

# Numerical simulation of polydisperse gas-particle flow in a vertical riser using a size-velocity quadrature-based moment method

Bo Kong<sup>1,2</sup> and Rodney O. Fox<sup>1,2</sup>

<sup>1</sup>Department of Chemical and Biological Engineering  
Iowa State University, Ames, IA, USA

<sup>2</sup>Ames Laboratory-DOE, Ames, IA, USA

NETL 2014 Workshop on Multiphase Flow Science

## Tasks accomplished in FY14:

### *Quadrature-based moment method (QBMM)*

- Advanced library to manage moments in CFD context, based on Hash-Table method
- Comprehensive moment inversion library (univariate/multivariate), including QMOM, EQMOM, TP, CQMOM, ECQMOM
- New explicit disperse-phase volume fraction limit scheme used in general QBMM
- New high-order moment kinetic flux algorithm to improve accuracy of continuous QBMM (EQMOM)

### *Polydisperse gas-particle flow*

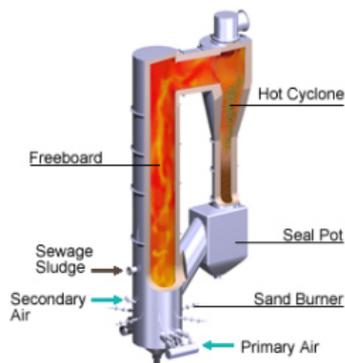
- Variable-particle-size model with size-conditioned particle velocity, based on EQMOM
- Polydisperse particle collision model, including granular pressure term

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  - Moment inversion
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# Motivation

Polydisperse multiphase flows: continuous phase and **disperse phase**

*Fluidized Bed*



*Bubble column*



*Fuel Injection*



In many commonly encountered applications

- polydispersity (e.g., size, density, shape) is present
- “size” and velocity of disperse phase are closely coupled

Thus, to accurately model polydisperse multiphase flows, joint number density function of “size” and velocity has to be properly described

# Existing models for polydisperse bubbly flows

## *Euler-Lagrange Models*

- Discrete Element Method (DEM)

*Limitation: Computationally expensive for industrial applications*

## *Euler-Euler Models*

- Population Balance Equation (PBE) carried by fluid velocity

*Limitation: Spatial fluxes do not depend on size*

- Class method with separate class velocities

*Limitation: Computationally expensive for continuous size distribution*

- Direct Quadrature Method of Moments (DQMOM) with a multi-fluid model

*Limitation: Weights and abscissas are not conserved quantities*

## Objective

Develop a robust and accurate moment-based polydisperse flow solver that incorporates microscale physics with reasonable computation cost

# Governing equations for polydisperse gas-particle flow

## Gas phase: Continuity and momentum transport equations

$$\frac{\partial}{\partial t} \rho_g \varepsilon_g + \nabla \cdot \rho_g \varepsilon_g \mathbf{U}_g = 0$$

$$\frac{\partial}{\partial t} \rho_g \varepsilon_g \mathbf{U}_g + \nabla \cdot \rho_g \varepsilon_g \mathbf{U}_g \otimes \mathbf{U}_g = \nabla \cdot \varepsilon_g \boldsymbol{\tau}_g - \nabla p + \rho_g \varepsilon_g \mathbf{g} + \mathbf{M}_{lb}$$

## Particle phase: Kinetic equation for joint size-velocity NDF $f(\xi, \mathbf{v})$

$$\frac{\partial f}{\partial t} + \mathbf{v} \cdot \frac{\partial f}{\partial \mathbf{x}} + \frac{\partial}{\partial \mathbf{v}} \cdot f \mathbf{A} = \mathbb{S}$$

where  $\mathbf{A}$  represents acceleration due to forces acting on each particle,  $\mathbb{S}$  represents other possible source terms (e.g., collisions, aggregation, break up, and chemical reaction in particles)

# Moments method for solving Kinetic Equation

## Moments for joint size-velocity NDF

$$m_{p,i,j,k} = \int \xi^p v_x^i v_y^j v_z^k f(\xi, \mathbf{v}) d\xi d\mathbf{v}$$

Lower-order moments have particular physical significance:

$$m_{1,0,0,0} = \rho_p \varepsilon_p, \quad m_{1,1,0,0} = \rho_p \varepsilon_p U_{bx}, \quad m_{1,0,1,0} = \rho_p \varepsilon_p U_{by}, \quad m_{1,0,0,1} = \rho_p \varepsilon_p U_{bz}$$

## Moments transport equation:

$$\frac{\partial m_{p,i,j,k}}{\partial t} + \frac{\partial m_{p,i+1,j,k}}{\partial x} + \frac{\partial m_{p,i,j+1,k}}{\partial y} + \frac{\partial m_{p,i,j,k+1}}{\partial z} = F_{p,i,j,k}$$

$$F_{p,i,j,k} = \int \xi^p v_x^i v_y^j v_z^k [i v_x^{-1} (A_x) + j v_y^{-1} (A_y) + k v_z^{-1} (A_z)] f(\xi, \mathbf{v}) d\xi d\mathbf{v}$$

Quadrature-Based Moment Methods (QBMM) are introduced to attain closure of higher-order moments (spatial fluxes) and  $F_{p,i,j,k}$

# Representation of joint size-velocity NDF

## Joint size-velocity NDF

$$n(\xi, \mathbf{v}) = f(\xi) g(\mathbf{v}|\xi)$$

## Comparison with traditional particle size population transport method

Kinetic equation for particle size number density (with  $\mathbb{S} = 0$ ) can be rewritten

$$\frac{\partial n}{\partial t} + \nabla \cdot \mathbf{U}n = 0$$

$$\frac{\partial n\mathbf{U}}{\partial t} + \nabla \cdot \mathbf{U} \otimes \mathbf{U}n = n\mathbf{g} + \mathbf{A}(\mathbf{U})n$$

$\mathbf{U}$  is often assumed to be independent of size  $\xi$ , however, a model with a continuous particle velocity conditioned on size  $\mathbf{U}(\xi)$  needed for polydisperse particles

## Reconstructed size NDF

$$n(\xi) = \sum_{\alpha=1}^N w_{\alpha} \delta_{\sigma}(\xi, \xi_{\alpha})$$

with parameters found from size moments:

- **Gamma** ( $0 < \xi < \infty$ )

$$\delta_{\sigma}(\xi, \xi_{\alpha}) \equiv \frac{\xi^{\lambda_{\alpha}-1} e^{-\xi/\sigma}}{\Gamma(\lambda_{\alpha}) \sigma^{\lambda_{\alpha}}}$$

with  $\lambda_{\alpha} = \xi_{\alpha}/\sigma$

- **Beta** ( $0 < \xi < 1$ )

$$\delta_{\sigma}(\xi, \xi_{\alpha}) \equiv \frac{\xi^{\lambda_{\alpha}-1} (1-\xi)^{\mu_{\alpha}-1}}{B(\lambda_{\alpha}, \mu_{\alpha})}$$

with  $\lambda_{\alpha} = \xi_{\alpha}/\sigma$  and  $\mu_{\alpha} = (1 - \xi_{\alpha})/\sigma$

First  $2N$  moments always exact

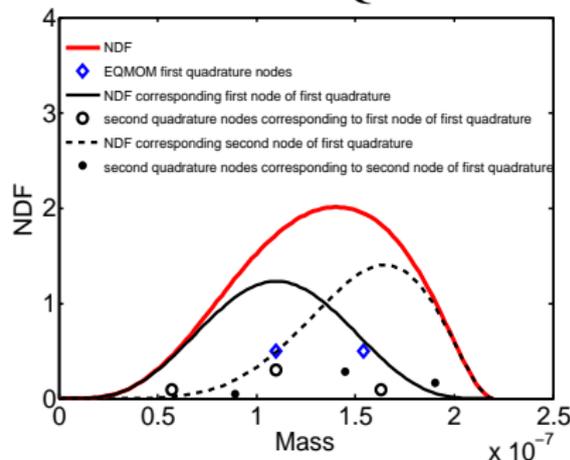
Converges to exact NDF as  $N \rightarrow \infty$

## Dual-quadrature form

$$\delta_{\sigma}(\xi, \xi_{\alpha}) \approx \sum_{\beta=1}^M w_{\alpha\beta} \delta(\xi - \xi_{\alpha\beta})$$

with known weights  $w_{\alpha\beta}$  and abscissas  $\xi_{\alpha\beta}$

## 2-node beta-EQMOM



# Size-conditioned particle velocity distribution $g(\mathbf{v}|\xi)$

**Monokinetic:** *PTC effect and Brownian fluctuation are both negligible*

$$n(\xi, \mathbf{u}) = \sum_{\alpha=1}^{N_s} \rho_{\alpha} K(\xi; \xi_{\alpha}, \sigma_s) \delta(\mathbf{u} - \mathbf{U}(\xi))$$

$\mathbf{U}(\xi)$  is size-conditioned particle mean velocity

**Anisotropic Gaussian:** *PTC small but Brownian fluctuation non-negligible*

$$n(\xi, \mathbf{u}) = \sum_{\alpha=1}^{N_s} \rho_{\alpha} K(\xi; \xi_{\alpha}, \sigma_s) g(\mathbf{u} - \mathbf{U}(\xi); \sigma^2(\xi) \underline{\mathbf{R}})$$

$\sigma^2(\xi)$  is size-conditioned granular temperature,  $\underline{\mathbf{R}}$  is normalized velocity covariance tensor

**ECQMOM method:** *PTC significant and Brownian fluctuation non-negligible*

$$n(\xi, u, v, w) = \sum_{\alpha=1}^{N_s} \rho_{\alpha} K(\xi; \xi_{\alpha}, \sigma_s) \left\{ \sum_{\beta=1}^{N_1} \rho_{\alpha\beta} g(u - U(\xi); u_{\alpha\beta}, \sigma_{1\alpha}) \left[ \sum_{\gamma=1}^{N_2} \rho_{\alpha\beta\gamma} g(v - V(\xi, u); v_{\alpha\beta\gamma}, \sigma_{2\alpha\beta}) \left( \sum_{\kappa=1}^{N_3} \rho_{\alpha\beta\gamma\kappa} g(w - W(\xi, u, v); w_{\alpha\beta\gamma\kappa}, \sigma_{3\alpha\beta\gamma}) \right) \right] \right\}$$

# Solving size-conditioned velocity

## Anisotropic Gaussian velocity distribution

$$g(\mathbf{u} - \mu(\xi), \sigma^2(\xi)\underline{\mathbf{R}}) = \frac{1}{(2\pi)^{3/2} \sqrt{|\sigma^2(\xi)\underline{\mathbf{R}}|}} \exp \left[ -\frac{1}{2\sigma^2(\xi)} (\mathbf{u} - \mathbf{U}(\xi))^T \underline{\mathbf{R}}^{-1} (\mathbf{u} - \mathbf{U}(\xi)) \right]$$

## Approximation method

$\mathbf{U}(\xi)$  and  $\sigma^2(\xi)$  can be approximated as

$$\mathbf{U}(\xi) = \sum_{n=0}^{2N_s} \mathbf{u}_n g_n(\xi) \quad \sigma^2(\xi) = \sum_{n=0}^{2N_s} \sigma_n g_n(\xi)$$

where  $\mathbf{u}_n(\xi)$  and  $\sigma_n$  are constant coefficients, and  $g_n(\xi)$  are basis functions, which can be defined using various kinds of **orthogonal polynomial functions** and **piecewise functions**

## Conditional mean velocity

Vector function  $\mathbf{U}(\xi)$  is defined to have following properties, which can be used to solve for  $\mathbf{u}_n(\xi)$

$$\sum_{\alpha=1}^{N_s} \rho_{\alpha} \int_{\Omega} \xi^s \mathbf{U}(\xi) K(\xi; \xi_{\alpha}, \sigma_s) d\xi = \begin{bmatrix} M_{s,1,0,0} \\ M_{s,0,1,0} \\ M_{s,0,0,1} \end{bmatrix} \quad M_{s,i,j,k} = \int_{\Omega} \int_{\mathbb{R}^3} \xi^s u^i v^j w^k n(\xi, \mathbf{u}) d\xi d\mathbf{u}$$

for  $s = 0, \dots, d_s$  with  $d_s \leq 2N_s$

# Solving size-conditioned velocity

## Conditional granular temperature

Similarly, the conditional granular temperature  $\sigma^2(\xi)$  has the following properties, which is used to solve for  $\sigma_n$ :

$$\sum_{\alpha=1}^{N_s} \rho_{\alpha} \int_{\Omega} \xi^s \left( \mathbf{U}(\xi) \cdot \mathbf{U}(\xi) + 3\sigma^2(\xi) \right) K(\xi; \xi_{\alpha}, \sigma_s) d\xi = M_{s,2,0,0} + M_{s,0,2,0} + M_{s,0,0,2}$$

for  $s = 0, \dots, d_s$  with  $d_s \leq 2N_s$

## Normalized velocity covariance tensor

Finally, normalized velocity covariance tensor (**size-independent**) is found using its definition:

$$\sum_{\alpha=1}^{N_s} \rho_{\alpha} \int_{\Omega} \xi^s \left[ \mathbf{U}(\xi) \otimes \mathbf{U}(\xi) + \sigma^2(\xi) \underline{\mathbf{R}} \right] K(\xi; \xi_{\alpha}, \sigma_s) d\xi = \begin{bmatrix} M_{s,2,0,0} & M_{s,1,1,0} & M_{s,1,0,1} \\ M_{s,1,1,0} & M_{s,0,2,0} & M_{s,0,1,1} \\ M_{s,1,0,1} & M_{s,0,1,1} & M_{s,0,0,2} \end{bmatrix}$$

# Sample size and sample velocity

*Sample size: Jacobi quadrature for Beta kernel function*

$$K(\xi; \xi_\alpha, \sigma_s) = \sum_{\beta=1}^{N_{jq}} \tilde{\rho}_{\alpha\beta} \delta(\xi, \tilde{\xi}_{\alpha,\beta})$$

*Sample velocity: 3-D Hermite quadrature for anisotropic Gaussian kernel function*

$$g(\mathbf{u} - \mathbf{U}(\xi), \sigma^2(\xi)\underline{\mathbf{R}}) = \sum_{\gamma=1}^{N_{hq}} \tilde{\rho}_\gamma \delta(\mathbf{u}, \tilde{\mathbf{u}}_\gamma) = \sum_{\gamma=1}^{N_{hq}} \tilde{\rho}_\gamma \delta\left(\mathbf{u}, \begin{bmatrix} \tilde{u}_\gamma \\ \tilde{v}_\gamma \\ \tilde{w}_\gamma \end{bmatrix}\right)$$

Using spectral decomposition scheme with triple 1-D Hermite quadratures

*Moments calculation using sample size and velocity*

Now moments can be calculated as

$$\begin{aligned} M_{s,i,j,k} &= \sum_{\alpha=1}^{N_s} \rho_\alpha \xi_\alpha^s u^i v^j w^k K(\xi; \xi_\alpha, \sigma_s) g(\mathbf{u} - \mathbf{U}(\xi), \sigma^2(\xi)\underline{\mathbf{R}}) \\ &= \sum_{\alpha=1}^{N_s} \rho_\alpha \sum_{\beta=1}^{N_{jq}} \tilde{\rho}_{\alpha\beta} \tilde{\xi}_{\alpha\beta}^s \sum_{\gamma=1}^{N_{hq}} \tilde{\rho}_{\alpha\beta\gamma} \tilde{u}_{\alpha\beta\gamma}^i \tilde{v}_{\alpha\beta\gamma}^j \tilde{w}_{\alpha\beta\gamma}^k \end{aligned}$$

# Kinetics-based finite-volume method: spatial fluxes

Spatial moment fluxes are decomposed into two contributions corresponding to positive and negative velocity in each spatial direction:

$$F_{s,i,j,k}^x = Q_{s,i,j,k}^{x,+} + Q_{s,i,j,k}^{x,-}$$

$$\begin{aligned} Q_{s,i,j,k}^{x,+} &= \int_{\mathbb{R}} \left( \int_0^{\infty} \xi^i u^{i+1} v^j w^k f_{sv}(\xi, \mathbf{u}) du \right) d\xi \\ &= \sum_{\alpha=1}^{N_s} \sum_{\beta=1}^{N_{jq}} \sum_{\gamma=1}^{N_{hq}} \max(\tilde{u}_{\alpha\beta\gamma}, 0) \rho_{\alpha} \tilde{\rho}_{\alpha\beta} \tilde{\rho}_{\alpha\beta\gamma} \tilde{\xi}_{\alpha\beta}^s \tilde{u}_{\alpha\beta\gamma}^i \tilde{v}_{\alpha\beta\gamma}^j \tilde{w}_{\alpha\beta\gamma}^k \end{aligned}$$

$$\begin{aligned} Q_{s,i,j,k}^{x,-} &= \int_{\mathbb{R}} \left( \int_{-\infty}^0 \xi^i u^{i+1} v^j w^k f_{sv}(\xi, \mathbf{u}) du \right) d\xi \\ &= \sum_{\alpha=1}^{N_s} \sum_{\beta=1}^{N_{jq}} \sum_{\gamma=1}^{N_{hq}} \min(\tilde{u}_{\alpha\beta\gamma}, 0) \rho_{\alpha} \tilde{\rho}_{\alpha\beta} \tilde{\rho}_{\alpha\beta\gamma} \tilde{\xi}_{\alpha\beta}^s \tilde{u}_{\alpha\beta\gamma}^i \tilde{v}_{\alpha\beta\gamma}^j \tilde{w}_{\alpha\beta\gamma}^k \end{aligned}$$

**Realizability condition:**

$$\Delta t = CFL \min_{\alpha\beta\gamma} \left( \frac{\Delta x}{|\tilde{u}_{\alpha\beta\gamma}|}, \frac{\Delta y}{|\tilde{v}_{\alpha\beta\gamma}|}, \frac{\Delta z}{|\tilde{w}_{\alpha\beta\gamma}|} \right)$$

## Forces: drag and gravity

Contributions to evolution of moments due to drag force acting on each particle are directly computed, operating on **sample velocities**  $\tilde{\mathbf{u}}$  from quadrature approximation by solving an ODE:

$$\frac{d\tilde{\mathbf{u}}}{dt} = \mathbf{A}_d + \mathbf{g} = K_D (\mathbf{u}_g - \tilde{\mathbf{u}}) + \mathbf{g}$$

The sample velocity at next time step is

$$\tilde{\mathbf{u}}^* = \tilde{\mathbf{u}}e^{-K_D\Delta t} + \left(1 - e^{-K_D\Delta t}\right) \left(\mathbf{u}_g + \frac{\mathbf{g}}{K_D}\right)$$

And overall drag force received by entire particle phase is

$$\mathbf{F}_{D,pg} = \sum m_p \cdot A_d = \frac{\rho_p \pi}{6} \sum_{\alpha=1}^{N_s} \sum_{\beta=1}^{N_{jq}} \rho_{\alpha} \tilde{\rho}_{\alpha\beta} \tilde{\xi}_{\alpha\beta}^3 \sum_{\gamma=1}^{N_{hq}} \tilde{\rho}_{\alpha\beta\gamma} K_{D,\alpha\beta\gamma} (\mathbf{u}_g - \tilde{\mathbf{u}}_{\alpha\beta\gamma})$$

So using Newton's first law, drag force received by gas phase is

$$\mathbf{F}_{D,gp} = -\mathbf{F}_{D,pg}$$

# Polydisperse collision model

## Moment transport equation

$$\frac{\partial M_{s,i,j,k}}{\partial t} + \frac{\partial M_{s,i+1,j,k}}{\partial x} + \frac{\partial M_{s,i,j+1,k}}{\partial y} + \frac{\partial M_{s,i,j,k+1}}{\partial z} = \mathbb{A}_{s,i,j,k} + \boxed{C_{s,i,j,k}}$$

Using operator splitting, collision term can be conveniently updated by solving

$$\frac{\partial M_{s,i,j,k}}{\partial t} = \boxed{C_{s,i,j,k}}$$

$$M_{s,i,j,k} = \sum_{\alpha=1}^{N_s} \sum_{\beta=1}^{N_{jq}} \rho_{\alpha} \tilde{\rho}_{\alpha\beta} \tilde{\xi}_{\alpha\beta}^s \sum_{\gamma=1}^{N_{hq}} \tilde{\rho}_{\alpha\beta\gamma} \tilde{u}_{\alpha\beta\gamma}^i \tilde{v}_{\alpha\beta\gamma}^j \tilde{w}_{\alpha\beta\gamma}^k = \sum_{a=1}^{N_t} w_a \xi_a^s G_{ijk}(\xi_a)$$

Since we can assume that size does not change due to collisions, and also that collisions are binary

$$\boxed{C_{s,i,j,k}} = \frac{\partial}{\partial t} \sum_{a=1}^{N_t} w_a \xi_a^s G_{ijk}(\xi_a) = \sum_{a=1}^{N_t} w_a \xi_a^s \frac{\partial G_{ijk}(\xi_a)}{\partial t} = \sum_{a=1}^{N_t} w_a \xi_a^s \sum_{b=1}^{N_t} C_{i,j,k}(\xi_a, \xi_b)$$

$$C_{i,j,k}(\xi_a, \xi_b) = C_{i,j,k}(\xi_a, \xi_b) + \nabla \cdot \mathbf{G}_{i,j,k}(\xi_a, \xi_b)$$

# Collision source term

*BGK model (valid to second order)*

$$C_{ijk}(\xi_a, \xi_b) = \kappa_{ab} (G_{ijk,ab}^* - G_{ijk,a}) = \frac{24g_{0,ab}\alpha_b\chi_{ab}^3\sqrt{\sigma_{ab}^2}}{\sqrt{\pi}d_{ab}} (G_{ijk,ab}^* - G_{ijk,a})$$

Zero-order moments  $C_{i+j+k=0}(\xi_a, \xi_b) = 0$

First-order moments  $C_{i+j+k=1}(\xi_a, \xi_b) = \kappa_{ab} (\mathbf{U}_{ab} - \mathbf{U}_a)$

Second-order moments  $C_{i+j+k=2}(\xi_a, \xi_b) = \kappa_{ab} \left( \mathbf{U}_{ab} \otimes \mathbf{U}_{ab} + \underline{\underline{\Sigma}}_{ab} - \mathbf{U}_a \otimes \mathbf{U}_a - \underline{\underline{\Sigma}}_a \right)$

For equilibrium Gaussian distribution

Mean velocity

$$\mathbf{U}_{ab} = \mathbf{U}_a + \frac{1}{4} (1 + e_{ab}) \mu_{ab} (\mathbf{U}_b - \mathbf{U}_a)$$

Covariance tensor

$$\underline{\underline{\Sigma}}_{ab} = \underline{\underline{\Sigma}}_a + \frac{1}{2} (1 + e_{ab}) \mu_{ab} \left[ \frac{1}{4} (1 + e_{ab}) \mu_{ab} \underline{\underline{\mathbf{S}}}_{ab} - \underline{\underline{\Sigma}}_a \right]$$

where  $\underline{\underline{\mathbf{S}}}_{ab} = 1/2(\underline{\underline{\Sigma}}_a + \underline{\underline{\Sigma}}_b + \sigma_{ab}^2 \mathbf{I})$ ,  $\underline{\underline{\Sigma}}_a = \sigma_a^2 \underline{\underline{\mathbf{R}}}$ ,  $\underline{\underline{\Sigma}}_b = \sigma_b^2 \underline{\underline{\mathbf{R}}}$

# Collisional flux and Granular pressure

## Collisional flux

$m^{\text{th}}$  component of collisional-flux term caused by collisions between particles of size  $\xi_a$  and  $\xi_b$  can be calculated as

$$\mathbf{G}_{m,ijk}(\xi_a, \xi_b) = \mathbf{G}_{m,ijk}^{(0)}(\xi_a, \xi_b) + \cancel{\mathbf{G}_{m,ijk}^{(1)}(\xi_a, \xi_b)}$$
$$\mathbf{G}_{m,ijk}^{(0)}(\xi_a, \xi_b) = \frac{3\chi_{ab}^2 \xi_a g_{0,ab}}{\xi_b} \int_{\mathbb{R}^6} I_{ijk}^{(m)}(\omega_{ab}, \mathbf{v}_a, \mathbf{v}_a - \mathbf{v}_b) f(\mathbf{v}_a) f(\mathbf{v}_b) d\mathbf{v}_a d\mathbf{v}_b$$

This term can be **explicitly** closed by using sample size and sample velocity, which can make system **unstable** in simulations

## Granular pressure

For first-order velocity moments  $M_{s,i+j+k=1}$ , collisional flux can be treated as **part of solid stress tensor**  $\underline{\underline{T}}_s$  in particle-phase momentum equation, which can be decomposed as

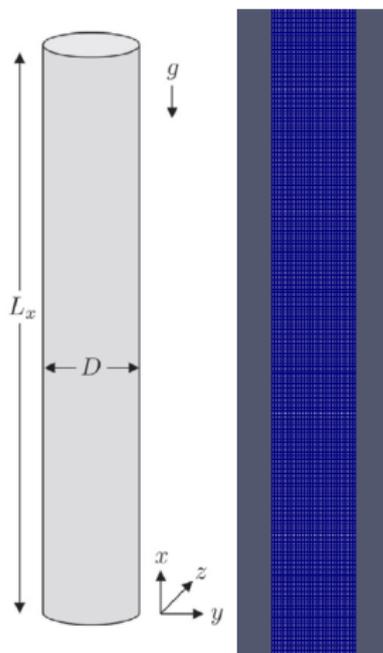
$$\underline{\underline{T}}_{s,k} = p_{s,k} \mathbf{I} + \underline{\underline{\tau}}_{s,k}$$

Granular pressure due to particle collisions for particle phase can be calculated as

$$p_{s,k} = \rho_s \sum_{a=1}^{N_t} w_a \left[ \sigma_a^2 + \sum_{b=1}^{N_t} w_b \frac{\chi_{ab}^3 \mu_{ab} (1 + e_{ab}) g_{0,ab} E_{ab}}{3\chi_{ba}} \right]$$

# Test case: Wall-bounded vertical riser

## Geometry and mesh (2D)

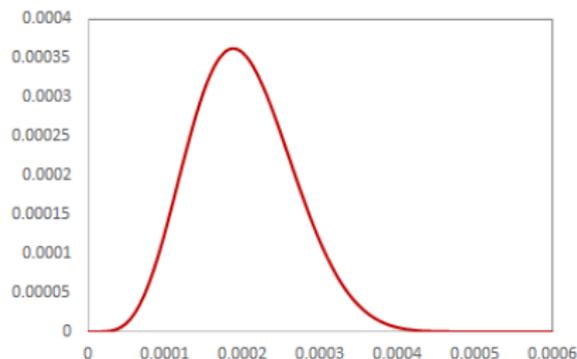


Periodic in X-direction

Gas phase is statistically stationary with zero volume flow rate

gas density ( $\rho_p$ )	1 kg/m <sup>3</sup>
gas viscosity ( $\nu_g$ )	1.84e-5 m <sup>2</sup> /s
particle density ( $\rho_p$ )	2000 kg/m <sup>3</sup>
mean diameter ( $d_p$ )	0.0002 m
restitution coeff (e)	0.9

Initial particle size distribution



## Animation, velocity fields, 2-5 second

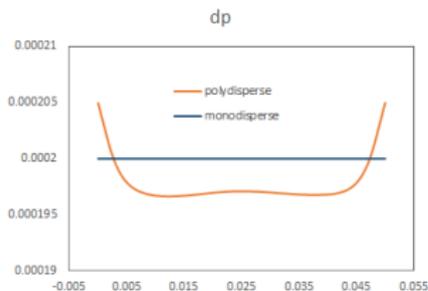
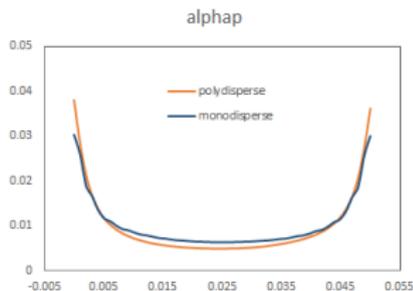
Particle-phase velocity, gas-phase velocity, and granular temperature

## Animation, scalar fields, 2-5 second

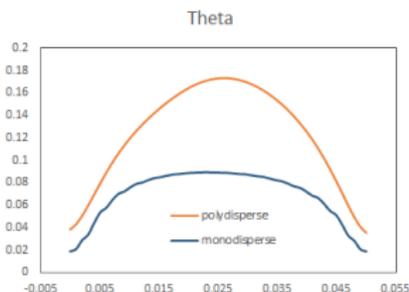
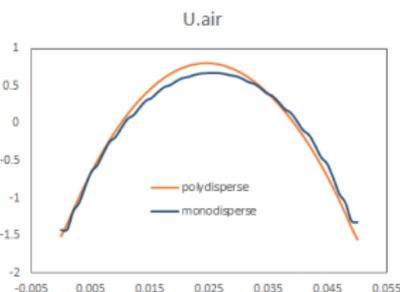
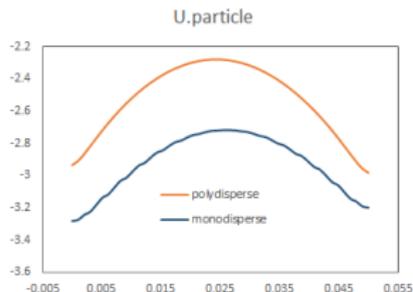
Volume fraction, mean particle diameter, and standard deviation

# Statistical results (time averaged)

## Particle volume fraction and mean diameter



## Particle velocity, gas-phase velocity, and granular temperature



# Summary

## Conclusions

- Novel approach to model polydisperse gas-particle flows with quadrature-based moment methods using kinetic equation for joint size-velocity number density function
- Quasi-2D wall-bounded vertical riser simulated with continuous particle size distribution initial condition
- Solver includes explicit representation of joint NDF using EQMOM that directly incorporates effects of polydispersity
- Size segregation is captured in simulations, and results demonstrate our approach is effective way to model complicated polydisperse gas-particle flows

## Plans for future work in FY15

- Detailed validation with 3-D experimental/Lagrangian simulation data for polydisperse gas-particle flows
- Implementation of new multiphase turbulence model, and validation with Lagrangian simulation of Capecelatro et al.

# Acknowledgment

- Financial support from DOE - National Energy Technology Laboratory (Contract Number: DE-AC02-07CH11358)

Thanks for your attention!

Questions?