



Predicting Transmissivity of a Fracture Under Shearing

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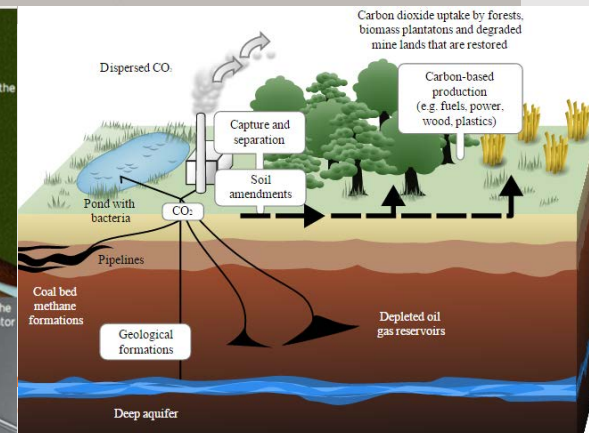
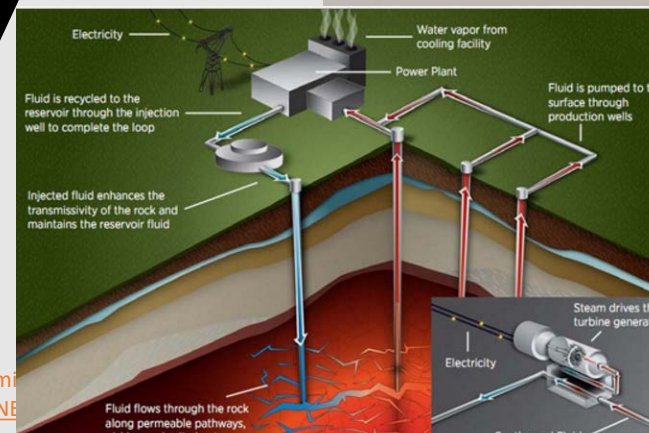
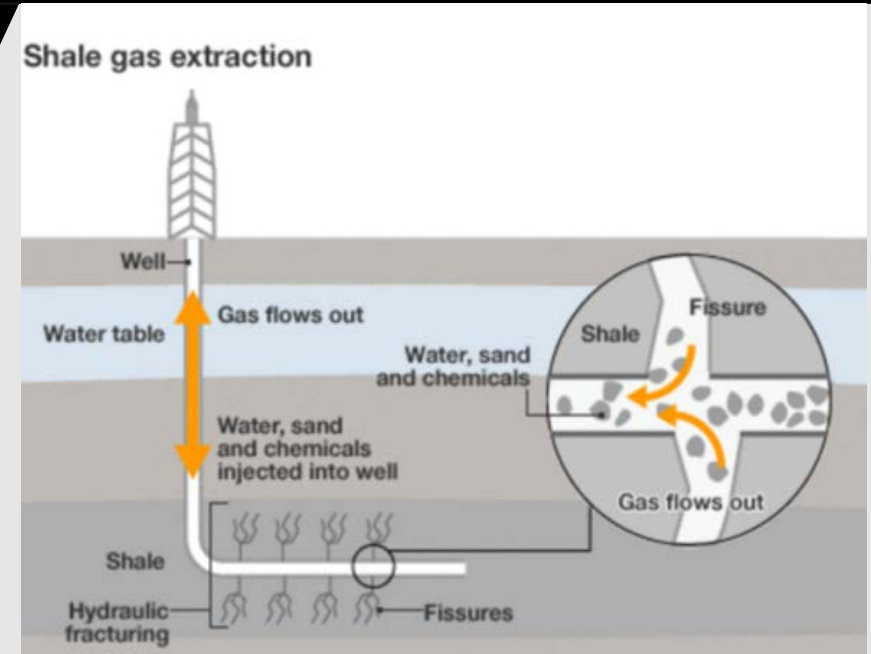
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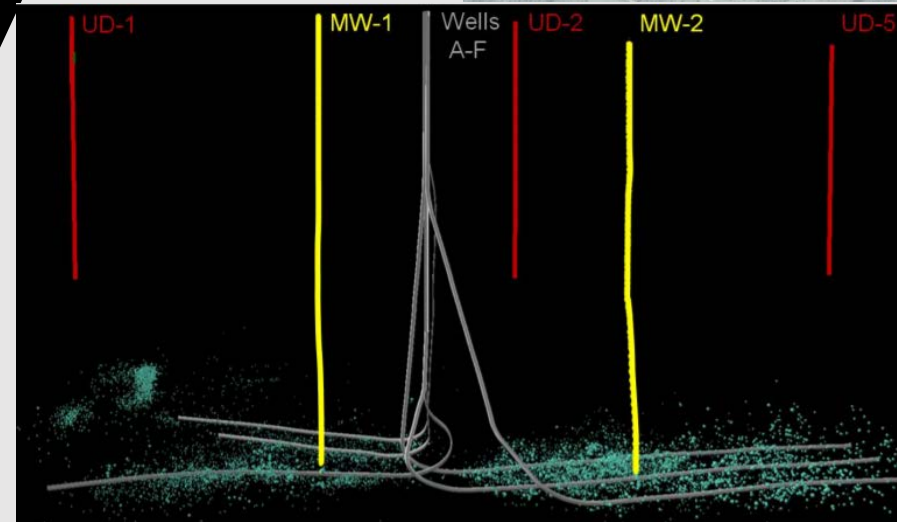
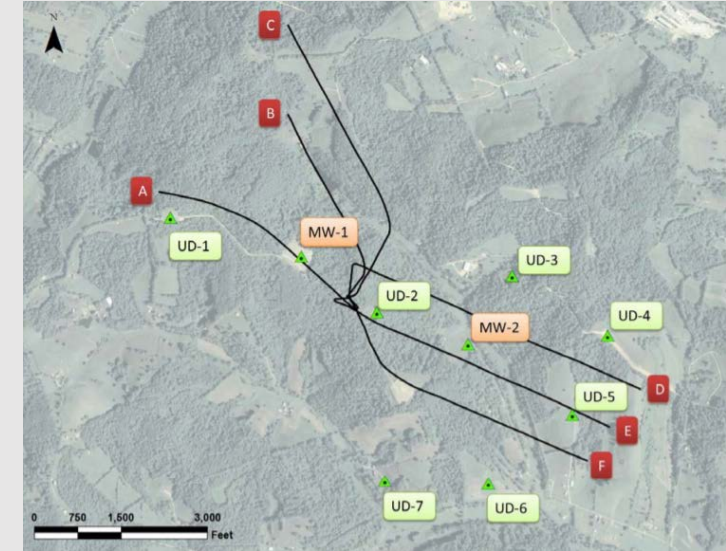
Outline

- Introduction
 - Fractures
 - Shearing
- Experimental Tests Rock Fractures at NETL in Morgantown
 - Preparing the sample
 - Mechanical shearing
 - Computed tomography (CT) scan
 - Permeability measurement
- Numerical Models
 - Full Navier-Stokes simulations
 - Modified Local Cubic Law (MLCL) method
 - Improved Cubic Law
- Results and Conclusions

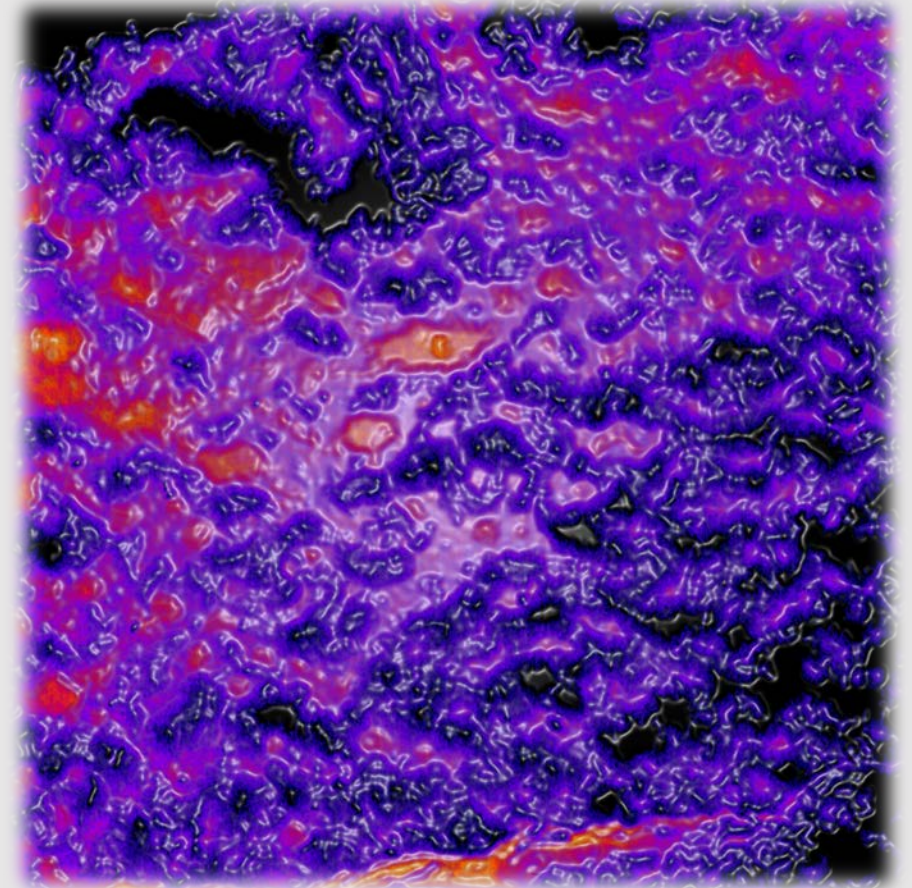
- Fractures are conduits in subsurface rocks
- Unconventional oil and gas resources
- Carbon sequestration reservoir
- Enhanced geothermal system



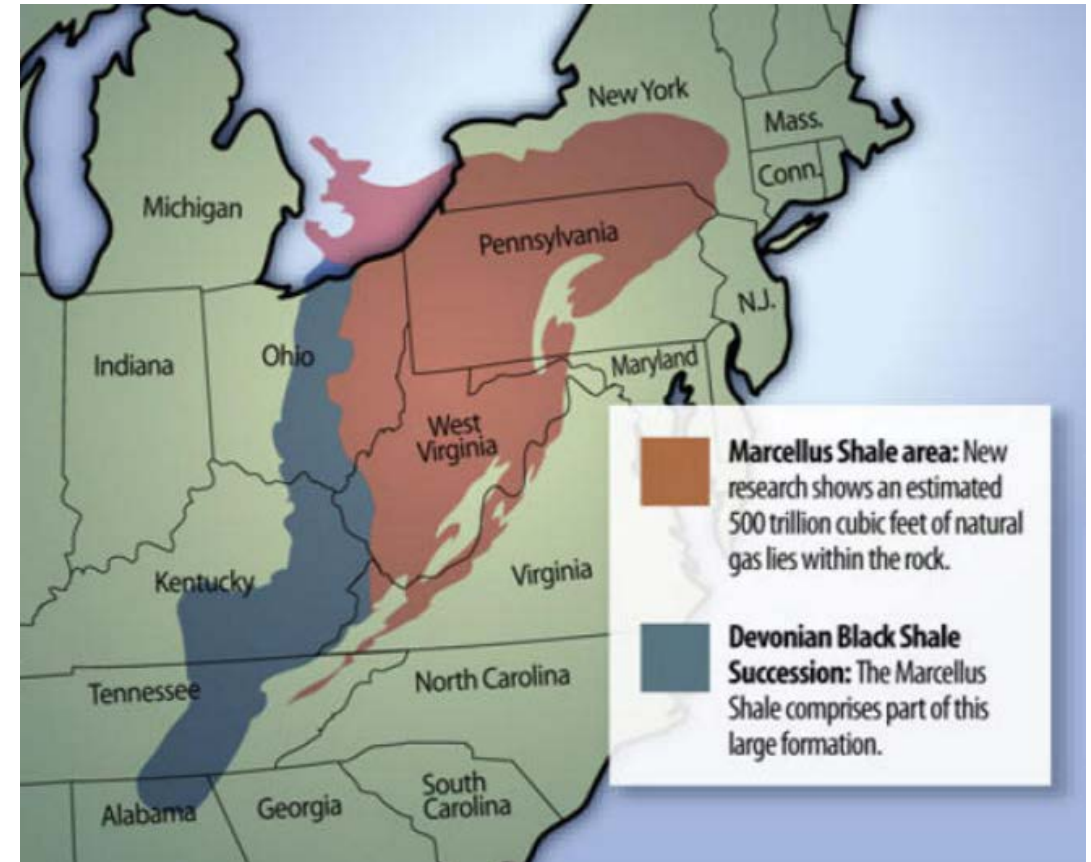
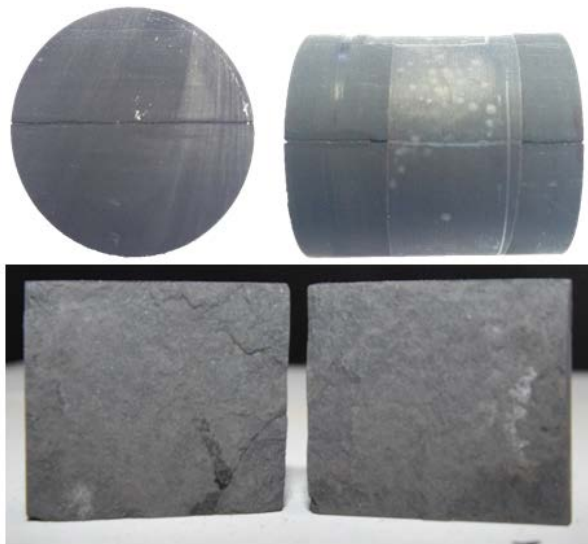
- Shearing is associated with micro-seismic events
 - Human Activities
 - Hydraulic fracturing
 - Change properties
 - Geometrical
 - Hydraulic



Experimental Section

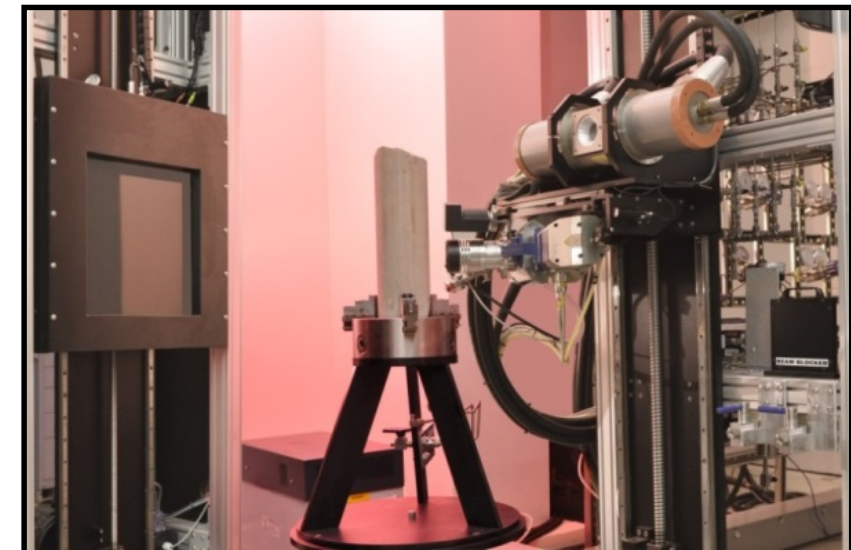
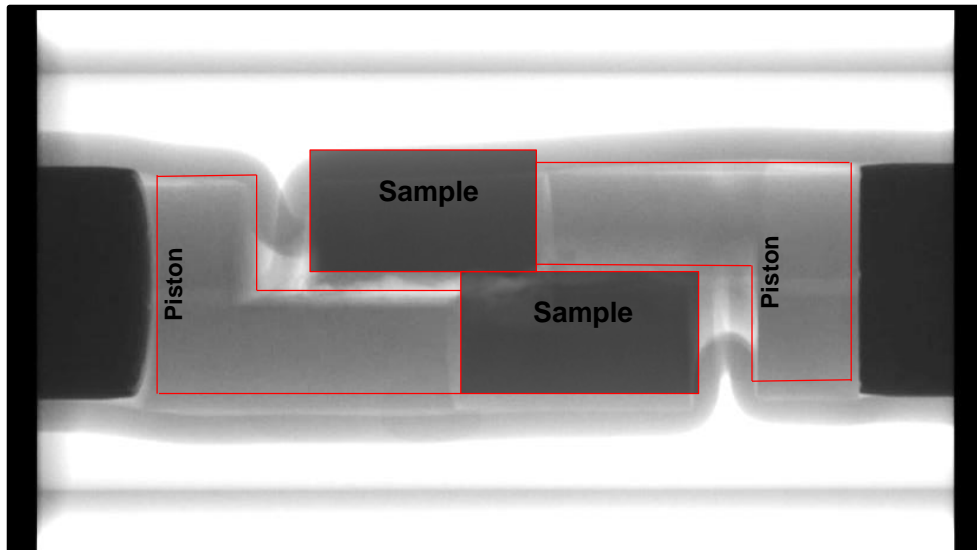
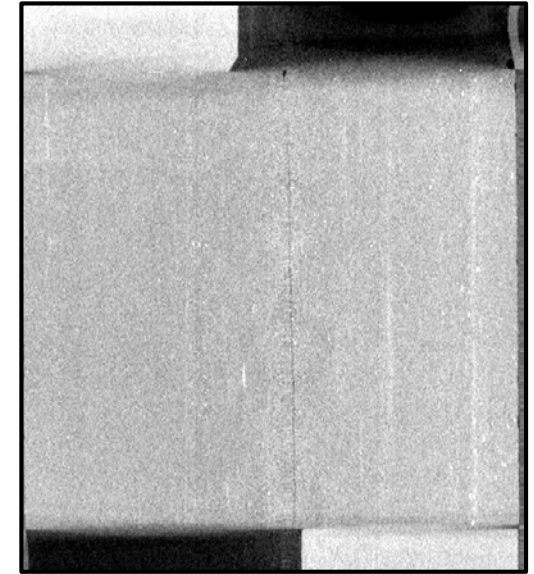


- Sample
 - Marcellus shale
 - Giant shale resource of natural gas
 - 3.8 (cm) diameter, 3.8 (cm) length
 - No natural fractures
 - Mechanically fractured

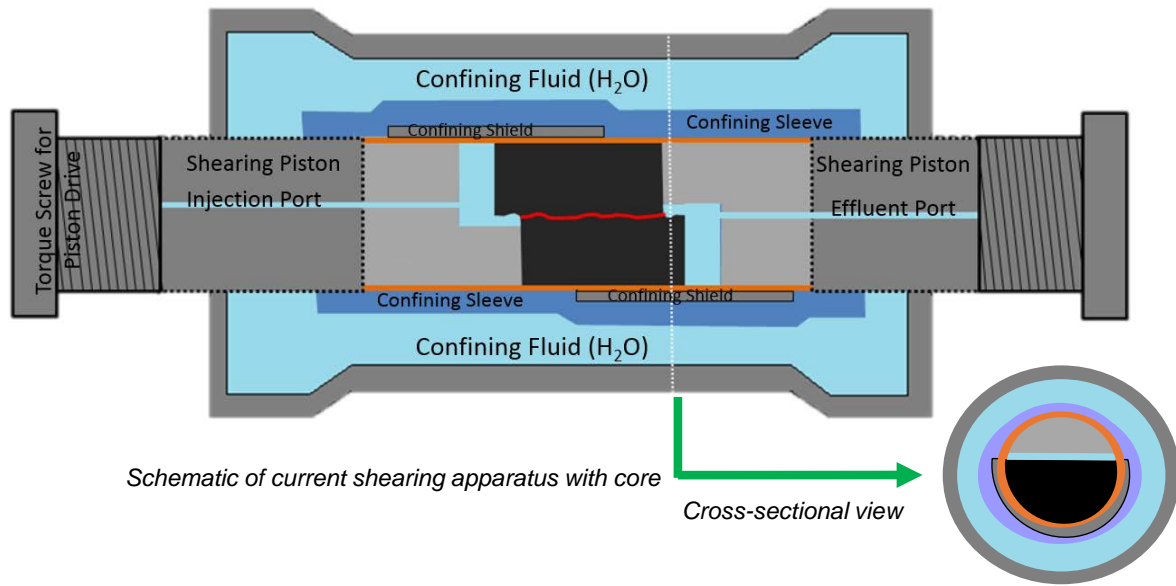


- Modified pistons within a Hassler core holder to shear fractured rocks in discrete steps
 - Total displacement of 4 cycles: 3.2 (mm)

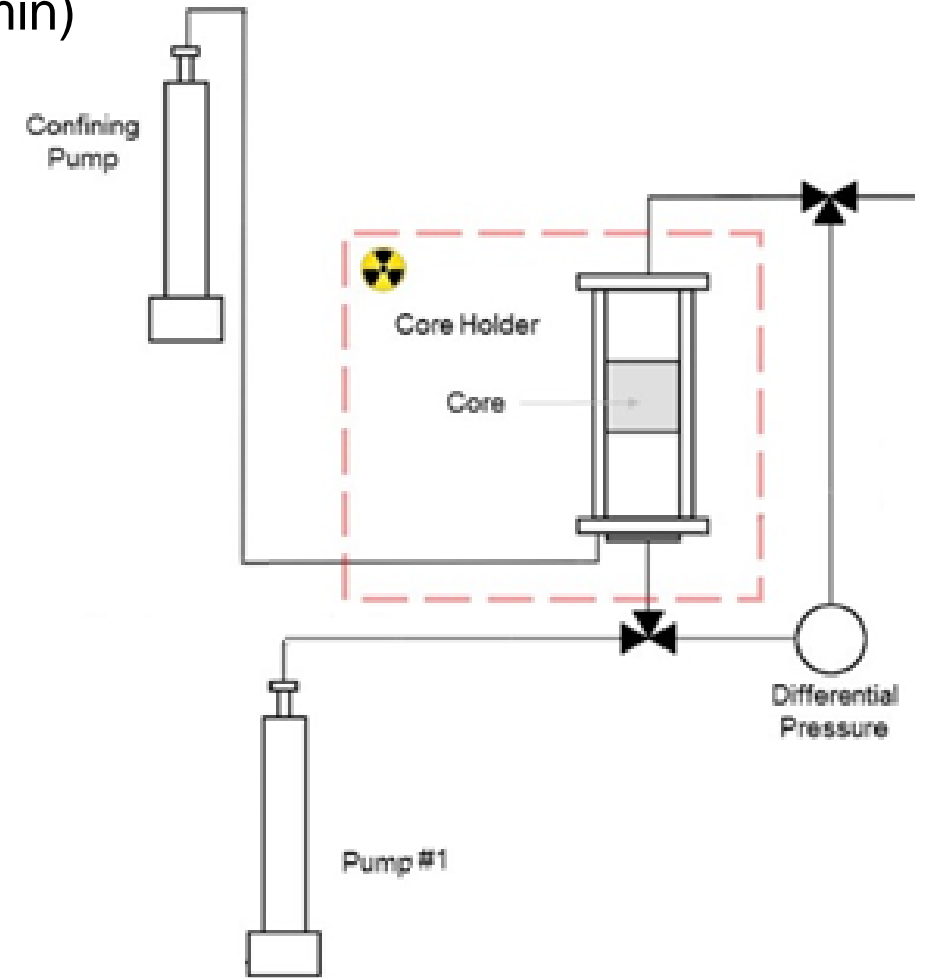
- Industrial computed tomography (CT) scanning with 26.8(μm) resolution
 - Obtain the geometry of the fracture



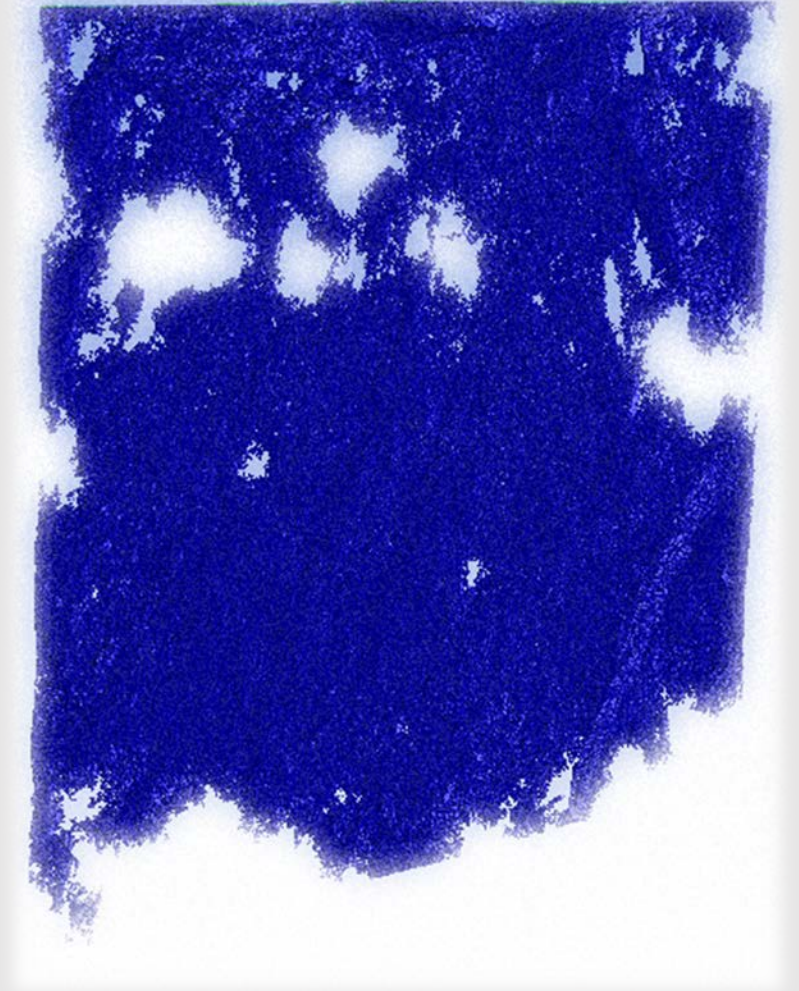
- Water fluid was injected with different flow rates (0-10 mL/min)
- Pressure drops were measured (0-2 MPa)



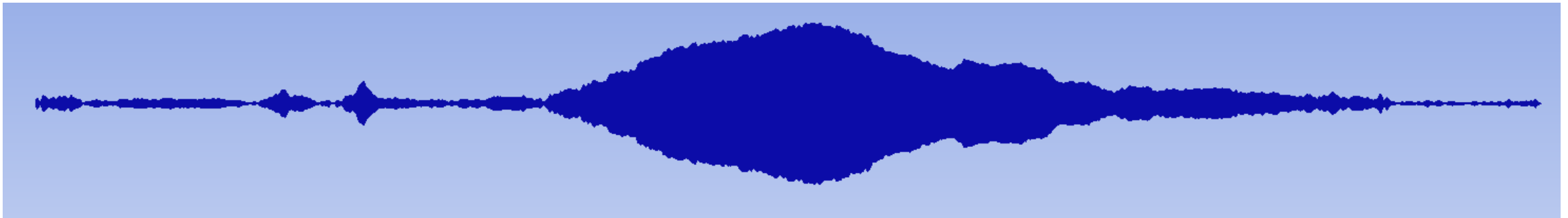
(mm)



Numerical Section



- Geometry
 - Full Map
 - Original resolution
 - Average Map
 - Reduced resolution
 - The small scale features of the rough fracture
 - Need less computational time
 - Effect of scan resolution



- ANSYS-Fluent Software

- Solve Conservation of Mass and Momentum Equations

$$\nabla \cdot \mathbf{u} = 0$$

$$\rho \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla P + \mu \nabla^2 \mathbf{u} + \rho \mathbf{g}$$

- Modified Local Cubic Law (MLCL) Model

- Collection of interconnected small parallel plates

- Laminar creeping flow

- Gradual variation

- Reynolds Equation: $0 = -\nabla P + \mu \nabla^2 u$

- $0 = -T_{x_{i,j}}(P_{i+1,j} - P_{i,j}) + T_{x_{i-1,j}}(P_{i,j} - P_{i-1,j}) - T_{z_{i,j}}(P_{i,j+1} - P_{i,j}) + T_{z_{i,j-1}}(P_{i,j} - P_{i,j-1})$

- $T_x = \beta_x \frac{h^3 \Delta z}{12 \Delta x}$, $T_z = \beta_z \frac{h^3 \Delta x}{12 \Delta z}$

➤ Cubic Law

➤ $\Delta p = \frac{12 \mu L}{W h_m^3} Q$

➤ Improved Cubic Law

➤ Roughness $h_{eq} = h_m \left(1 + 9 \left(\frac{\sigma_{apert}}{h_m} \right)^2 \right)^{-\frac{1}{6}}$

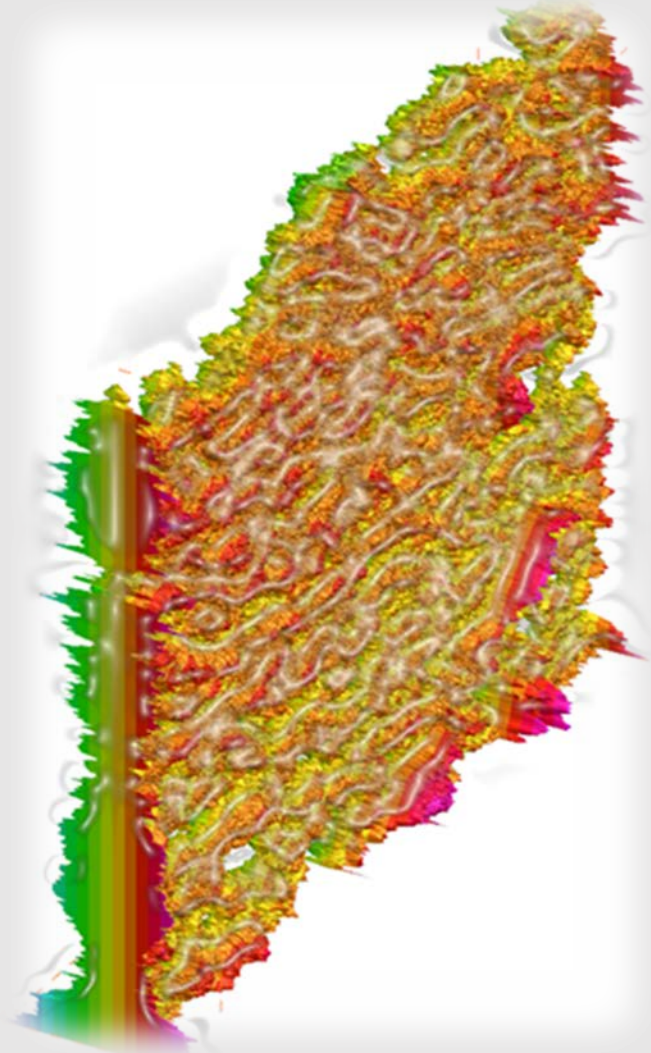
➤ Inertia and undulation $h_{eq} = h_m \left(1 - \frac{\sigma_{apert}}{h_m} \frac{\sqrt{\sigma_{slope}}}{10} \sqrt{Re} \right)^{\frac{1}{3}}$

➤ Equivalent aperture height

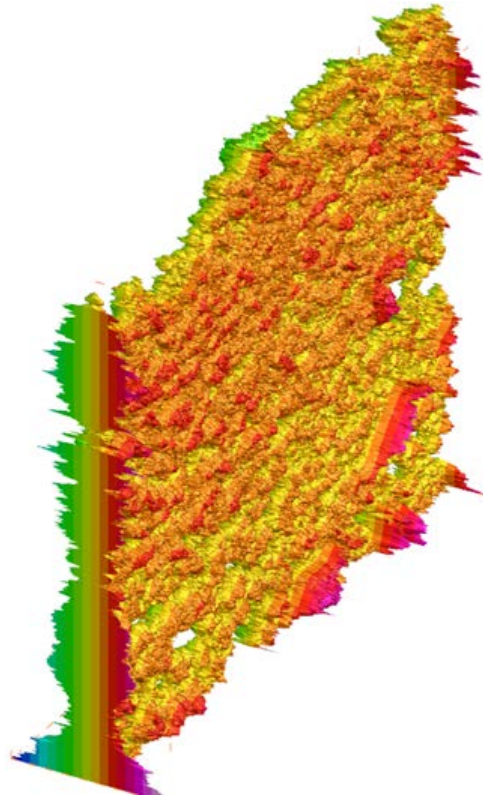
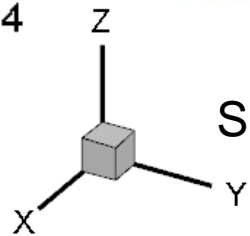
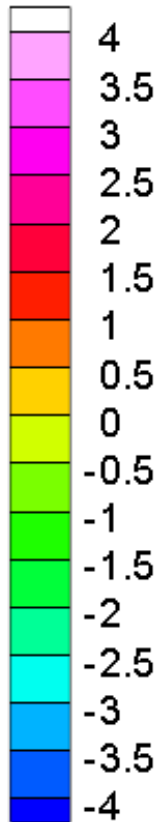
➤ $h_{eq} = h_m \left(1 + 9 \left(\frac{\sigma_{apert}}{h_m} \right)^2 \right)^{-\frac{1}{6}} \left(1 - \frac{\sigma_{apert}}{h_m} \frac{\sqrt{\sigma_{slope}}}{10} \sqrt{Re} \right)^{\frac{1}{3}}$

➤ $\Delta p = \frac{12 \mu L}{W h_{eq}^3} Q$

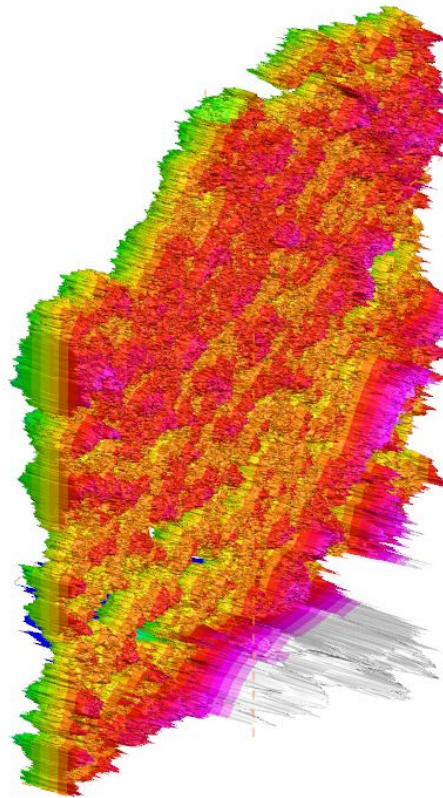
Results



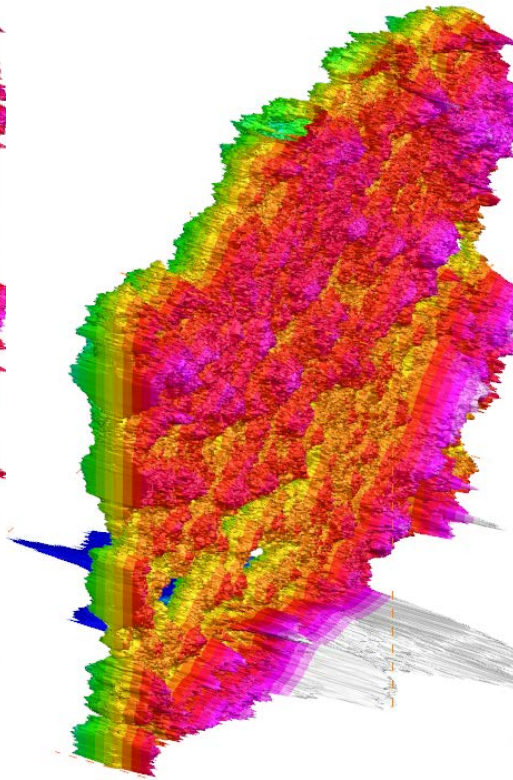
Height (mm)



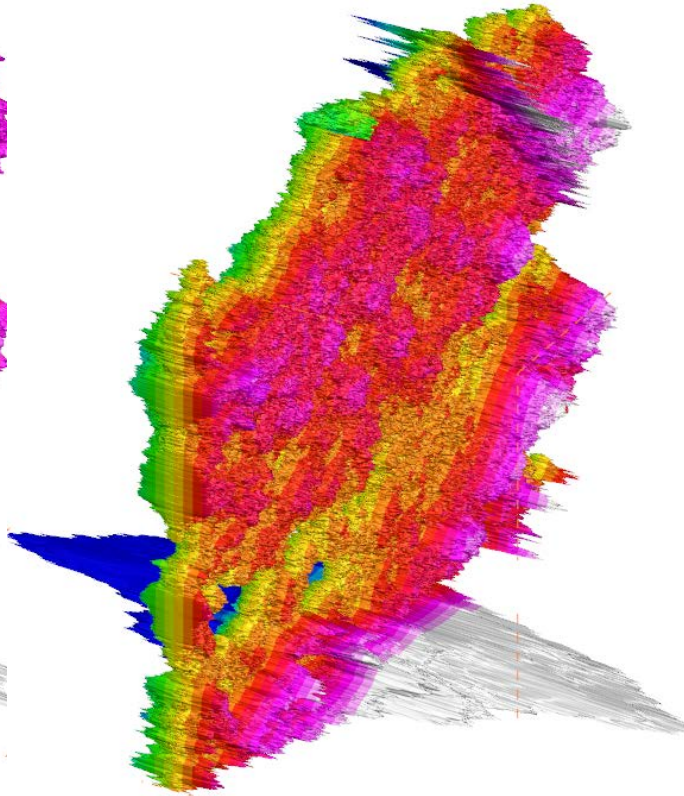
Shear Step 1



Shear Step 2



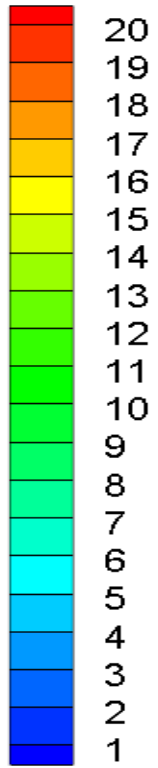
Shear Step 3



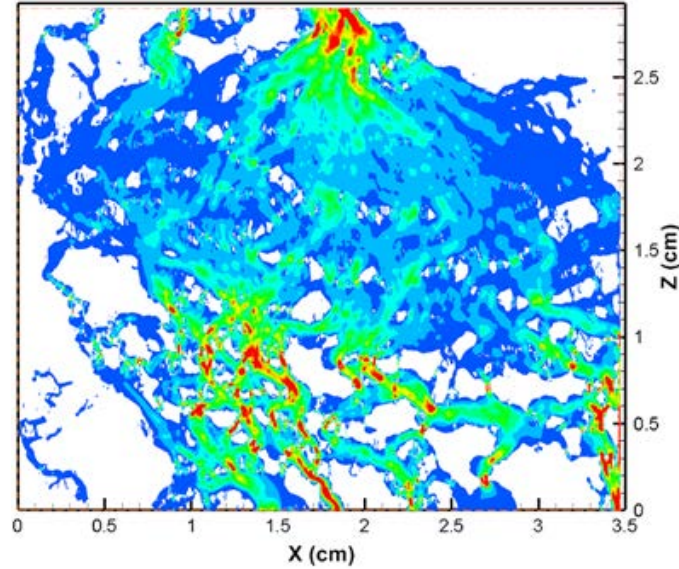
Shear Step 4

Velocity Contours

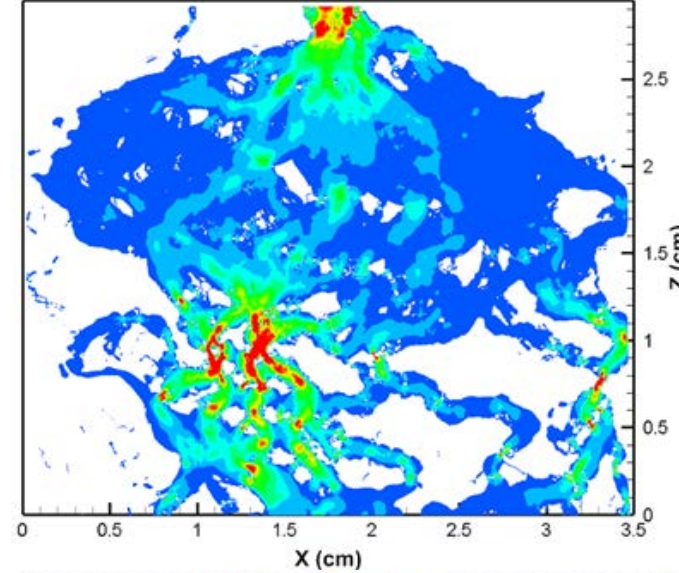
Velocity Magnitude (cm/s)



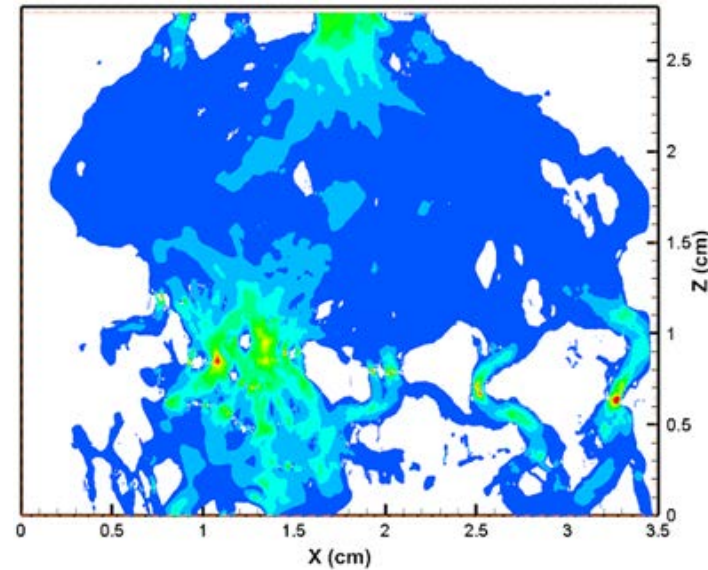
Shear Step 1



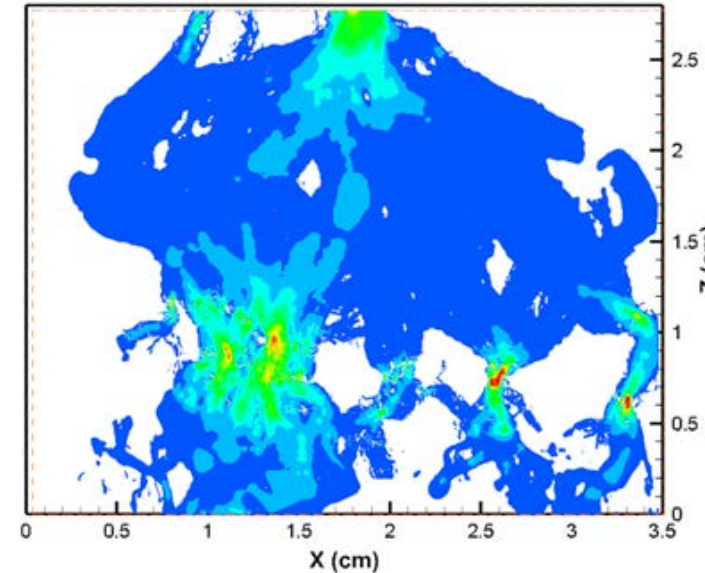
Shear Step 2



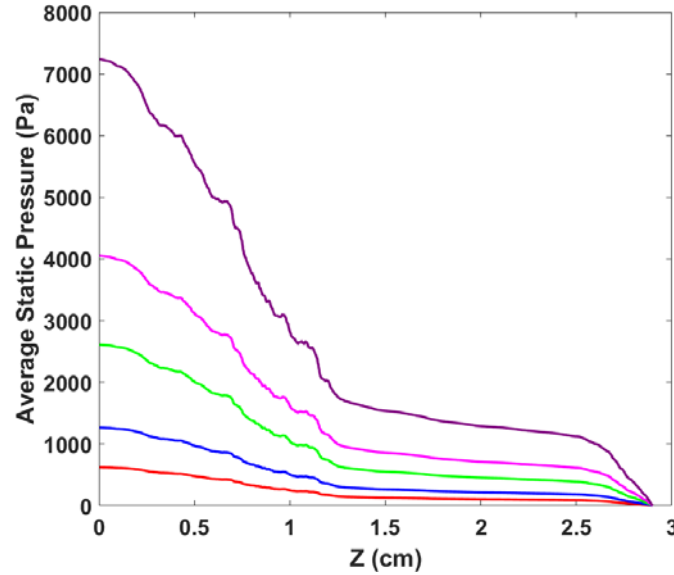
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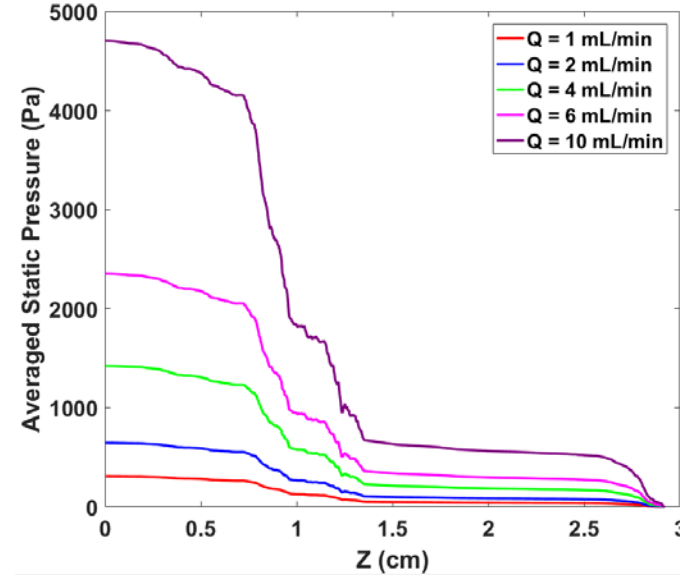
Shear Step 4



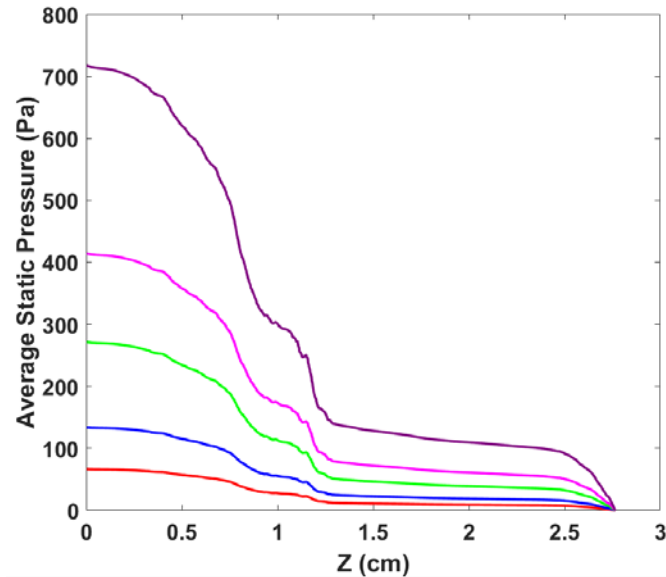
Shear Step 1



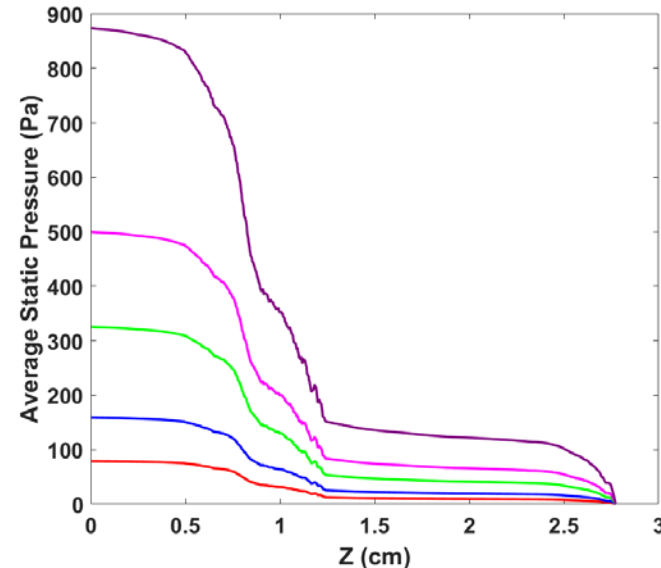
Shear Step 2



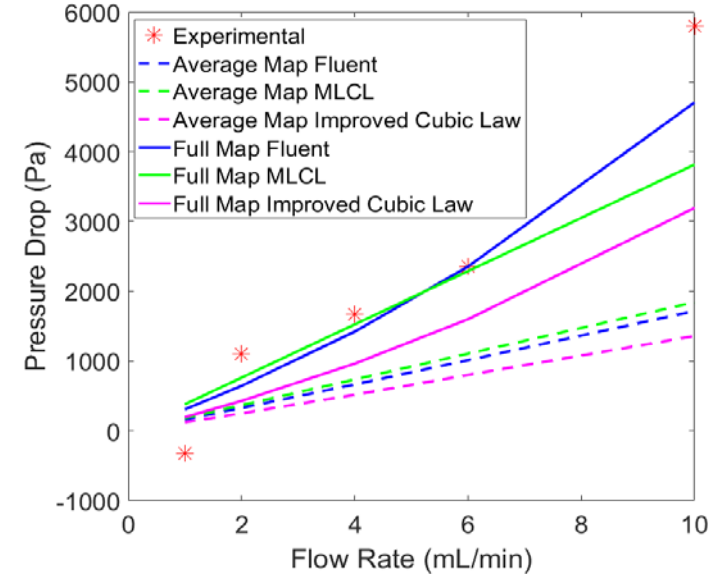
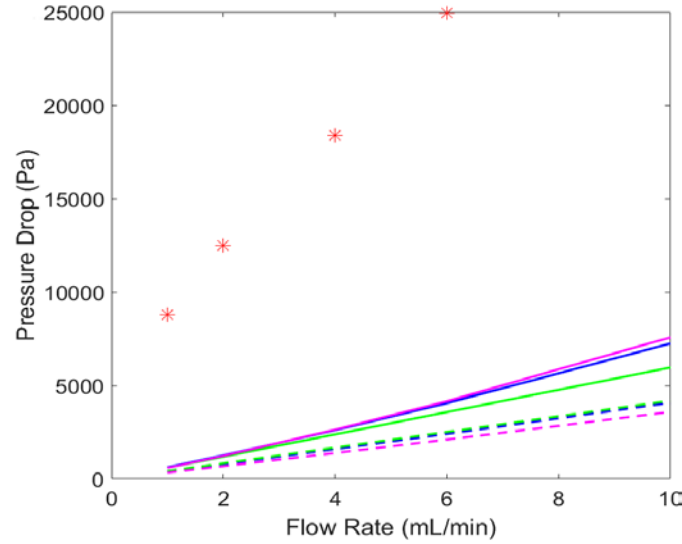
Shear Step 3



Shear Step 4

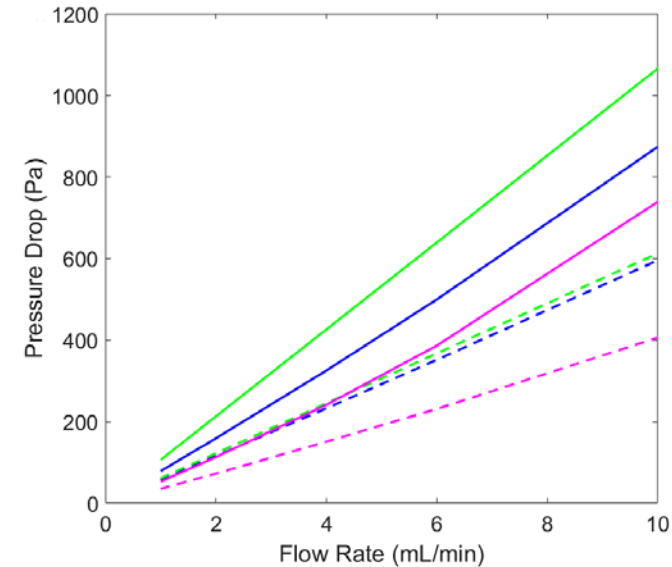
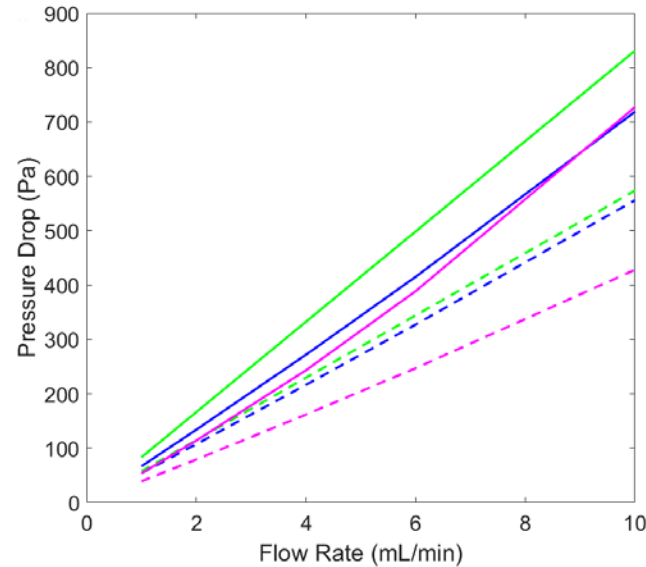


Shear Step 1



Shear Step 2

Shear Step 3



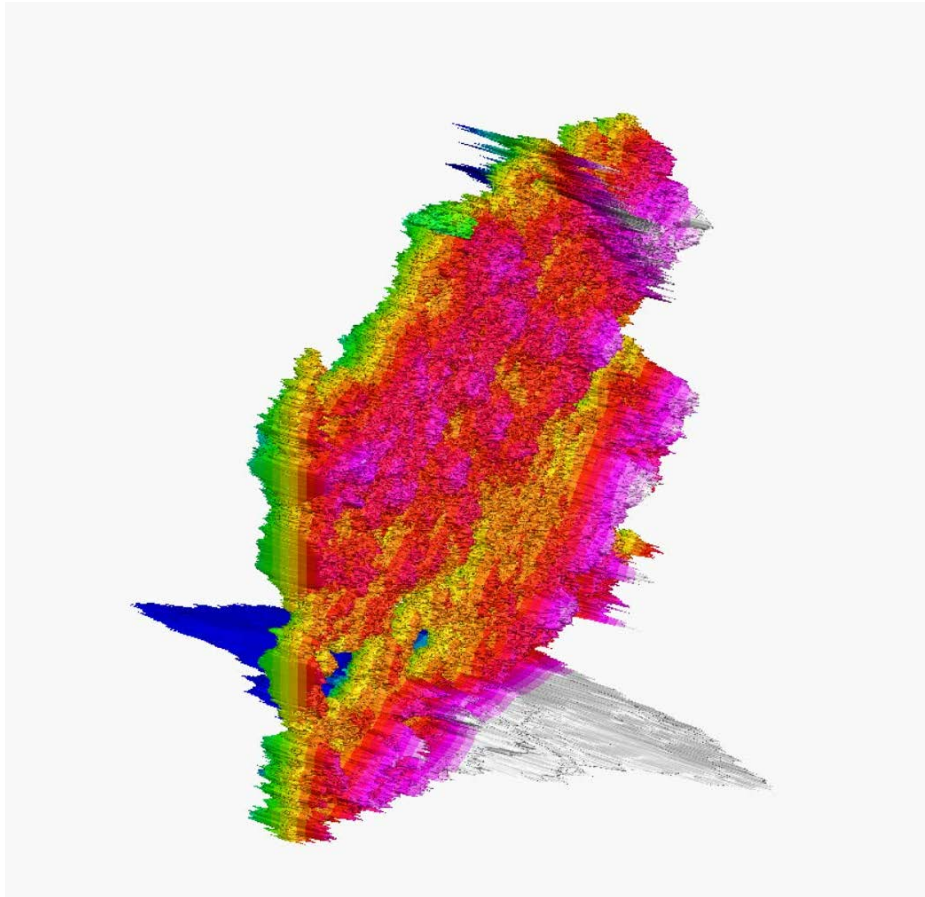
Shear Step 4

- A sheared Marcellus shale fracture was studied experimentally.
 - Sheared at different steps.
 - Permeability was measured at different flow rates.
 - The fracture was CT scanned at a high-resolution of 26.8 μm .
 - Geometry of the fractures was captured at each step.

- Low-resolution representations of the CT scans were created at 268 μm (average map).

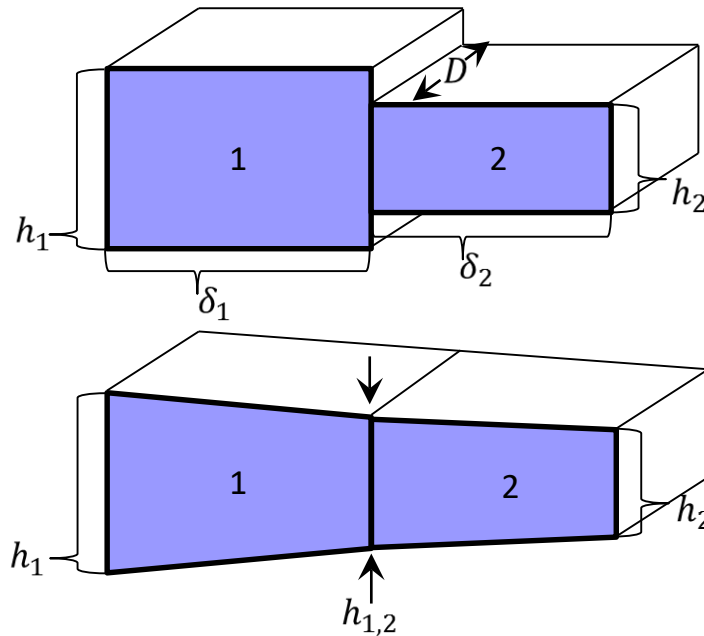
- The fracture flows were studied numerically for both the average and full maps.
 - ANSYS-Fluent Software.
 - The MLCL method.
 - The Improved Cubic Law.

- Shearing increased the average aperture.
- Pressure drops decreased.
- Flow velocities decreased.
- Smaller pressure drops for the average compared to those of the full map.
- Significant effects of small scale surface roughness.
- Importance effects of the resolution of the CT scan.
- Agreement between the numerical predictions.



thank you!

Grid Block Transition:



Local Cubic Law:

$$Q = \frac{(h_{1,2}^3 \cdot D)}{(12 \cdot \mu)} \cdot \frac{\Delta P_{1,2}}{\delta_{1,2}}$$

Stokes Tapered Plate Correction:

$$\delta_{1,2} = \frac{\delta_1 + \delta_2}{2} \quad \tan(\theta_{1,2}) = \frac{|h_1 - h_2|}{\delta_{1,2}}$$

$$h_{1,2}^3 = \left[\frac{2 \cdot h_1^2 \cdot h_2^2}{h_1 + h_2} \right] \cdot \left[\frac{3(\tan(\theta_{1,2}) - \theta_{1,2})}{\tan^3(\theta_{1,2})} \right]$$

This method strongly tends towards the smaller aperture

- CT scanning relies on capturing a large number of 2D x-ray
- Bulk matrix of rock was generated
- Fracture geometry was isolated via imageJ

