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Efficiently Modeling Primary Liquid Atomization using an Eulerian-Lagrangian Hybrid Model in ANSYS Fluent

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Outline



Spray applications



Transition criterion, Dynamic Mesh Adaption

Case study and comparison with experiments

Summary



Eulerian-Lagrangian Hybrid Model (VOF-DPM Hybrid Model)

Released in R19.0 ANSYS Fluent

VOF

- Interface Tracking
- Capture instabilities and large structures
- Fine mesh
- Small time steps

VOF→DPM Transition • Transition criteria: e.g.: Diameter,

Asphericity

- DPM
- Disperse (largest) part of spray
- Small, spherical droplets undergoing further changes
- Coarse mesh
- Large time steps

Eulerian-Lagrangian Hybrid Model Methodology

- VOF to DPM Transition Criteria
- Transition Control
- Dynamic Mesh Adaption

VOF to DPM Transition Criteria

Algorithm seeks to detect lumps which satisfy following two criteria:

- **1. Size Range** (Minimum and Maximum volume-equivalent diameter)
 - Volume equivalent sphere diameter of the lump

2. Shape

- Lumps with shape close to spherical shape
- Asphericity measure calculated in two ways
 - Normalized radius standard deviation (or variance)
 - Average radius-surface orthogonality

Lump must satisfy both size and shape based criteria to get elected for transition.





Above: Lumps colored by volume-equivalent diameter

Below: Lumps colored by asphericity criteria



Blue - almost spherical (good candidate for transition) Red - highly <u>a</u>spherical (Further breakage possible, not considered for transition)

Lump election using shape/asphericity

Goal is to identify lumps which are close to spherical shape using following criteria.

Asphericity = (1 – sphericity), i.e. 0 for perfect spheres, > 0 for eggs, leaves, etc.

- Normalized radius standard deviation

 Standard deviation of the distance between the facet center and the lump center of gravity (r₁, r₂, ... r_i)
 Asphericity → standard deviation normalized by the average radius
- Average radius-surface orthogonality

 Calculated from relative orthogonality of every facet of the lump surface

Relative orthogonality range from 0 to 1



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Lump election using shape/asphericity





Normalized standard deviation of drop radius

1-[radius-surface orthogonality]



Dynamic Mesh Adaption

 Resolves gas-liquid interface
 Travals with the interface

• Travels with the interface



Mesh continuously refined with moving interface



Lagrangian parcels are injected after mesh coarsening

Lump detection algorithm works with all different mesh topologies (hex, tet, polyhedral) and different mesh adaption algorithms including PUMA!!

Mesh

Refinement

Dynamic Adaption Methods

Hanging Node Adaption

 Available for all mesh topologies except Polyhedra



Polyhedral unstructured mesh adaption (PUMA)

- Refine all 3D cell types (polyhedra, tetrahedra, hexahedra, and so on)
- Consumes less memory



Case study: Liquid Jet in Crossflow

| Crossflow Weber number | 16 (bag breakup regime) |
|-------------------------|--|
| Momentum flux ratio | 121 |
| Nozzle state | TURBULENT |
| Nozzle diameter | 2 mm |
| Split factor | 1e6 (splitting inhibited) |
| Turbulence | SST K-Omega with SBES |
| P-v coupling | PISO |
| Pressure discretisation | PRESTO! |
| VOF scheme | Explicit |
| VOF discretisation | Geo-reconstruct |
| URF | Pres=0.9,Mom=0.95 |
| AMG settings | Conservative+Aggressive coarsening |
| Initial mesh | 6.9 million hex cells – 15 cells across nozzle in breakup region |
| Adapted mesh | 14.9 million – max 2 levels of refinement - 60 cells across nozzle |
| Mesh adaption | Normalised vf gradient (0.01 to 0.05) + isovalue adaption 0.45 to 0.55 |
| Secondary Break-Up | No |

Liquid Jet in Crossflow





Liquid Jet in Crossflow



DPM data collection for faster DPM only simulation

VOF to DPM Hybrid Model

- Collection of DPM statistics

DPM only simulation

- Using DPM statistics to perform DPM only simulation





Liquid Jet in Cross Flow – Comparison with experimental data

| Operating Conditions | | | | |
|-------------------------------------|--------------------------|--|--|--|
| V _{Liq} (m/s) | 32 | | | |
| m _{Liq} (kg/s) | 0.004 | | | |
| D _{liq} (mm) | 0.458 | | | |
| Liquid Density (kg/m ³) | 780.6 | | | |
| Liquid viscosity (Pa.s) | 0.0007 | | | |
| Air Density (kg/m³) | 5.88 | | | |
| Chamber Temperature (K) | 300 | | | |
| Operating Pressure (psi) | 73.48 | | | |
| Surface Tension (N/m) | 0.0197 | | | |
| Secondary breakup | Wave | | | |
| Air flow rate | Inlet Profile | | | |
| Weber Number (We) | 1000 & <mark>1500</mark> | | | |
| Momentum Flux Ratio (J) | 10 & 20 | | | |
| Mesh Topology | Hex and Poly | | | |
| Mesh Count | 10M (Hex); 4.5M (Poly) | | | |



Sekar, J., Rao, A., Pillutla, S., Danis, A., Hsieh, S., Proceedings of ASME Turbo Expo 2014

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Generating Sauter Mean Diameter Data

- Several 1 mm x1 mm bounded planes stacked up at z/d=30 and z/d=60 locations (d=diameter of orifice)
 - Act as probes
- Every time a particle hits the probe, the data is recorded in a file
- These probes collect data for several liquid passes
- Time averaged Sauter Mean diameter values for each probe compared to measured data



Results: Dynamic Mesh Adaption

- Uniform background
 - Hex ~ 2.2 Mil. Cells
 - Poly ~ 2 Mil. Cells
- Mesh adaption based on gradient of liquid volume fraction
 - 2 Levels of Mesh adaption
- Liquid penetration for both mesh types are in good agreement with measurements
- Sauter mean diameter predictions are overall good at both locations
 - Some discrepancies found for hex mesh type

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Comparison of the SMDs along the wallnormal center line at z/d=60

• Experiment • Hex-adapt • Poly-adapt

X (mm)

Summary

- A new VOF-DPM transition model in ANSYS Fluent
- VOF-DPM transition tool combined with dynamic mesh adaption enables to carry out a detailed numerical analysis of spray behavior at affordable computational cost.
- Application of the VOF-DPM hybrid model on industry relevant jet in crossflow and diesel sprays shows encouraging results.

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