

**U. S. Department of Energy – National Energy Technology Laboratory (NETL)
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**Effects of particle Froude number on the sub-grid
behavior of fluidized gas-particle flows**

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At the 2021 NETL Multiphase Flow Science workshop we presented:

On the effect of particle Froude number in sub-grid modeling of gas-solid fluidized flows

Among the conclusions of that work we stated that:

Before new sub-grid models could be derived accounting for particle Froude number, further work would be required to account for:

higher domain average gas Reynolds numbers
a variety of domain average solid volume fractions

Those goals have been achieved, and related outcomes are now exposed in two presentations:

- 1) Results accounting for ranges of domain average gas Reynolds numbers and solid volume fractions, for a range of particle Froude numbers**
- 2) New sub-grid models for effective drag, filtered and residual stresses**

Presentation (1) follows next.

Filtered two-fluid modeling

We ultimately aim to provide sub-grid models for filtered two-fluid modeling.

$$\begin{aligned} \frac{\partial}{\partial t}(\rho_g \bar{\phi}_g) + \nabla \cdot (\rho_g \bar{\phi}_g \tilde{\mathbf{v}}_g) &= 0 & \frac{\partial}{\partial t}(\rho_s \bar{\phi}_s) + \nabla \cdot (\rho_s \bar{\phi}_s \tilde{\mathbf{v}}_s) &= 0 \\ \frac{\partial}{\partial t}(\rho_g \bar{\phi}_g \tilde{\mathbf{v}}_g) + \nabla \cdot (\rho_g \bar{\phi}_g \tilde{\mathbf{v}}_g \tilde{\mathbf{v}}_g) &= -\bar{\phi}_g \nabla \cdot \tilde{\boldsymbol{\sigma}}_g - \nabla \cdot \mathbf{r}'_g - \bar{\mathbf{M}}_I + \rho_g \bar{\phi}_g \mathbf{g} \\ \frac{\partial}{\partial t}(\rho_s \bar{\phi}_s \tilde{\mathbf{v}}_s) + \nabla \cdot (\rho_s \bar{\phi}_s \tilde{\mathbf{v}}_s \tilde{\mathbf{v}}_s) &= -\nabla \cdot \bar{\boldsymbol{\sigma}}_s - \nabla \cdot \mathbf{r}'_s - \bar{\phi}_s \nabla \cdot \tilde{\boldsymbol{\sigma}}_g + \mathbf{B}'_{gs} + \bar{\mathbf{M}}_I + \rho_s \bar{\phi}_s \mathbf{g} \\ \bar{\mathbf{M}}_I &= (1-H)\bar{\beta}(\tilde{\mathbf{v}}_g - \tilde{\mathbf{v}}_s) \\ \tilde{\boldsymbol{\sigma}}_g &= \left[\tilde{\mathbf{P}}_g - (\lambda_g + \frac{2}{3}\mu_g)(\nabla \cdot \tilde{\mathbf{v}}_g) \right] \mathbf{I} - 2\mu_g \tilde{\boldsymbol{\mathbf{s}}}_g \\ \bar{\boldsymbol{\sigma}}_s &= \left[\bar{\mathbf{P}}_s - (\lambda_s + \frac{2}{3}\mu_s)(\nabla \cdot \mathbf{v}_s) \right] \mathbf{I} - 2\bar{\mu}_s \tilde{\boldsymbol{\mathbf{s}}}_s = \mathbf{P}_{\text{fil},s} \mathbf{I} - 2\mu_{\text{fil},s} \tilde{\boldsymbol{\mathbf{s}}}_s \\ \mathbf{r}'_l &= \rho_l \bar{\phi}_l \tilde{\mathbf{v}}_l \tilde{\mathbf{v}}_l - \rho_l \bar{\phi}_l \tilde{\mathbf{v}}_l \tilde{\mathbf{v}}_l = \mathbf{P}_{\text{res},l} \mathbf{I} - 2\mu_{\text{res},l} \tilde{\boldsymbol{\mathbf{s}}}_l \\ \tilde{\boldsymbol{\mathbf{s}}}_l &= \frac{1}{2} \left[\nabla \tilde{\mathbf{v}}_l + (\nabla \tilde{\mathbf{v}}_l)^T \right] - \frac{1}{3} (\nabla \cdot \tilde{\mathbf{v}}_l) \mathbf{I} \end{aligned}$$

Effective, filtered and residual closures

$$H = 1 - \frac{\beta_{\text{eff}}}{\bar{\beta}} \quad \beta_{\text{eff}} = \frac{\overline{\beta(\mathbf{v}_g - \mathbf{v}_s)}}{(\tilde{\mathbf{v}}_g - \tilde{\mathbf{v}}_s)}$$

$$\mathbf{P}_{\text{fil},s} = \frac{1}{3} \text{tr} \left[\bar{\mathbf{P}}_s - (\lambda_s + \frac{2}{3}\mu_s)(\nabla \cdot \mathbf{v}_s) \right]$$

$$\mu_{\text{fil},s} = \bar{\mu}_s$$

$$\mathbf{P}_{\text{res},l} = \frac{1}{3} \text{tr}(\mathbf{r}'_l)$$

$$\mu_{\text{res},l} = \frac{|\mathbf{r}'_{\text{shear},l}|}{2|\tilde{\boldsymbol{\mathbf{s}}}_{\text{shear},l}|}$$

We go for effective, filtered and residual parameters by filtering over predictions from highly resolved simulations (HRS) with microscopic two-fluid modeling.



Microscopic two-fluid modeling

On the basis of Anderson and Jackson' formulation, with microscopic closures as implemented into the MFI code by Agrawal et al. (2001).

$$\frac{\partial}{\partial t}(\rho_g \phi_g) + \nabla \cdot (\rho_g \phi_g \mathbf{v}_g) = 0$$

$$\frac{\partial}{\partial t}(\rho_s \phi_s) + \nabla \cdot (\rho_s \phi_s \mathbf{v}_s) = 0$$

$$\frac{\partial}{\partial t}(\rho_g \phi_g \mathbf{v}_g) + \nabla \cdot (\rho_g \phi_g \mathbf{v}_g \mathbf{v}_g) = -\phi_g \nabla \cdot \boldsymbol{\sigma}_g - \mathbf{M}_I + \rho_g \phi_g \mathbf{g}$$

$$\frac{\partial}{\partial t}(\rho_s \phi_s \mathbf{v}_s) + \nabla \cdot (\rho_s \phi_s \mathbf{v}_s \mathbf{v}_s) = -\nabla \cdot \boldsymbol{\sigma}_s - \phi_s \nabla \cdot \boldsymbol{\sigma}_g + \mathbf{M}_I + \rho_s \phi_s \mathbf{g}$$

$$\mathbf{M}_I = \beta(\mathbf{v}_g - \mathbf{v}_s)$$

$$\boldsymbol{\sigma}_\ell = \left[P_\ell - \left(\lambda_\ell + \frac{2}{3} \mu_\ell \right) (\nabla \cdot \mathbf{v}_\ell) \right] \mathbf{I} - 2\mu_\ell \mathbf{s}_\ell$$

$$\mathbf{s}_\ell = \frac{1}{2} \left[\nabla \mathbf{v}_\ell + (\nabla \mathbf{v}_\ell)^T \right] - \frac{1}{3} (\nabla \cdot \mathbf{v}_\ell) \mathbf{I}$$

Microscopic closures

Drag

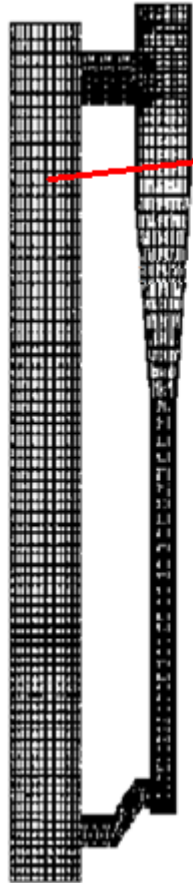
Wen and Yu (1966)

Solid phase pressure and viscous stresses

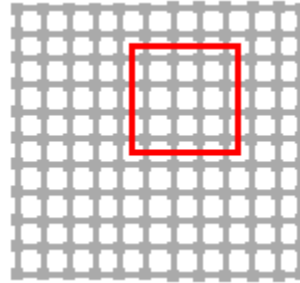
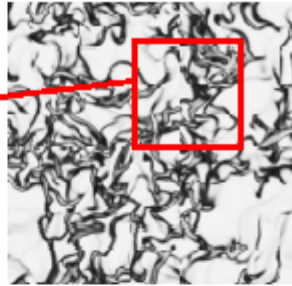
Lun et al. (1984),

as adapted by Agrawal et al. (2001)

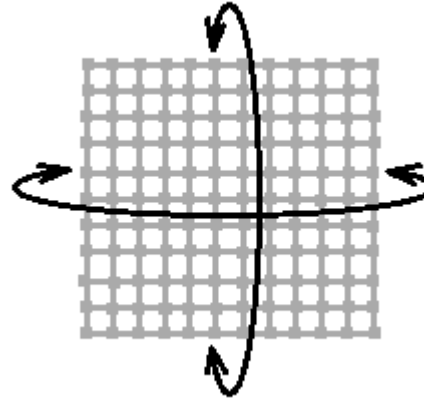
Highly resolved simulations (MFIx) / filtering



LSS



HRS



- All periodic boundaries
- 16 x 16 cm domain
- 128 x 128 grids
- 1.25 x 1.25 mm grid cells
- up to 4 x 4 cm filter sizes

| | |
|---|---|
| d_p | 40 / 75 / 150 / 300 μm |
| $Fr_p = v_t^2 / (gd_p)$ | 12.21 / 64.85 / 286.69 / 799.22 |
| ρ_s | 1500 kg/m^3 |
| e | 0.9 |
| ρ_g | 1.3 kg/m^3 |
| μ_g | 1.8×10^{-5} kg/(m s) |
| $\langle \phi_s \rangle$ | 0.05 / 0.15 / 0.25 / 0.35 / 0.45 / 0.55 |
| $\langle Re_g \rangle / \langle Re_g \rangle_{\text{susp}}$ | 1 / 8.15 / 16.30 / 24.45 |

Filtered data classified
by narrow ranges of

$$\bar{\phi}_s, \tilde{V}_{\text{slip},y}$$

Some results

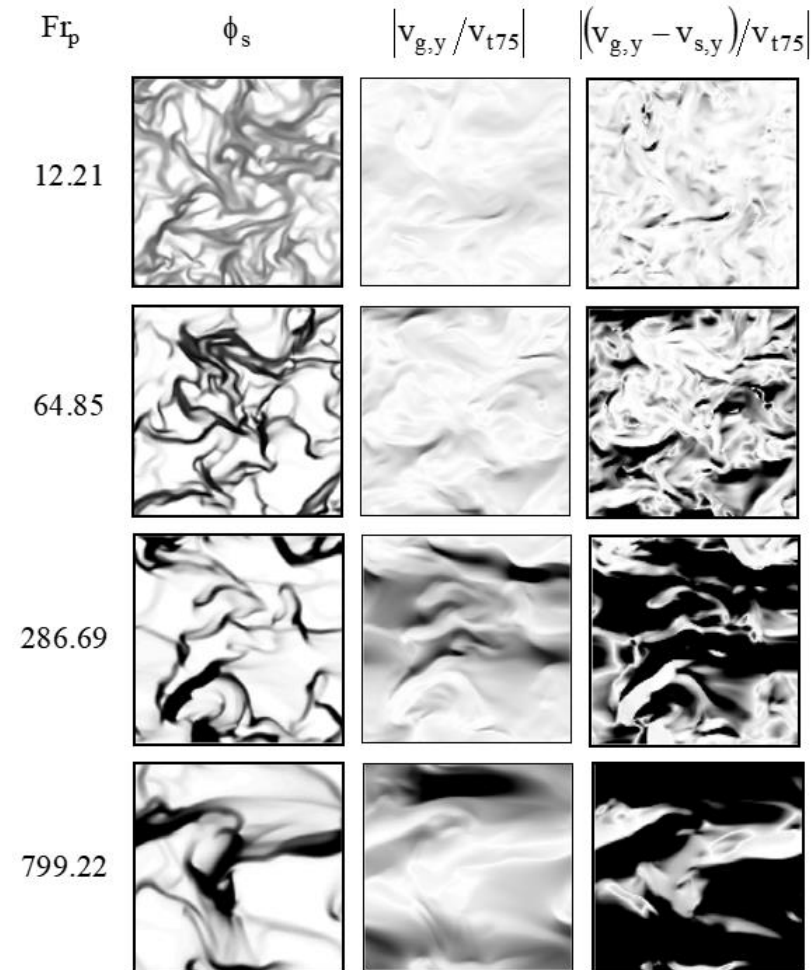
Grayscale plots (in the statistical steady state regime)

For a case with $\langle \phi_s \rangle = 0.15$ and $\langle \text{Re}_g \rangle / \langle \text{Re}_g \rangle_{\text{susp}} = 1$

[ϕ_s from 0 (white) to 0.64 (black)

$|v_{g,y} / v_{t75}|$ from 0 (white) to >28.71 (black)

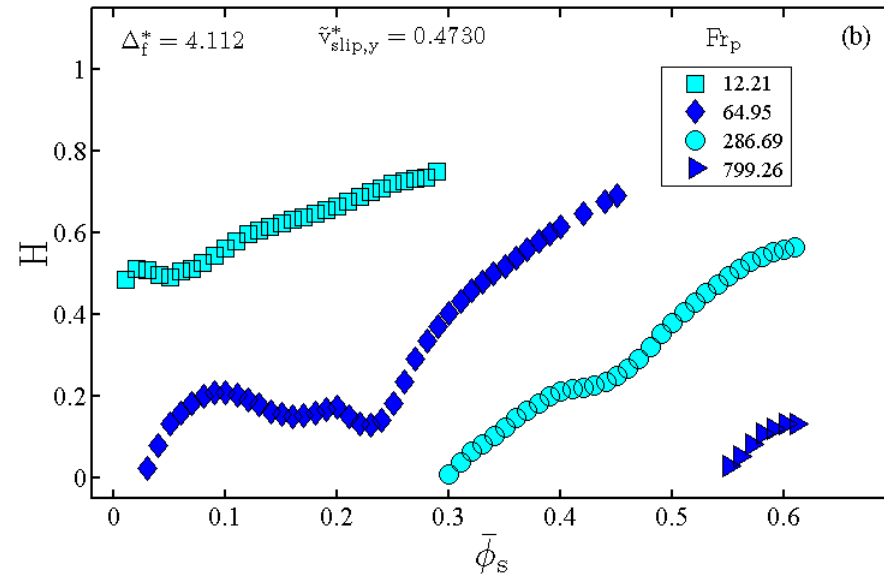
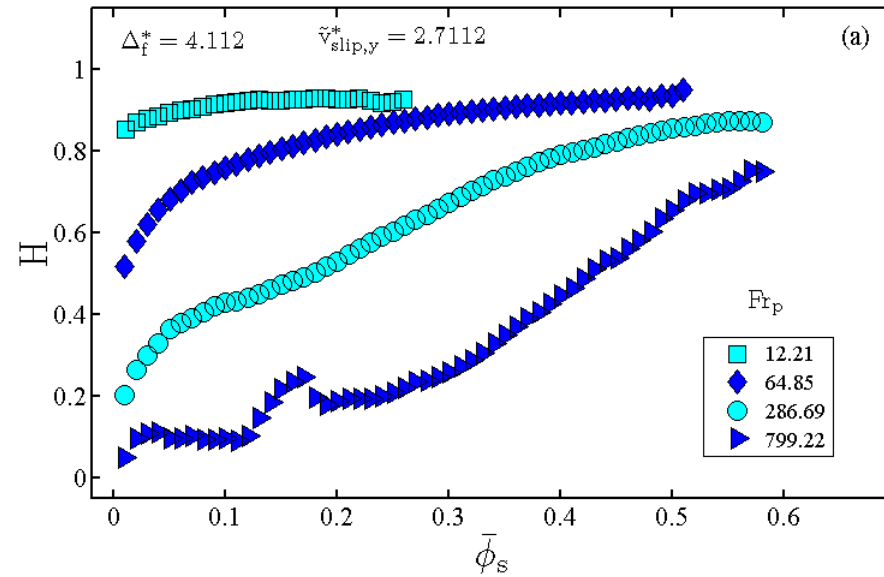
$|(v_{g,y} - v_{s,y}) / v_{t75}|$ from 0 (white) to >2.93 (black)]

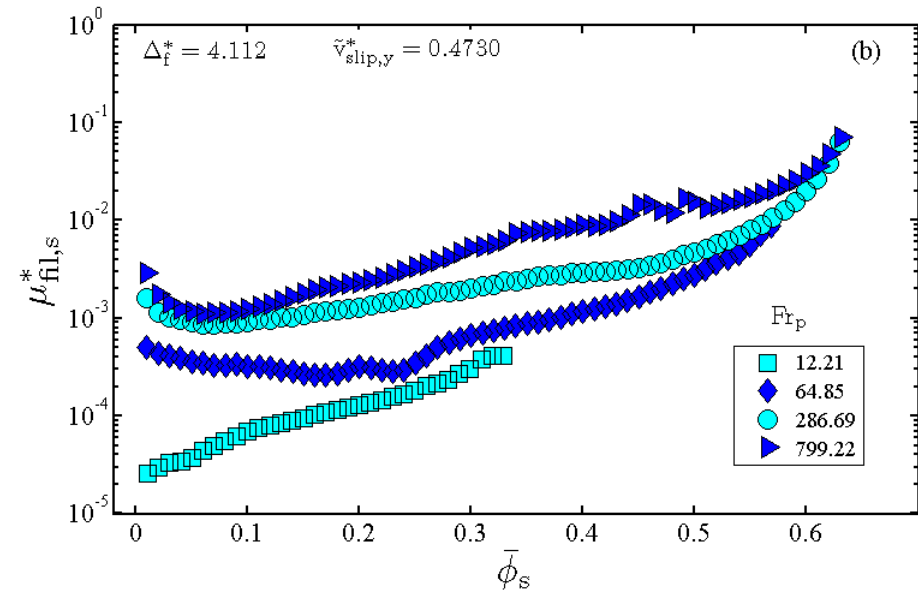
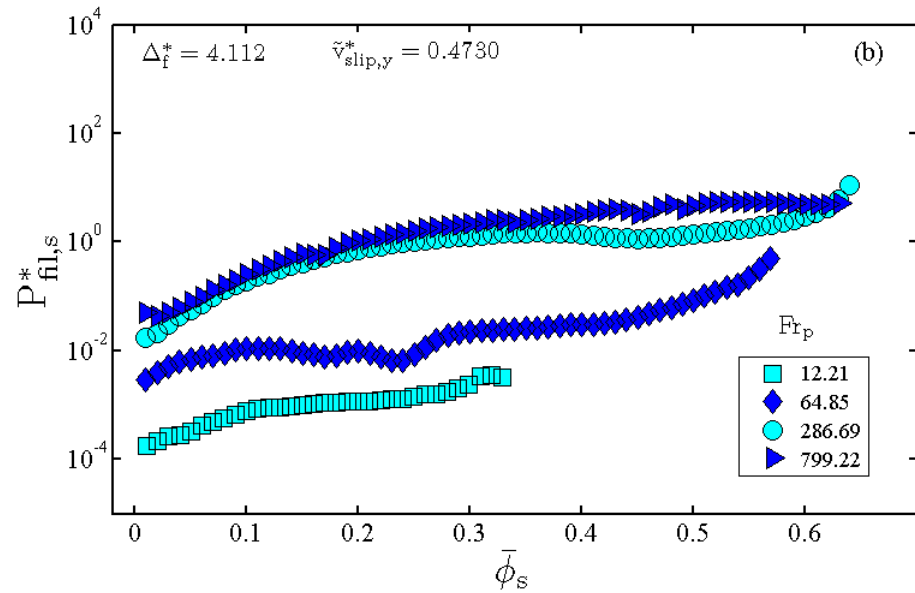
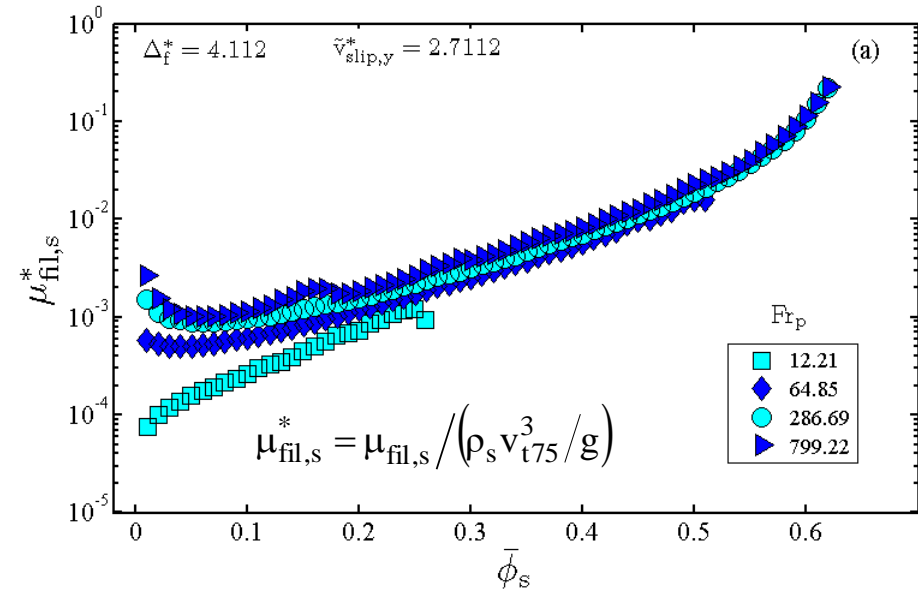
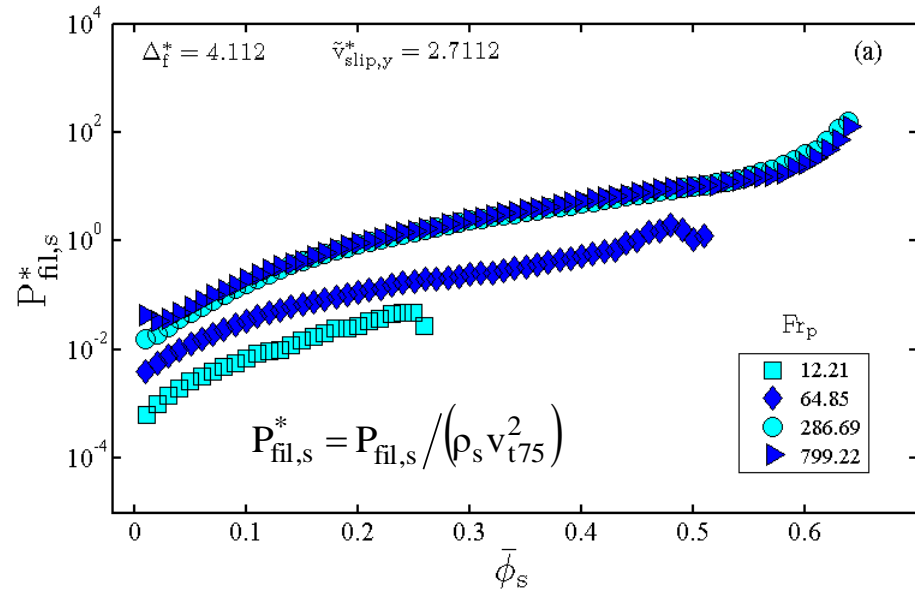


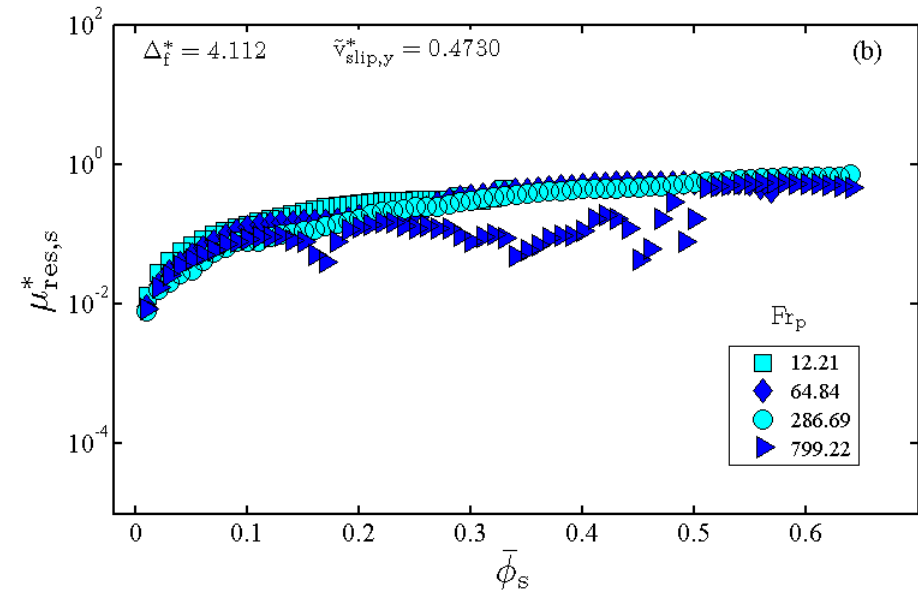
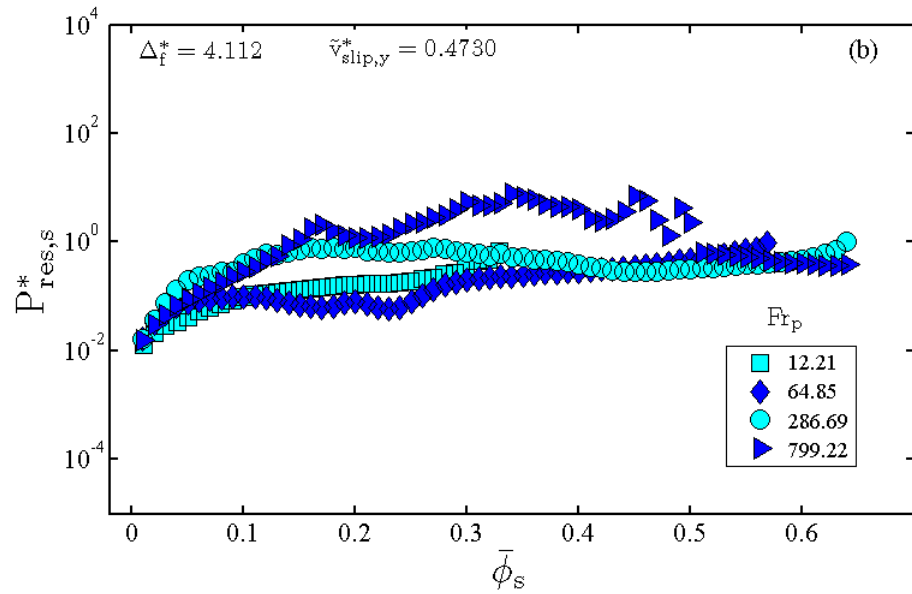
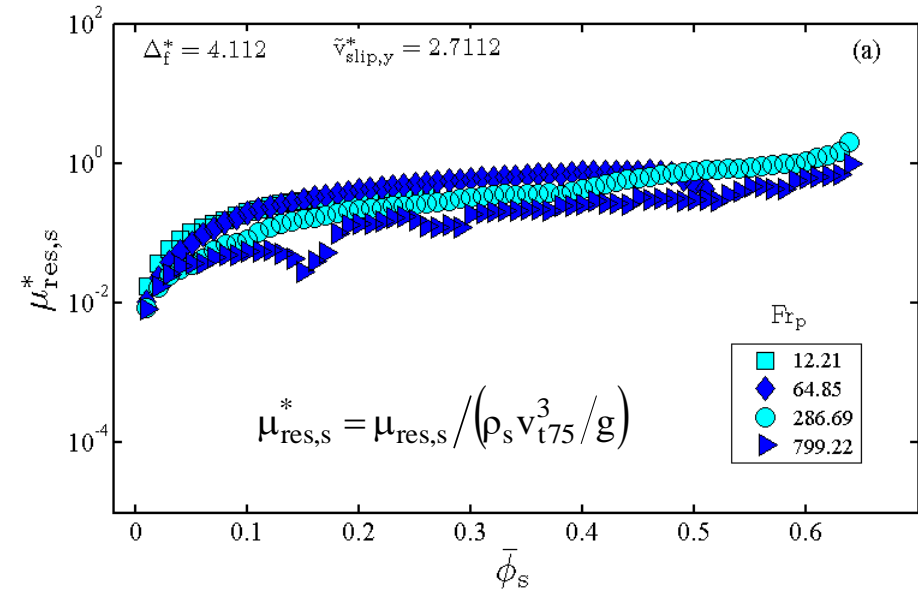
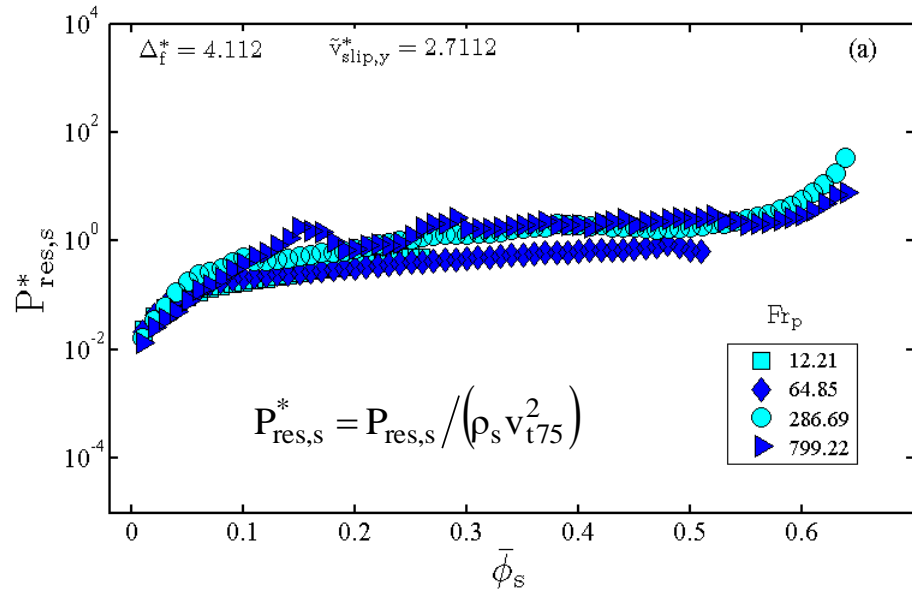
$$\tilde{v}_{\text{slip},y}^* = \left| \tilde{v}_{\text{slip},y} / v_{t75} \right|$$

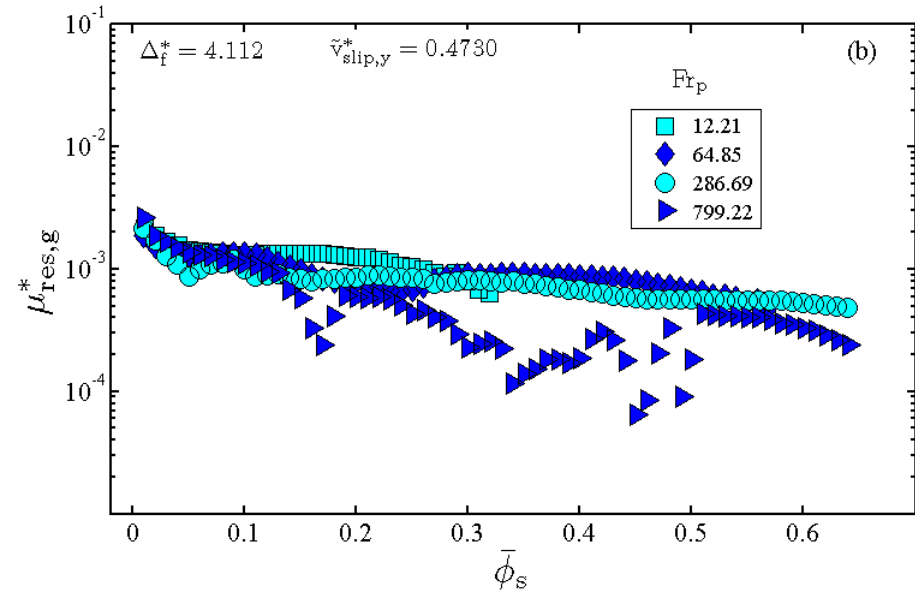
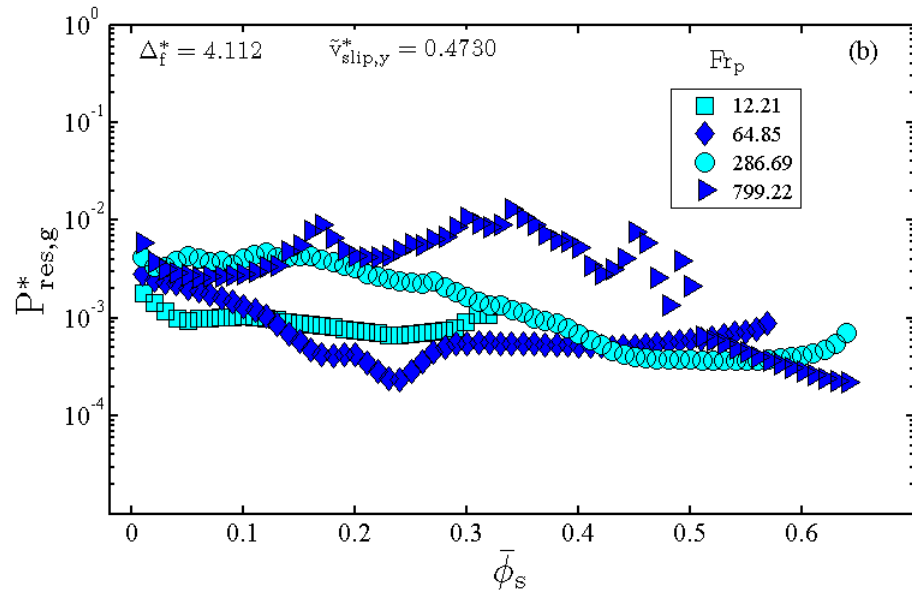
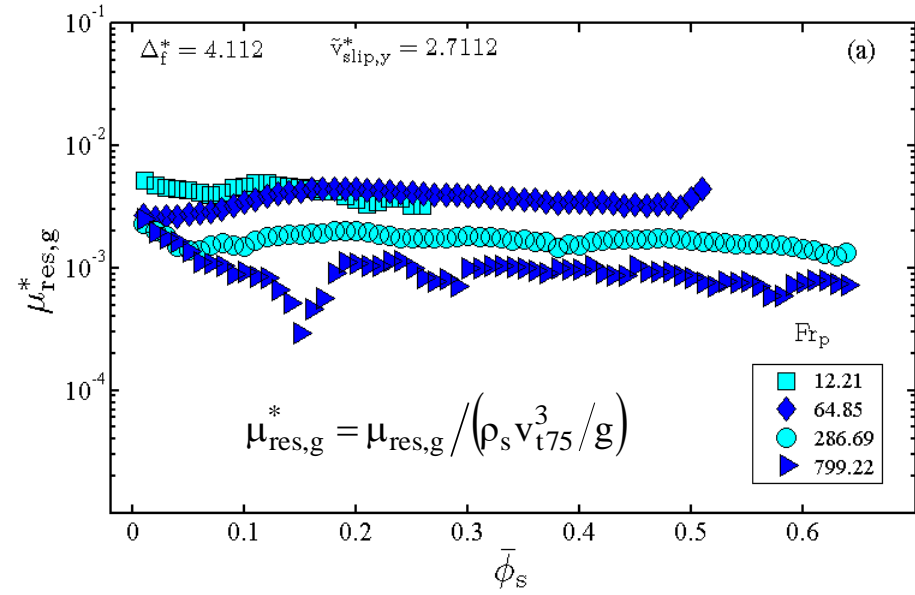
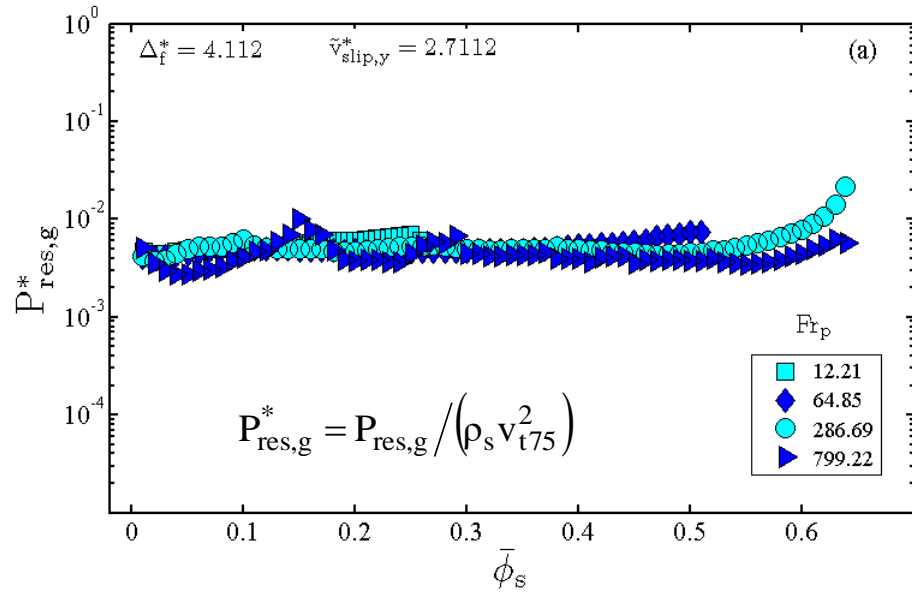
$$\Delta_f^* = \Delta_f / (v_{t75}^2 / g)$$

$$\text{Fr}_p = v_t^2 / (gd_p)$$











Conclusions

- Flow heterogeneity grows with decreasing Fr_p (more refined structures; higher local velocity fluctuations)

Causing

- Higher H (higher corrections over homogeneous drag)
- Higher $\mu_{res,s}^*$, $\mu_{res,g}^*$ (velocity fluctuations/kinetic effects overcome collisional effects)
- Lower $P_{fil,s}^*$, $\mu_{fil,s}^*$, $P_{res,s}^*$, $P_{res,g}^*$ (collisional effects overcome velocity fluctuations/kinetic effects)
- As compared to the previous study, the present results show similar qualitative behaviors for all the concerning sub-grid parameters, while quantitative differences were observed in response to dissimilar non-local effects caused by the variety of macro-scale conditions that were practiced.

(refer to companion presentation for proposed sub-grid models)

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Please direct any questions to milioli@sc.usp.br

Thank you very much!

