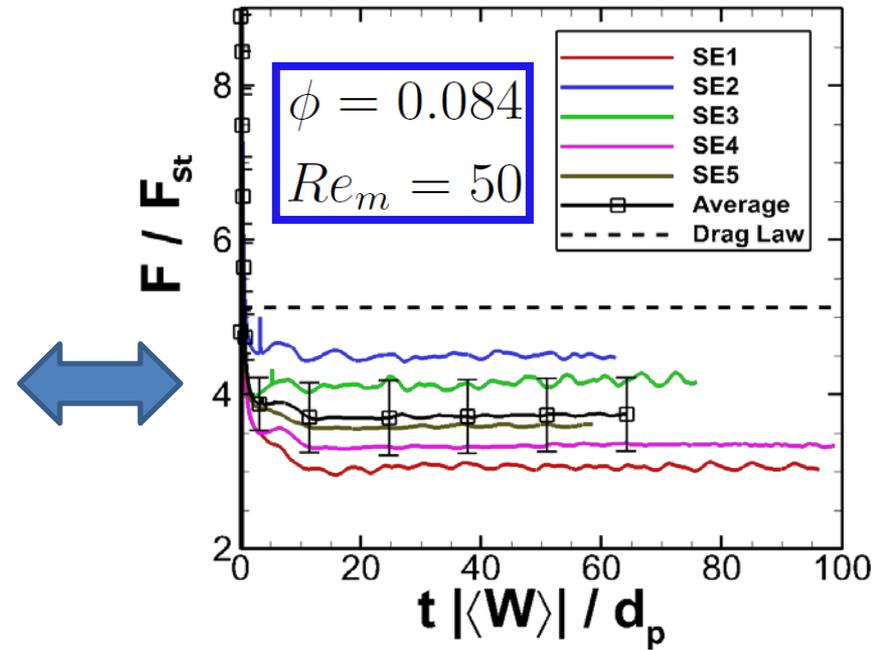
➤ Consistent ϕ , $g(r)$



Sub-ensembles represent statistical properties of the whole domain



Direct Numerical Simulation



- Drag reduction is observed in clustered configurations
- Maximum reduction occurs at lower Re_m
- Higher volume fraction simulations are in progress

Cluster Drag: Dependencies

- Solid-phase volume fraction and mean-slip Reynolds number

✓ Similar to uniform particle configuration drag law

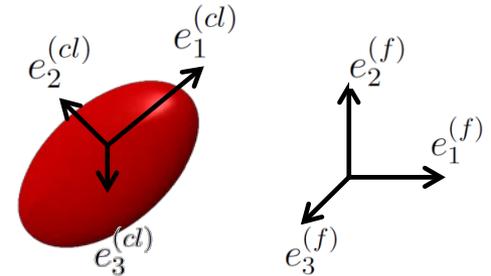
$$\phi, Re_m$$

- Cluster size R_g

- Anisotropy in clusters $\mathbf{e}^{(f)} \otimes \mathbf{e}^{(cl)}$

✓ Alignment of cluster principal

axis and mean flow unit vector



- The ratio of frontal area to the wetted area of a cluster

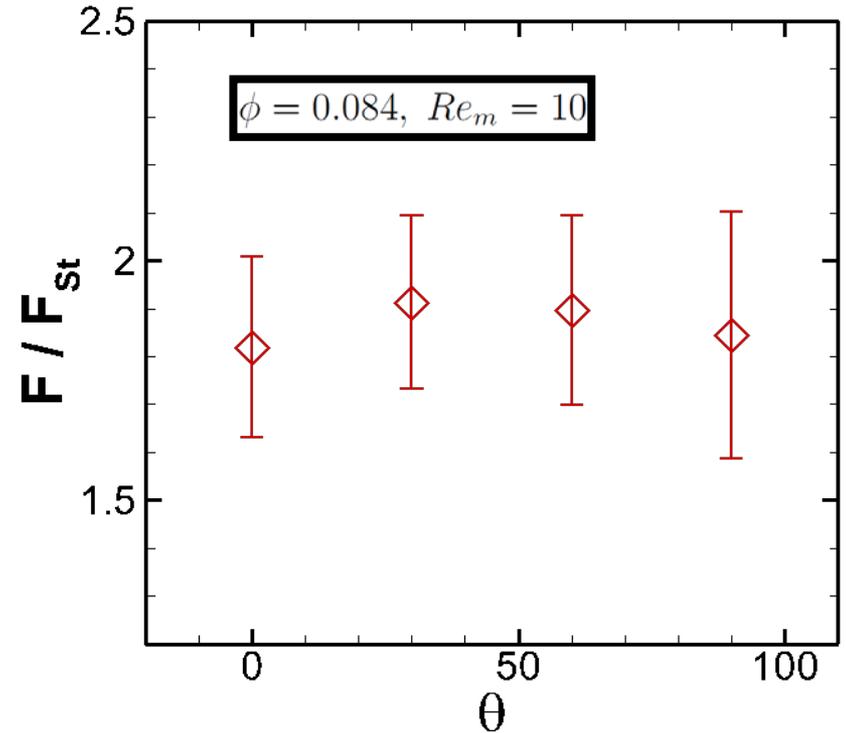
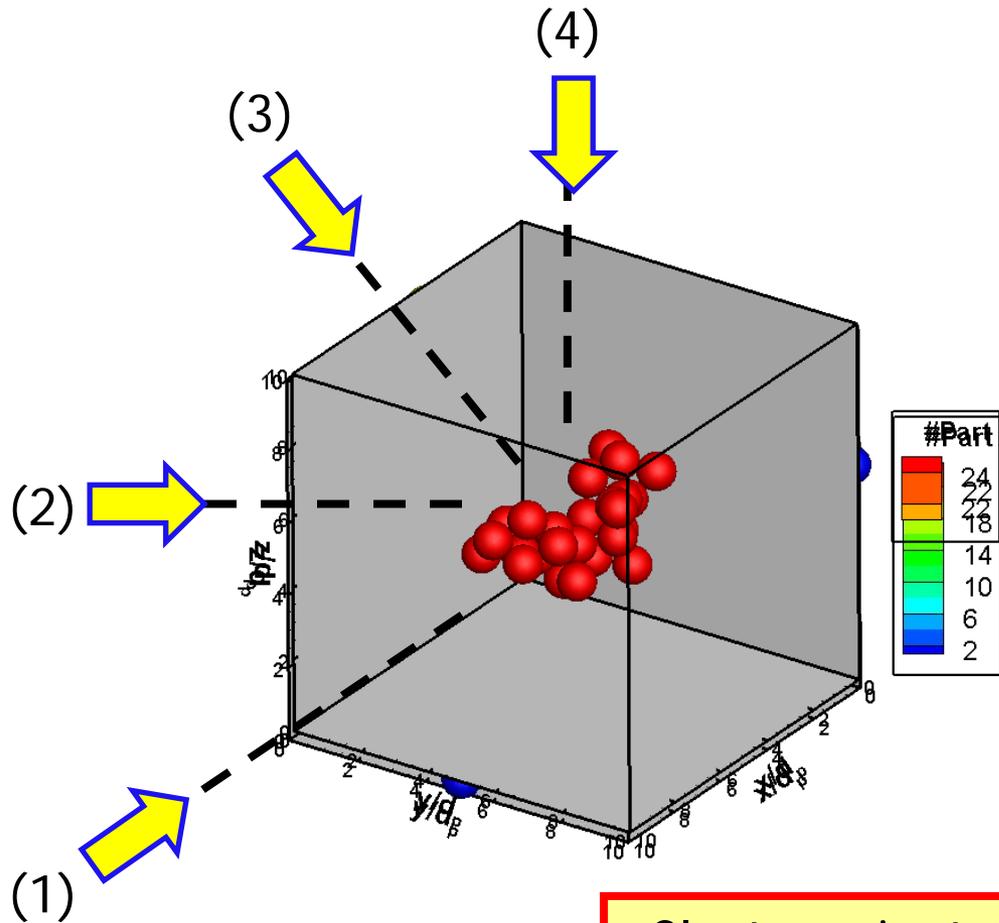
$$\frac{A_{\text{frontal}}}{A_{\text{wetted}}}$$

- Tentative proposal for cluster drag law

$$F_{cl} = f \left(\frac{\langle \Delta A_r \rangle_{\text{hydro}}}{A_{p-p}}, \phi, Re_m, \frac{R_g}{d_p}, \mathbf{e}^{(f)} \otimes \mathbf{e}^{(cl)}, \frac{A_{\text{frontal}}}{A_{\text{wetted}}} \right)$$

Analysis of Drag Force

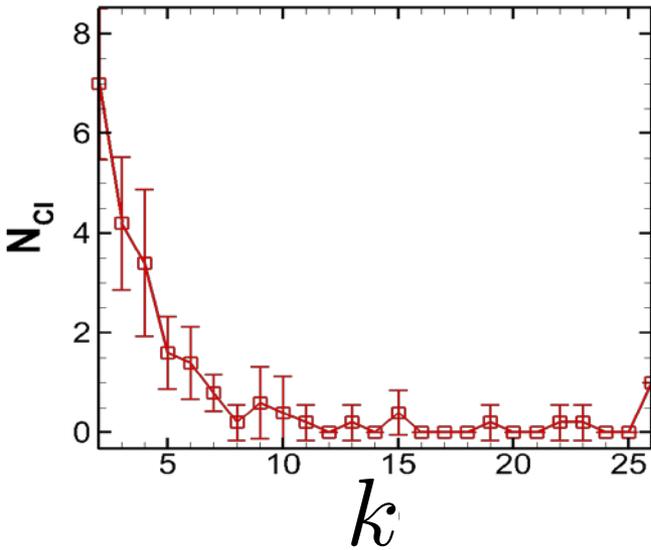
□ Cluster alignment to the mean flow



• Cluster orientation does not affect the total drag force significantly

Analysis of Drag Force

□ Distribution of drag in clusters in simulated cases



$$P(N_p = k) \quad F_{\text{Equi.}} = F_{\text{Uni.}}(\tilde{Re}_m, \tilde{\phi})$$

Cluster size distribution

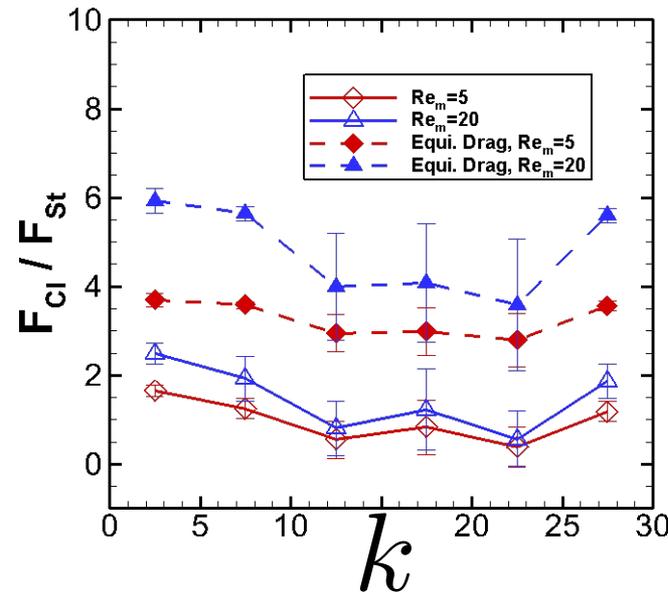
$$\tilde{d}_p = d_p N_p^{1/3} \quad \tilde{\phi} = \phi$$

$$\tilde{Re}_m = Re_m \frac{\tilde{d}_p}{d_p}$$

$$\langle F_{Cl} \rangle = \sum_k \langle F_{Cl} | N_p = k \rangle P(N_p = k)$$

$$\langle F_{Cl} | N_p = k \rangle = C(\dots) F_{\text{Uni.}}(\tilde{Re}_m, \tilde{\phi})$$

Porosity parameter



- $F_{\text{equi.}}$ is proportional to the cluster drag by a porosity parameter
- Can the total drag can be computed by knowing the porosity parameter and cluster size distribution? Preliminary results are promising!

Summary

□ Conclusion

- Flow physics in clustering particle suspensions: interplay of
 - ✓ Granular temperature arising from mean flow hydrodynamics
 - ✓ Ratio of adhesive energy to particle granular temperature: affects structure of clusters
 - ✓ Particle clusters affect mean drag and mean flow hydrodynamics
- Drag reduction is observed in gas-solid flows with clusters compared to uniform particle configurations (fixed assemblies)

□ Future work

- Gain better physical understanding of cohesive suspensions using PR-DNS (provide agg./breakage kernels for kinetic/PBE)
- Compare cluster statistics with experimental results; tune parameters as necessary to reproduce
- Develop a physics-based drag law for particle clusters based on PR-DNS results