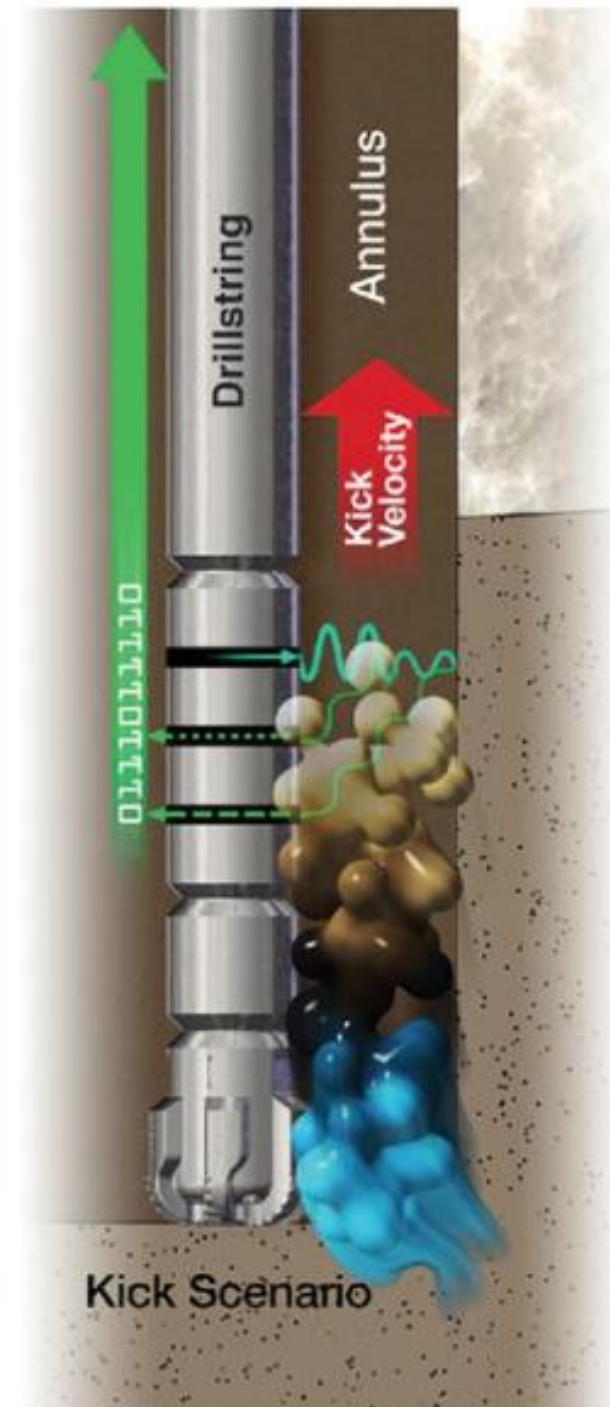


# Computational Modeling of Acoustic-Solid Interaction for Early Kick Detection in Wellbores Using Logging-While-Drilling (LWD) Tools

- 
- **Felipe Maciel (Louisiana State University)**  
fmacie3@lsu.edu
  - Paulo Waltrich (Louisiana State University)
  - Janine Galvin-Carney (NETL)
  - Brian Tost (Oregon State University/NETL-LRST)
  - Brian Fronk (Oregon State University)
  - Foad Haeri (NETL-LRST)

August 2<sup>nd</sup>, 2023



# Motivation: Early Kick Detection (EKD)

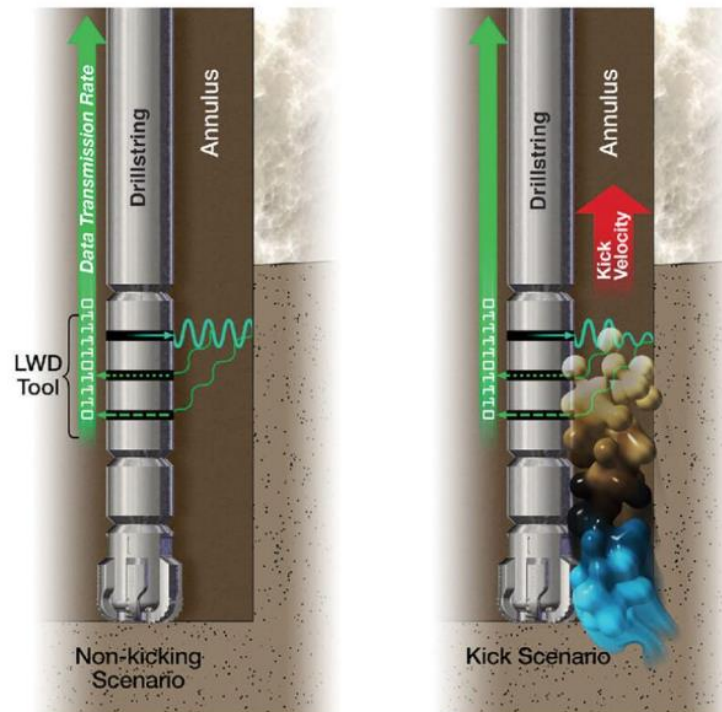
Unexpected gas invasion (kick) into the borehole is a persistent threat during drilling. Traditional kick detection has a significant time lag (hours) and is affected by missed and false detection.

Gas influx can result in a loss of well control and/or blowouts. Accurate Early Kick Detection (EKD) is crucial to improvement in well control safety.



Deepwater Horizon explosion in Louisiana's Gulf of Mexico on April 20, 2010 (Photo: US coast guard)

The suggested method for **Early Kick Detection (EKD)** involves utilizing geophysical signals from **Logging-While-Drilling (LWD)** sensors, enabling real-time detection within minutes<sup>2,3</sup>.



- Field and laboratory data are scarce and not easily accessible.
- Unlocking Valuable Data in Wellbore Dynamics
- Produce a comprehensive multiphase flow dataset to support advanced EKD

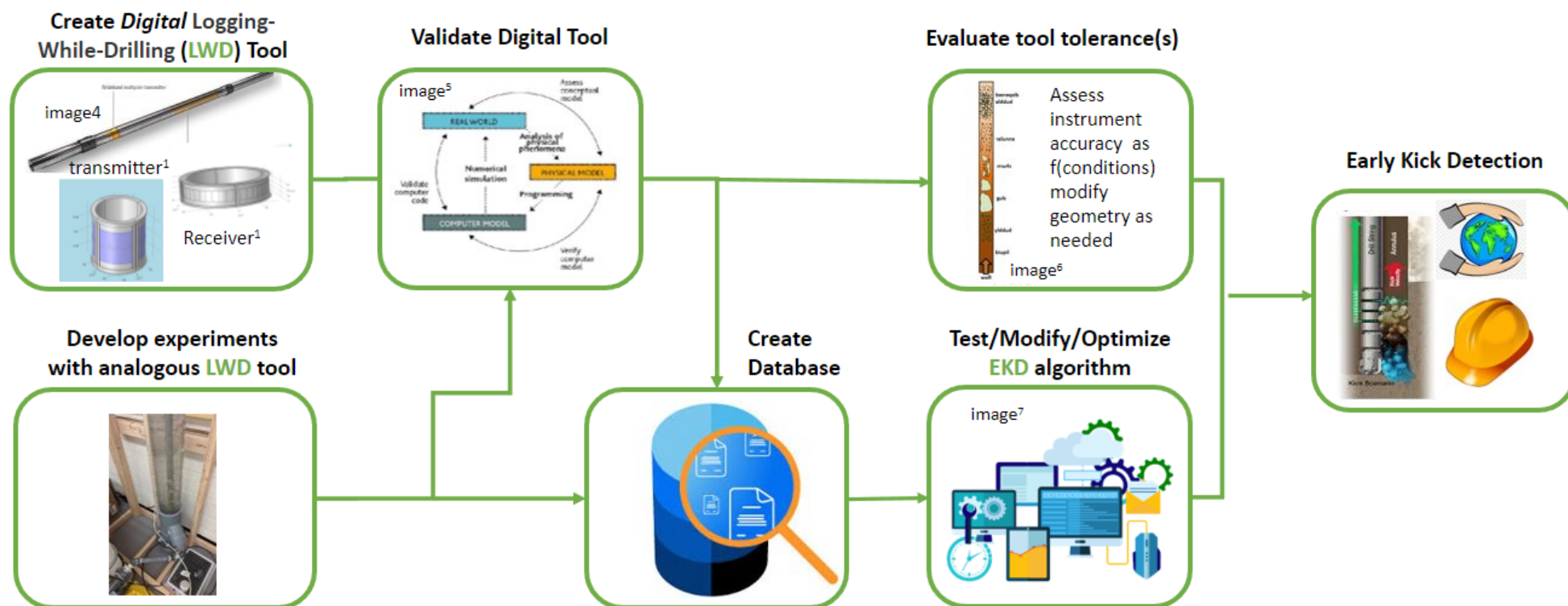
2) Rose, K., et. al., 2019, USPO #10253620;

3) Adapted from Tost, B., et. al., 2016,

<https://doi.org/10.2172/1327810>

# Method Overview / Objectives

- The main methodology is based on combining experimental and numerical acoustic simulation to generate synthetic data and develop an EKD algorithm.
- Produce synthetic data** to help fill the knowledge gap and to aid in Early Kick Detection (EKD) algorithm development



1) Jiang, et al., *Proceedings of the 2014 COMSOL Conference in Boston*, Understanding Logging-While-Drilling Transducers with COMSOL Multiphysics® Software; 4) Alford, et al., *Oilfield Review* Spring 2012: 24, no. 1.; 5) Lapuerta, C., et al., *Nuclear Eng. And Design*, 2012, 253, <https://doi.org/10.1016/j.nucengdes.2011.09.068>; 6) Unalmis, O. H., 2015, doi: 10.1121/2.0000069; 7) web: Custom Advisory Group <http://www.customeradvisorygroup.com/grc---process-control-implimentations.html>

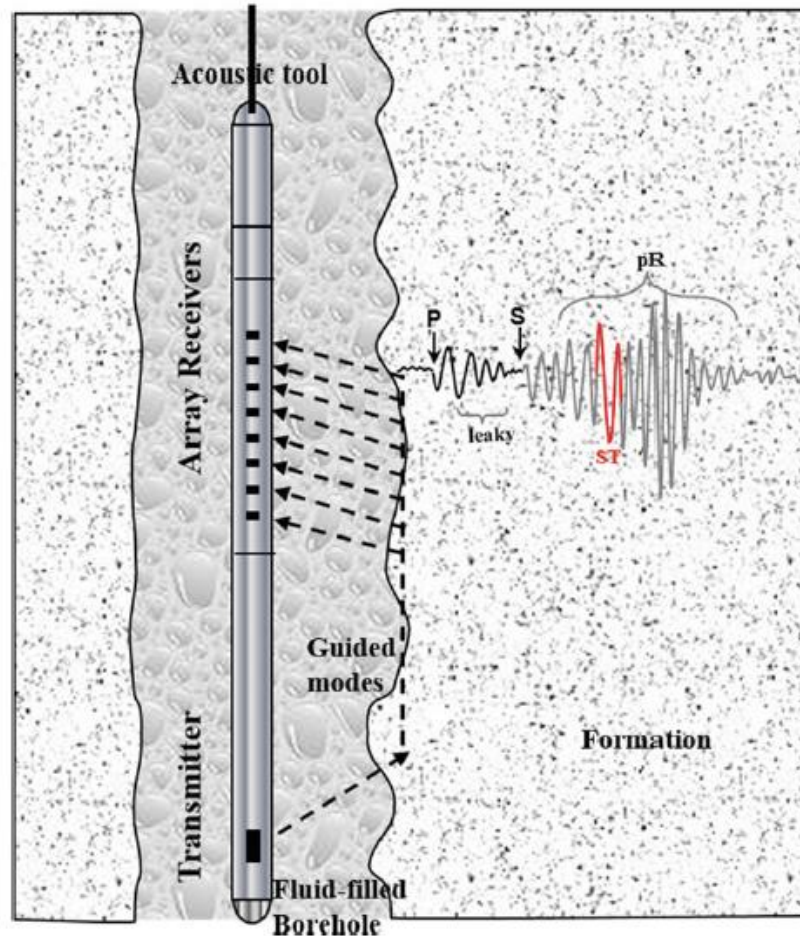
# Wellbore Acoustic Modeling

LWD Sonic tool sends a signal

The acoustic wave travels through the fluid to the rock.

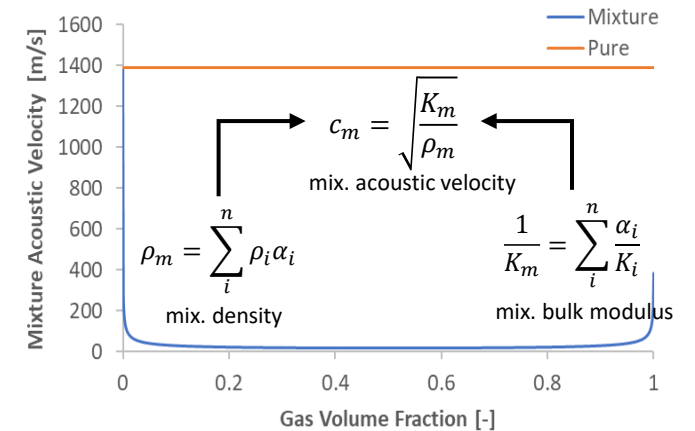
Acoustic waves traveling through the fluid to transmitters

Acoustic waves traveling from the rock back to the fluid and to the receiver



Sonic Logging: Illustration of acoustic logging with a source (transmitter) and an array of receivers. 9

Literature review and numerical analysis show promising results for early kick detection via **LWD and acoustic methods**. Sonic signals are sensitive to variations of gas fraction bringing up the potential of using LWD and acoustic methods for early kick detection.



# Computational Acoustic: Pressure Acoustics (Fluid)

## Modeling Sound Wave propagation

General Scalar Wave Equation (GSWE): Simulation of custom acoustic propagation.

$$\frac{1}{\rho c^2} \frac{\partial^2 p_t}{\partial t^2} + \nabla \cdot \left( -\frac{1}{\rho} (\nabla p_t - \mathbf{q}_d) \right) = Q_m$$

- Describes small acoustic pressure variations ( $p_t$ )
- Accommodates monopole ( $Q_m$ ) and dipole sources ( $\mathbf{q}_d$ )
- Flexibility to incorporate fluid-solid interactions -> different modes of propagation

### Current simplifications/challenges:

- Resonance effects are neglected
- Interphase (mass/momentum) transfer is neglected

COMSOL  
MULTIPHYSICS®

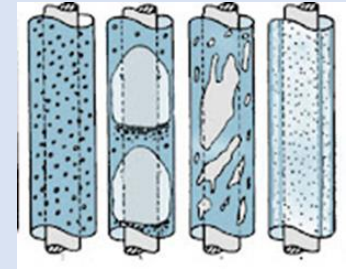
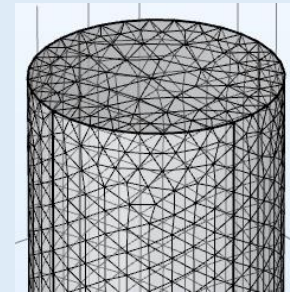


## Modeling Two-Phase Medium:

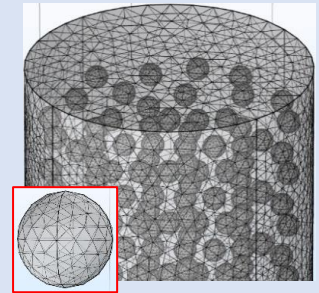
Two-phase gas-liquid mixtures may be expected in the event of a gas kick

- 1) Homogenized model using a mixture approximation (Wood's Equation):

$$\frac{1}{c_{mix}^2} = (\alpha_g \rho_g + \alpha_l \rho_l) \left( \frac{\alpha_l}{\rho_l c_l^2} + \frac{\alpha_g}{\rho_g c_g^2} \right)$$



- 2) Discrete bubble approach



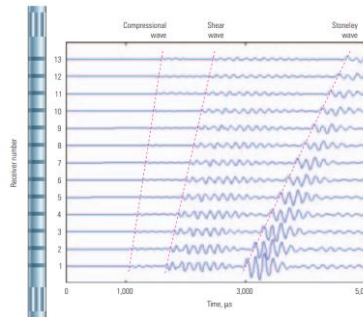
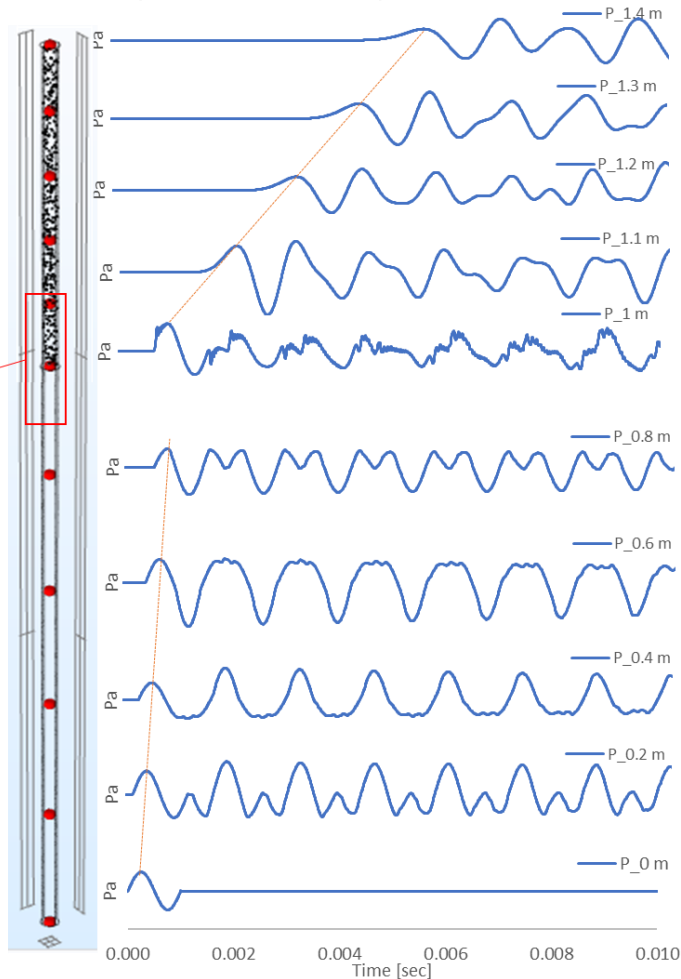
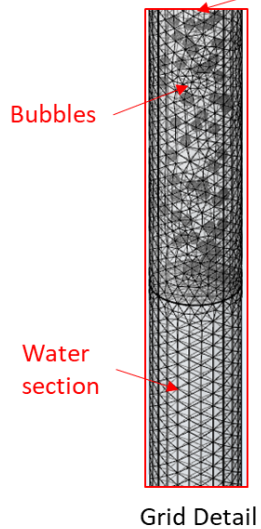
- + Does not require a mixture model
- + Allows for scattering
- Computationally expensive

# Computational Acoustic: Pressure Acoustics (Fluid)

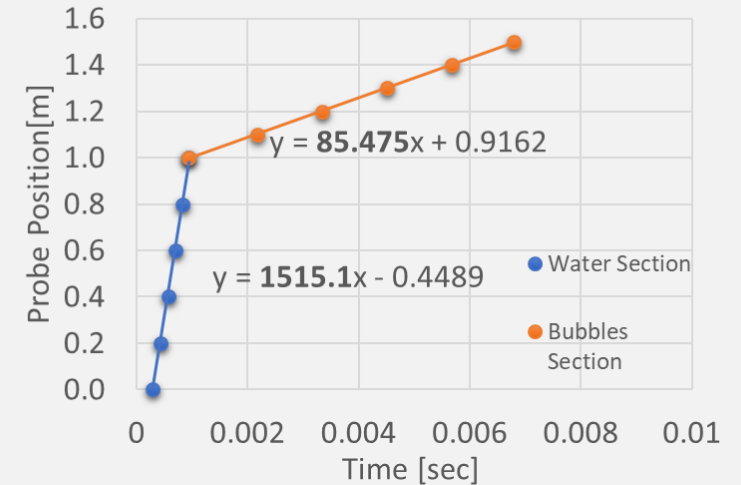
## Wave Propagation in a Wellbore

Water and Multiphase Section (2% Void fraction)

**Pipe:**  
 $D_{\text{pipe}} = 0.025 \text{ m}$   
 $H_{\text{pipe}} = 1 \text{ m}$   
**Random Bubbles**  
 $D_{\text{bubble}} = 3 \text{ mm}$   
 Void Fraction = 2 %  
**Signal:**  
 Frequency = 1 kHz  
 Amplitude = 10 Pa



Speed of sound analysis: First peak arrival at probes



Input data:

Gas fraction = 2 %  
 $c_{\text{water}} = 1480 \text{ m/s}$   
 $c_{\text{air}} = 343 \text{ m/s}$  (bubbles)  
 Signal freq = 1000 Hz

COMSOL Results:

$c_{\text{water}} = 1515.1 \text{ m/s}$   
 $c_{\text{mix}} = 85.47 \text{ m/s}$

Analytic for  $\alpha = 2\%$

$c_{\text{mix-Wood's}} = 85.6 \text{ m/s}$   
 Error of  $c_{\text{water}}$  2.4% and  $c_{\text{mix}}$  0.15%

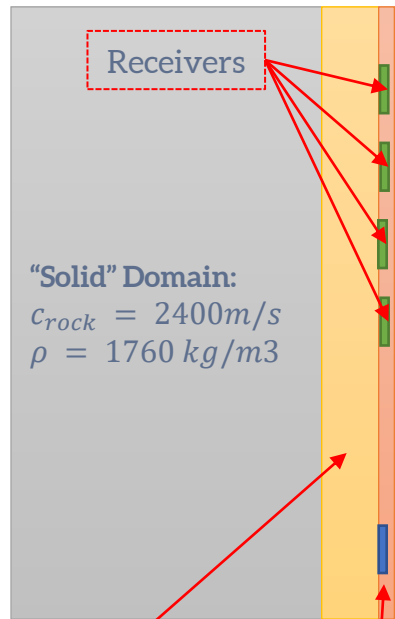
**A similar speed of sound to the water and the effective mixture model is predicted**

# Computational Acoustic: Pressure Acoustics (Fluid)

## Wave Propagation in Wellbore

Pressure acoustic model considering density and speed of sound like the rock formation and a wellbore fluid of around **0.15 % gas fraction**.

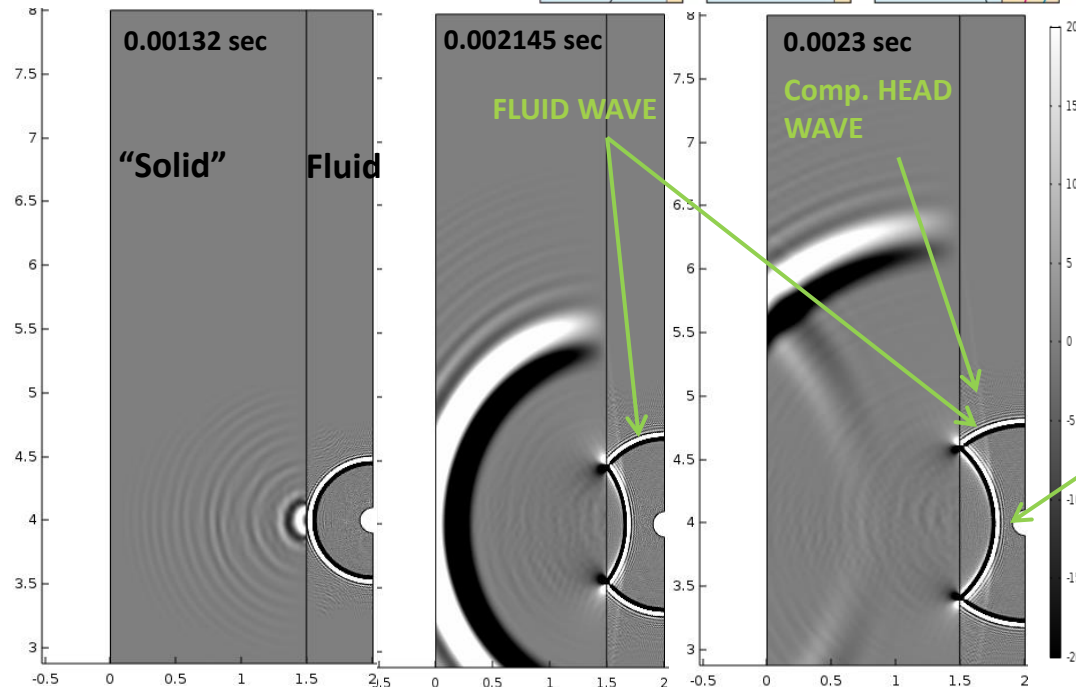
*No solid mechanics modeling is involved.*



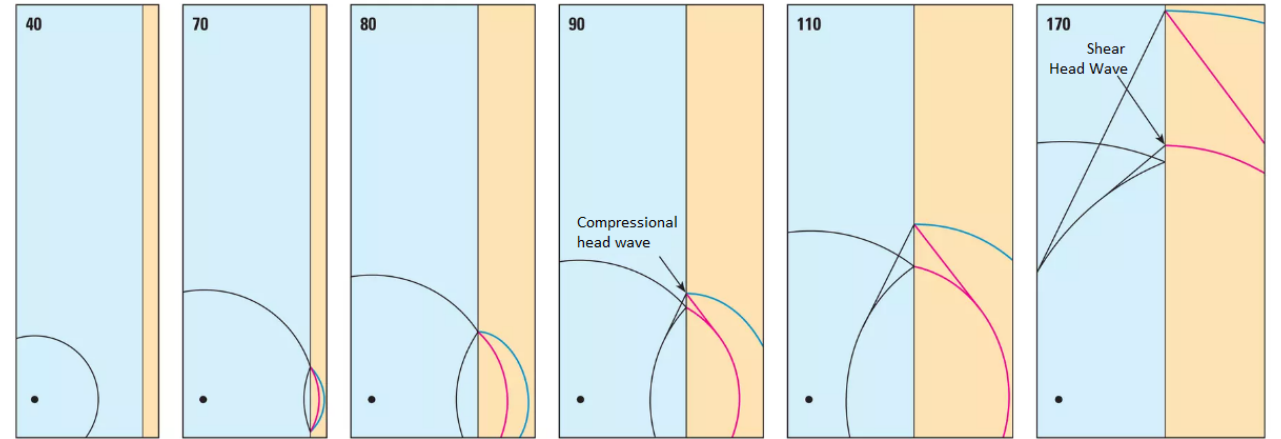
**"Solid" Domain:**  
 $c_{rock} = 2400\text{m/s}$   
 $\rho = 1760\text{ kg/m}^3$

**Wellbore fluids**  
 $c_{fluid} = 300\text{ m/s}$   
 $\rho_{fluid} = 1000\text{ kg/m}^3$

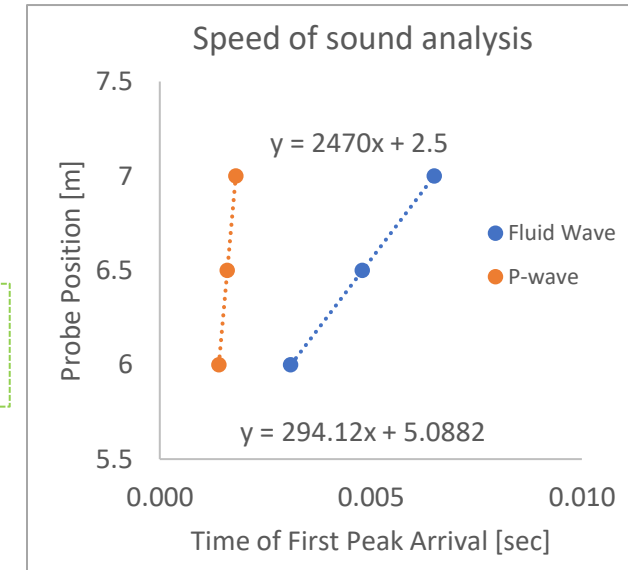
Acoustic Source



Acoustic Pressure Source:  $f = 5\text{KHz}$



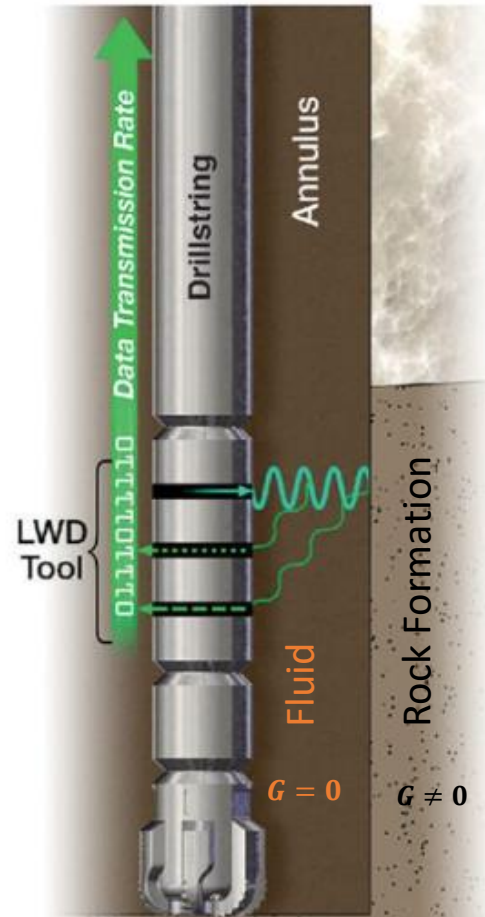
(10)



# Computational Acoustics: Solid Mechanics (Solid)

Wave propagation in a through depends on solid mechanical Mechanical Properties

- Elastic waves in rocks propagate with a velocity that is given by elastic stiffnesses and the density ( $\rho$ ) of the solid material. (Fjær et al, 2008)
- Speed of sound of compressional wave ( $c_p$ ) and shear wave ( $c_s$ ) are defined based on the mechanical properties



Speed of sound of compressional Wave (p-wave)

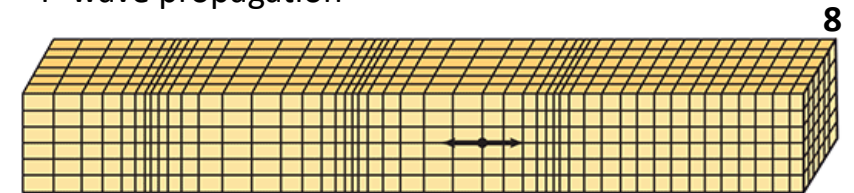
$$c_p = \sqrt{\left(K + \frac{4}{3}G\right)/\rho}$$

Speed of sound of Shear Wave (s-wave)

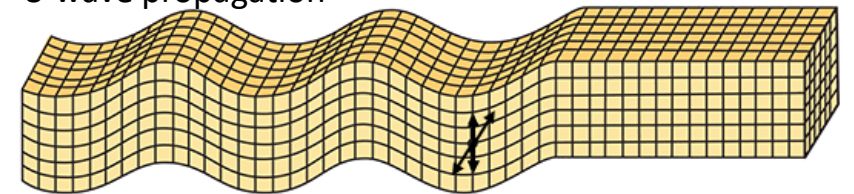
$$c_s = \sqrt{G/\rho}$$

G: Shear Modulus  
K: Bulk Modulus  
 $\rho$ : Density

P-wave propagation

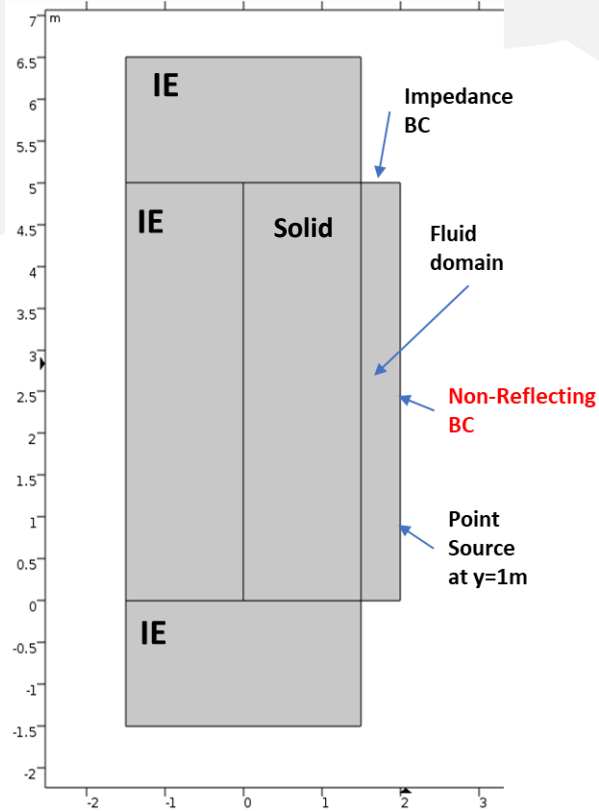


S-wave propagation





# Wave Propagation in Wellbore: Multiphysics

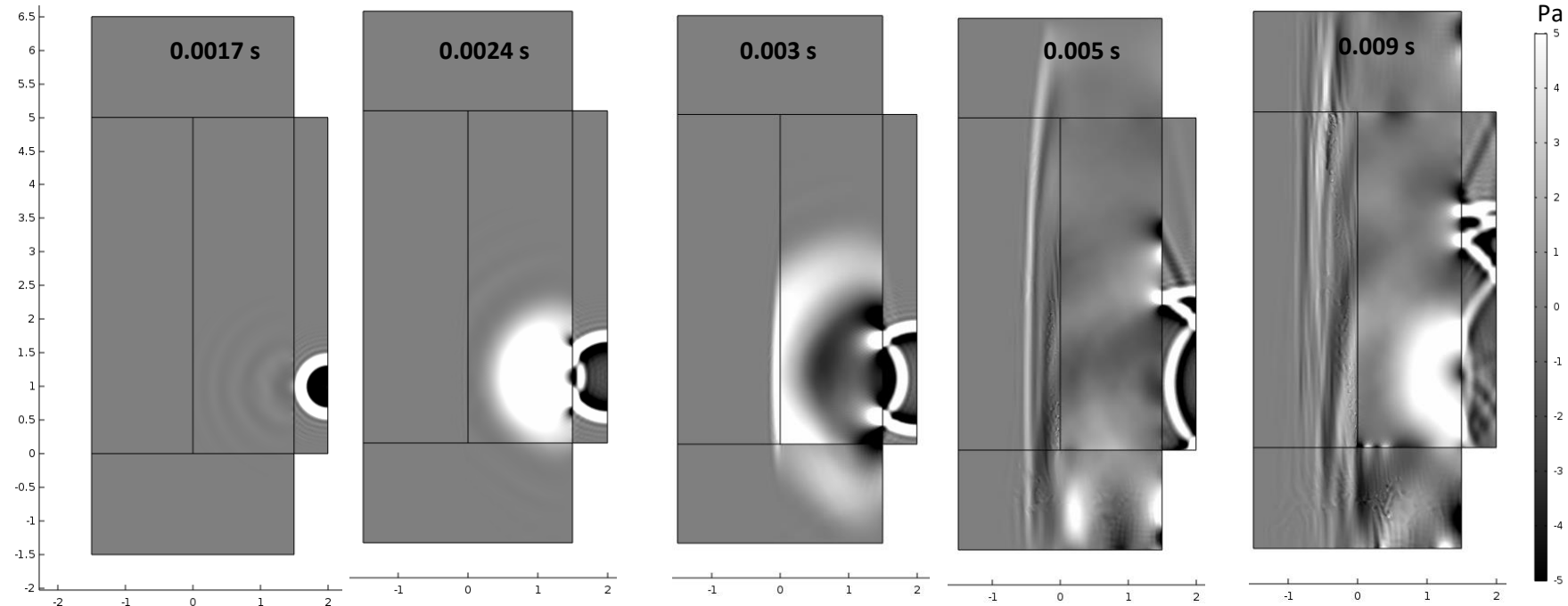


**Fluid Domain**  
 $\rho = 1000 \text{ kg/m}^3$   
 $c = 300 \text{ m/s}$   
 $L_x = 0.5 \text{ m}$   
 $L_y = 5 \text{ m}$

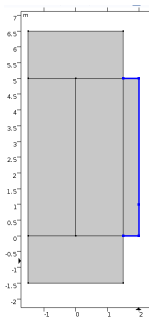
**Rock**  
 $\rho = 1760 \text{ kg/m}^3$   
 $c_{comp} = 1880 \text{ m/s}$   
 $c_{shear} = 767 \text{ m/s}$   
 $L_x = 1.5 \text{ m}$   
 $L_y = 5 \text{ m}$

## Multiphysics: Pressure Acoustics + Solid Mechanics

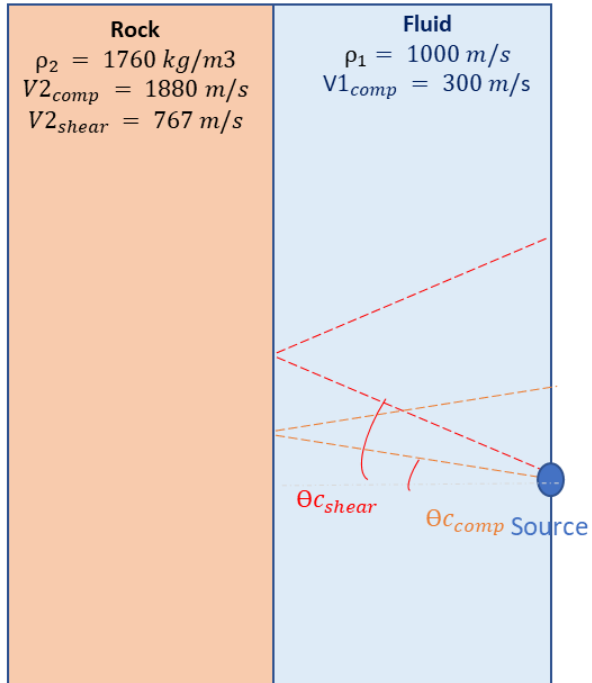
Transient evolution of acoustic wave propagation



# Wave Propagation in Wellbore: Multiphysics



## Critical angles ( $\theta_c$ ) validation: Compressional and shear waves

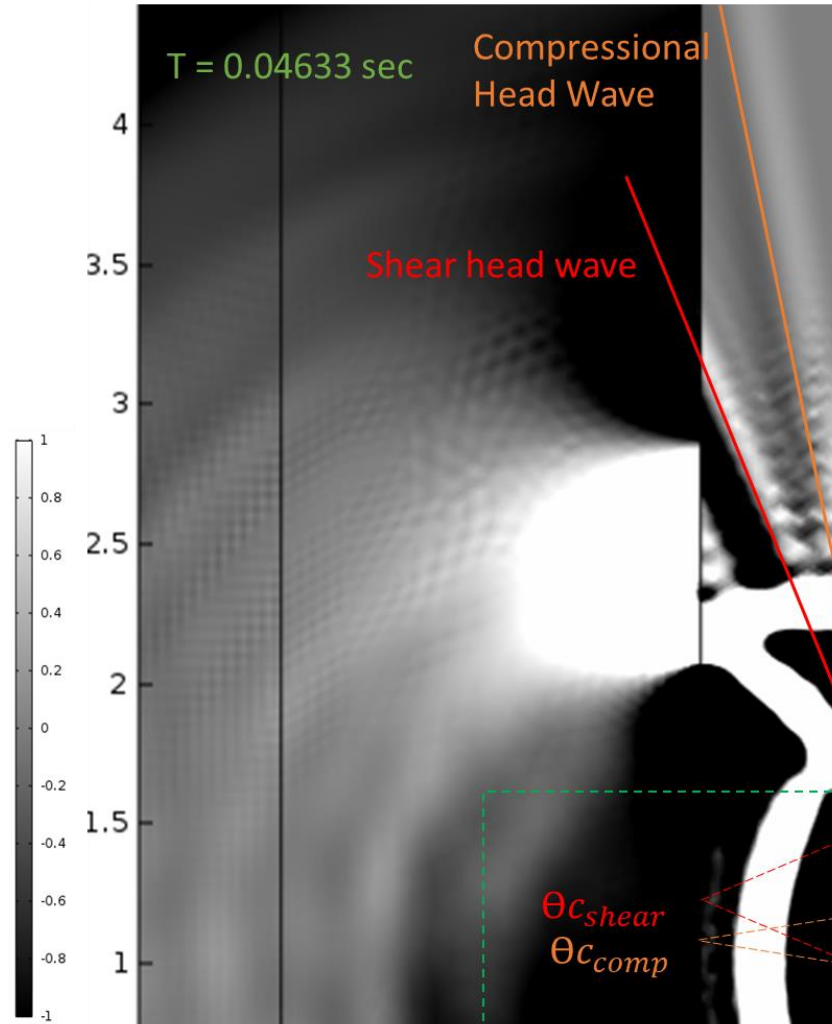


### Compressional Wave

- $\theta_{C_{comp}} = \arcsin(V_{1_{comp}}/V_{2_{comp}})$
- $\theta_{C_{comp}} = \arcsin(300/1880)$
- $\theta_{C_{comp}} = 9.18$

### Shear Wave

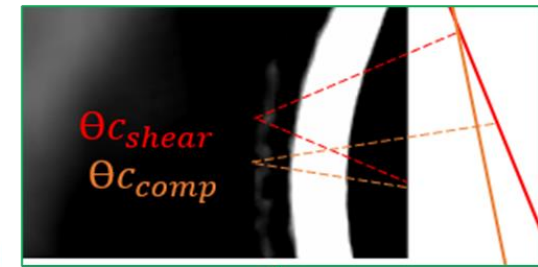
- $\theta_{C_{shear}} = \arcsin(V_{1_{comp}}/V_{2_{shear}})$
- $\theta_{C_{shear}} = \arcsin(300/767)$
- $\theta_{C_{shear}} = 23.02$



Critical Angles Representation  
compressional head waves and shear head waves are visible at this specific instant of time.

$\theta_{C_{comp}} = 9.182$   
 $\theta_{C_{shear}} = 23.02$

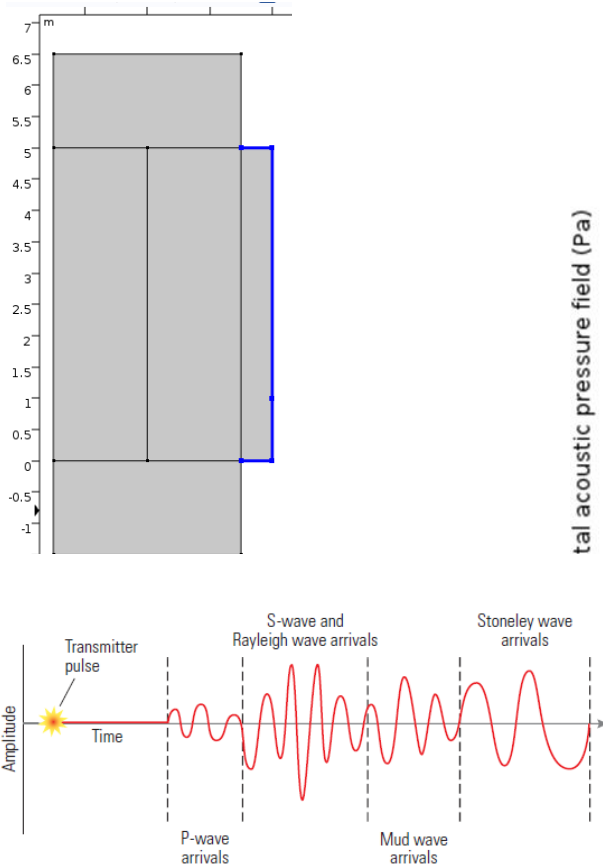
For angles of incidence larger than  $\theta_c$ , the sound wave is completely reflected out or at least refracted to 90 degrees creating a surface wave.



**\*\*The model can accurately predict the critical angles for both p-wave and s-wave**

# Wave Propagation in Wellbore: Multiphysics

## Wave Propagation in Wellbore



Head wave compressional  
 $t_{Hcomp} \text{ (sec)} = 0.005136 \text{ @4m}$   
 $t_{Hcomp} \text{ (sec)} = 0.0054 \text{ @4.5m}$

Shear Head wave  
 $t_{Hshear} \text{ (sec)} = 0.00723 \text{ @4m}$   
 $t_{Hshear} \text{ (sec)} = 0.00788 \text{ @4.5m}$

Direct Arrivals  
 $t_{Dm} \text{ (sec)} = 0.01025 \text{ @4m}$   
 $t_{Dm} \text{ (sec)} = 0.01192 \text{ @4.5m}$

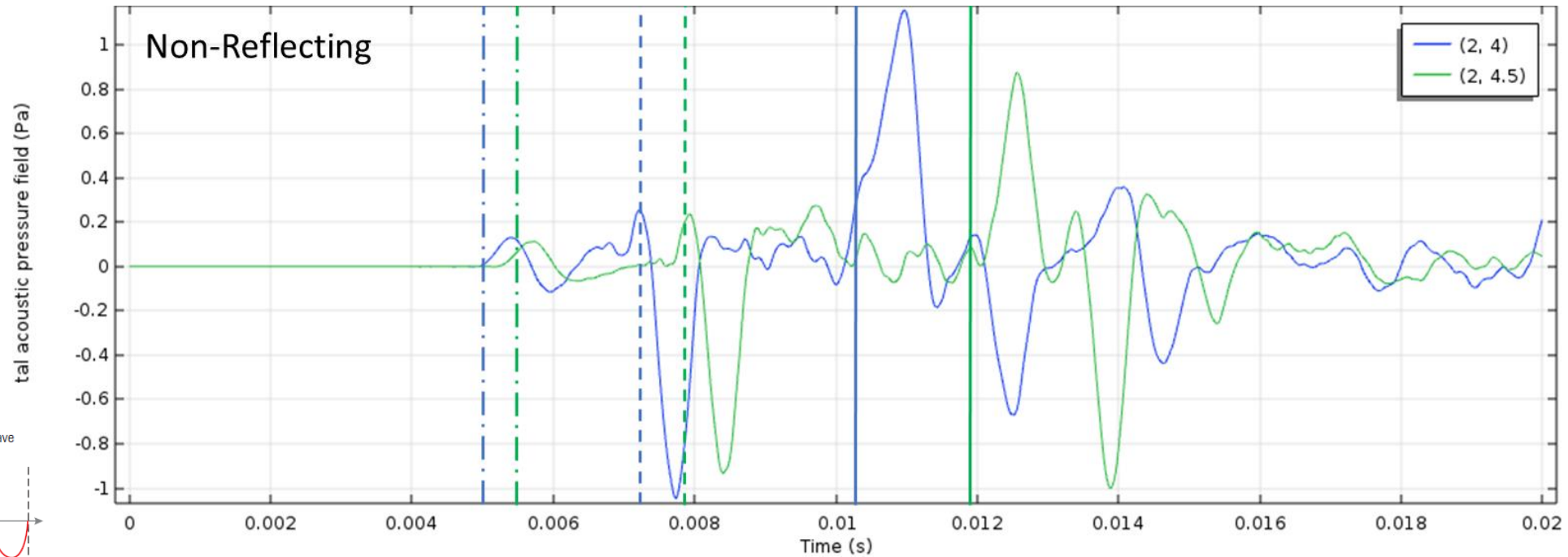
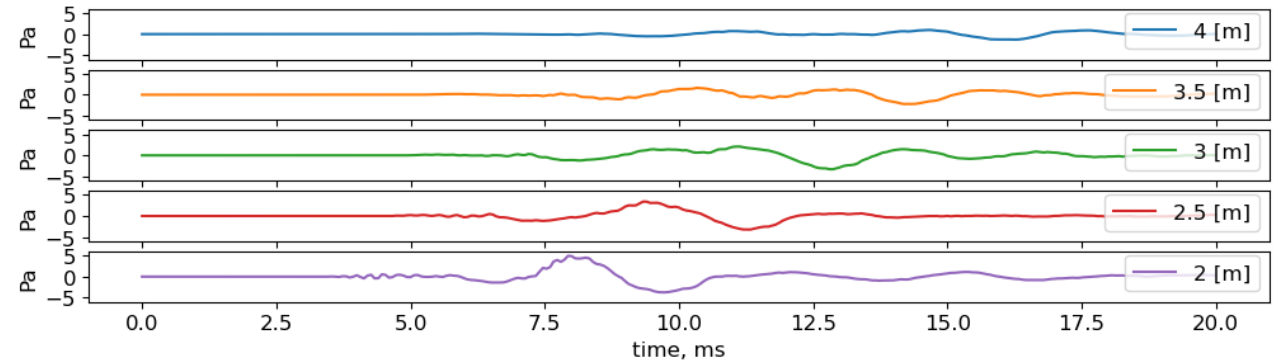
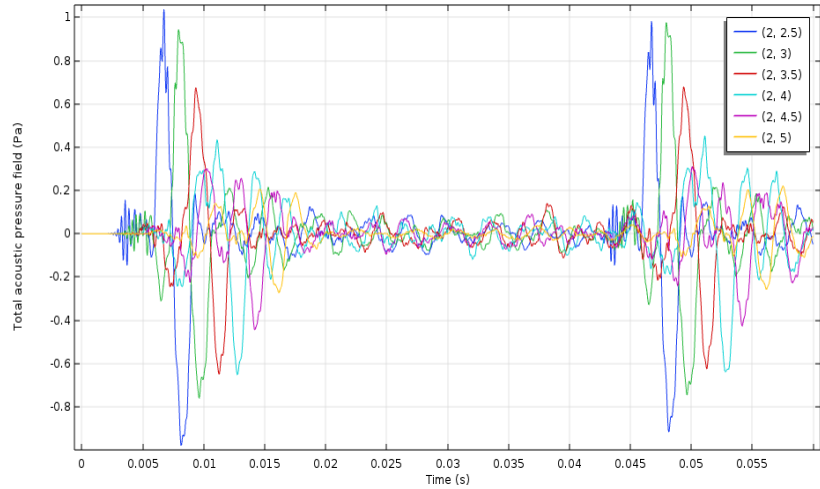
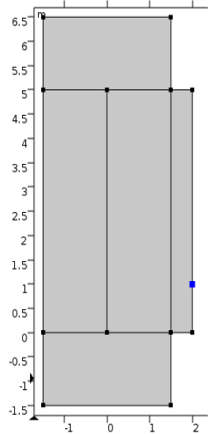


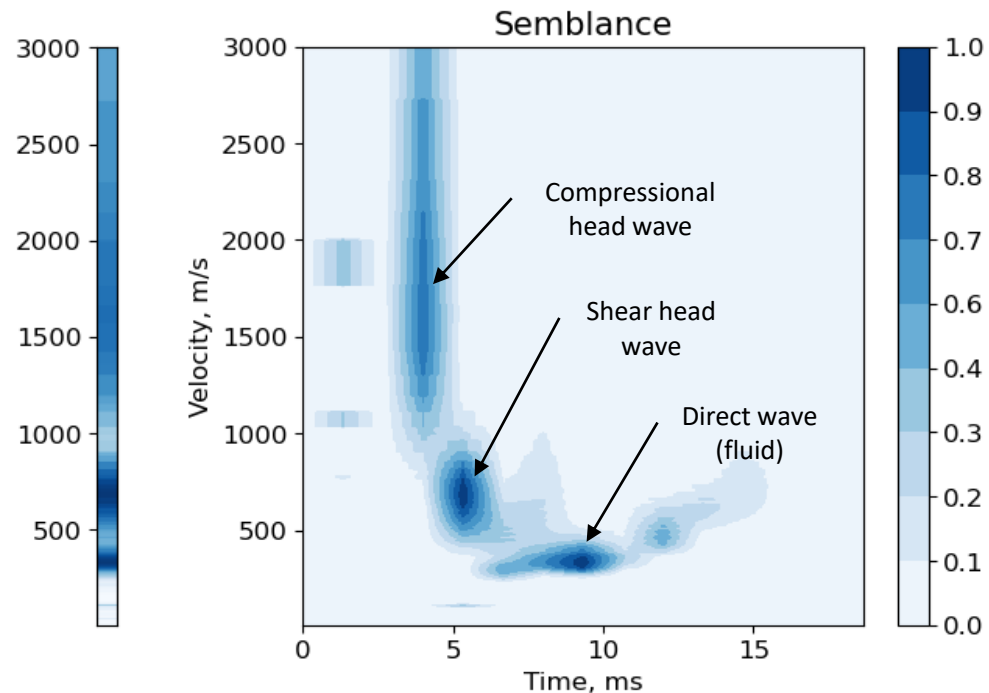
Image from<sup>4</sup>

# Signal Analysis/Algorithm Development



**Simulation:**  
F0 = 300Hz  
Monopole Source Amplitude = 10 Pa

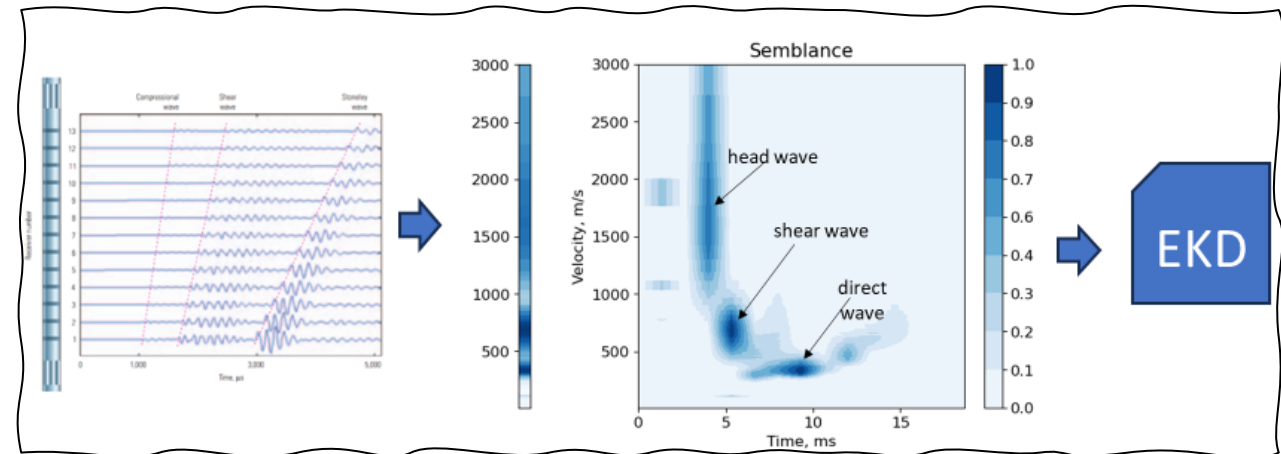
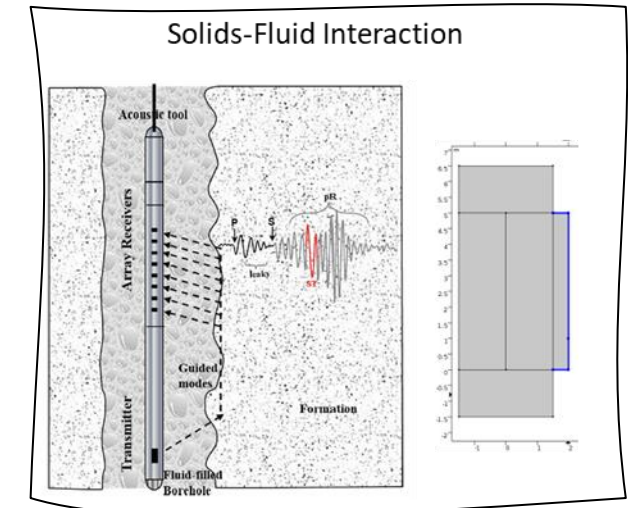
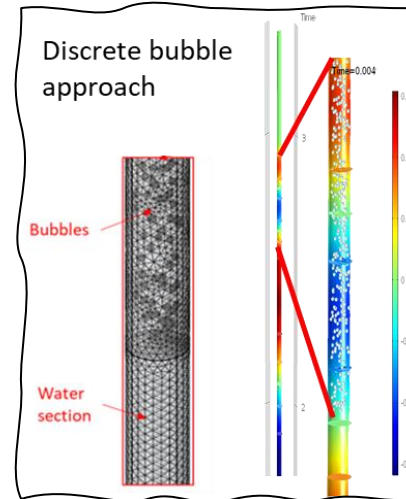
Compressional head wave:  $c_p = 1880$  m/s  
Shear head wave:  $c_s = 767$  m/s  
Direct mud wave:  $c_{fluid} = 300$  m/s



**Semblance Plot:**  
Conventional methods to automate, visually, and identify the propagation modes.

# Final Remarks / Next Steps

- The model can accurately predict the speed of sound of p-wave and s-wave
- Continue to Explore Solids-Fluid Interaction Component
  - Can we identify and use the stoneley wave to detect changes in the fluid gas fraction
- Discrete bubble approach
  - Investigate how the bubble mixture as opposed to homogenous mixture impacts wave train
- Automate data analysis method (identifying a kick)
  - Signal analysis/machine learning techniques
  - Can we identify a kick using the wave train?



# Acknowledgements

---

- Louisiana State University
- National Energy Technology Laboratory
- Oregon State University



# Questions?

**Felipe Maciel**

**Research Associate, Louisiana  
State University**

**Email me at: [fmacie3@lsu.edu](mailto:fmacie3@lsu.edu)**

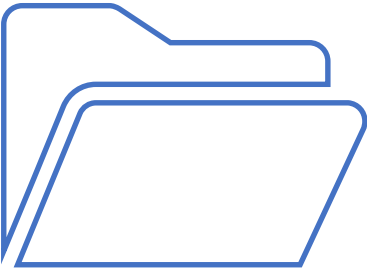


# References

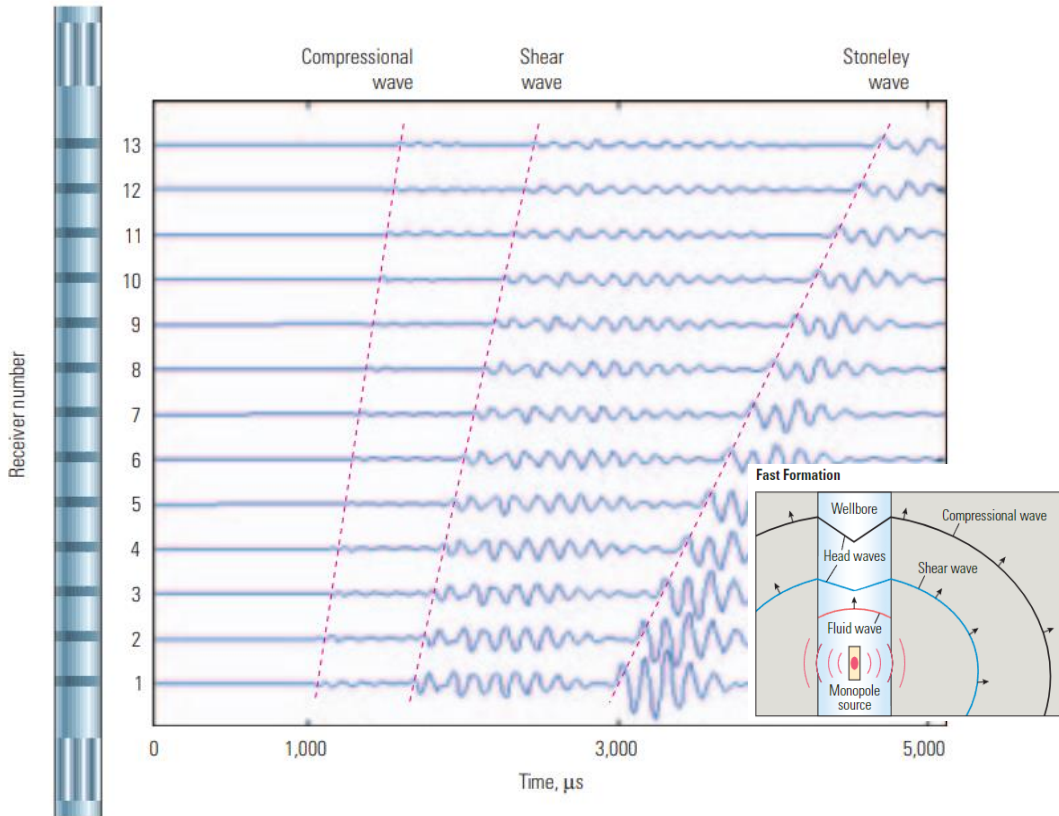
- 1) Jiang, et al., Proceedings of the 2014 COMSOL Conference in Boston, Understanding Logging-While-Drilling Transducers with COMSOL Multiphysics® Software;
- 2) Rose, K., et. al., 2019, USPO #10253620;
- 3) Adapted from Tost, B., et. al., 2016, <https://doi.org/10.2172/1327810>
- 4) Alford, et al., Oilfield Review Spring 2012: 24, no. 1.;
- 5) Lapuerta, C., et al., Nuclear Eng. And Design, 2012, 253, <https://doi.org/10.1016/j.nucengdes.2011.09.068>;
- 6) Unalmis, O. H., 2015, doi: 10.1121/2.0000069;
- 7) web: Custom Advisory Group [http://www.customeradvisorygroup.com/grc---process-control-  
implementations.html](http://www.customeradvisorygroup.com/grc---process-control-implementations.html)
- 8) Peterie, Shelby L., Richard D. Miller, and Julian Ivanov. "Seismology and its applications in Kansas." *Kansas: Kansas Geological Survey* (2014).
- 9) Wang et al. Bottomhole Acoustic Logging. <https://doi.org/10.1007/978-3-030-51423-5>
- 10) Haldorsen et al., Borehole Acoustics. Ridgefield, Connecticut, USA. 2006



Backup Slides

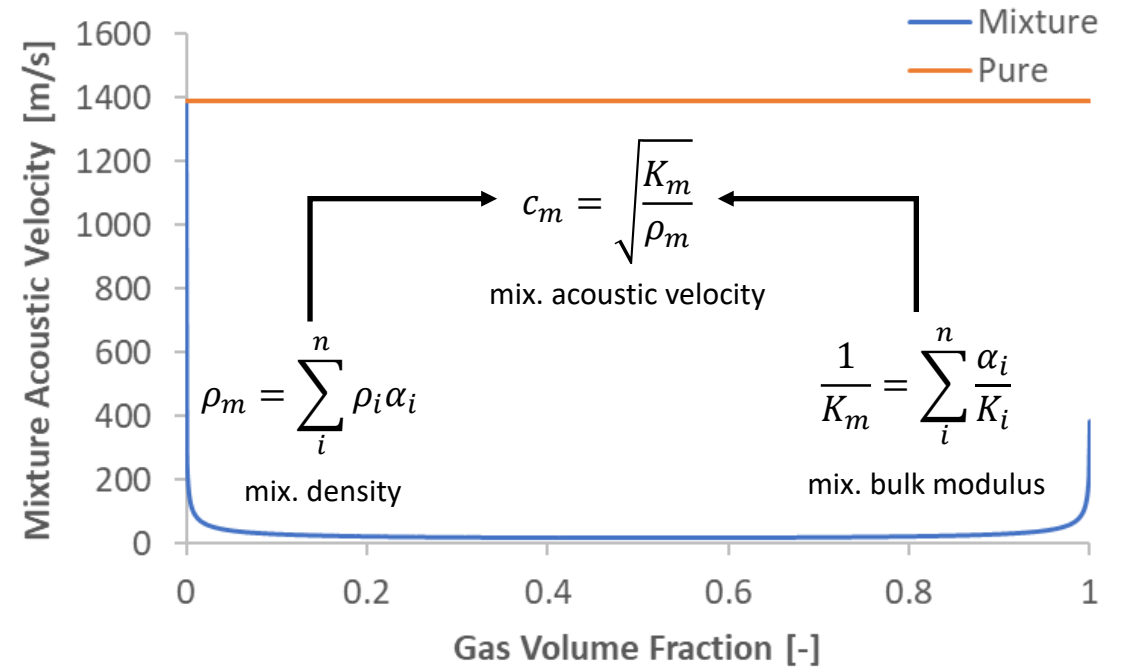


# Acoustic Velocity: Logging While Drilling



Typical waveforms from LWD signal in a fast formation showing compressional, shear, and Stoneley waves. (Haldirsen et al, 2006)

Literature review and numerical analysis show promising results for early kick detection via **LWD and acoustic methods**



Sonic signals are sensitive to variations of gas fraction bringing up the potential of using LWD and acoustic methods for early kick detection.

# Computational Acoustic: Pressure Acoustics (Fluid)

- Modeling Sound Wave propagation: The General Scalar Wave Equation (GSWE) allows simulation of custom acoustic properties:

$$\frac{1}{\rho c^2} \frac{\partial^2 p_t}{\partial t^2} + \nabla \cdot \left( -\frac{1}{\rho} (\nabla p_t - \mathbf{q}_d) \right) = Q_m$$

- Describes small acoustic pressure variations ( $p_t$ )
- Accommodates monopole ( $Q_m$ ) and dipole sources ( $\mathbf{q}_d$ )
- Flexibility to incorporate fluid-solid interactions -> different modes of propagation

*In a gas kick event, two-phase mixtures are expected.*

Wood's 1989 Equation: Mixture Speed of Sound

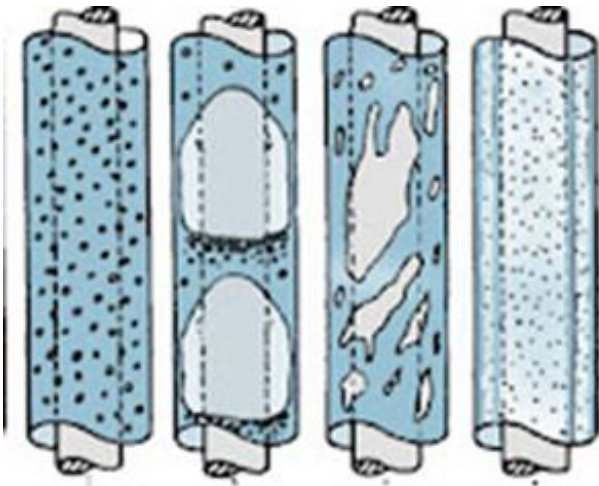
( $l$  and  $g$  denote liquid and gas respectively)

$$\frac{1}{c_{mix}^2} = (\alpha_g \rho_g + \alpha_l \rho_l) \left( \frac{\alpha_l}{\rho_l c_l^2} + \frac{\alpha_g}{\rho_g c_g^2} \right)$$

# Computational Acoustic: Pressure Acoustics (Fluid)

## Modeling Two-Phase Medium:

Two-phase gas-liquid mixtures may be expected in the event of a gas kick

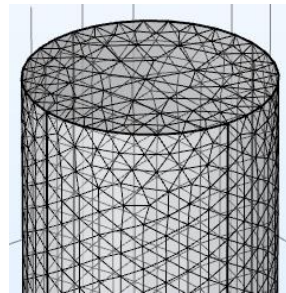


### Current simplifications/challenges:

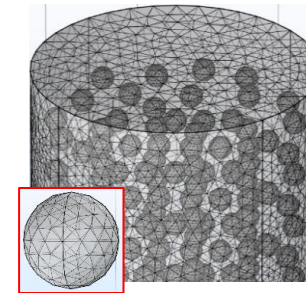
- Resonance effects are neglected
- Interphase (mass/momentum) transfer is neglected

- Homogenized model using a mixture approximation (Wood's Equation):

$$\frac{1}{c_{mix}^2} = (\alpha_g \rho_g + \alpha_l \rho_l) \left( \frac{\alpha_l}{\rho_l c_l^2} + \frac{\alpha_g}{\rho_g c_g^2} \right)$$

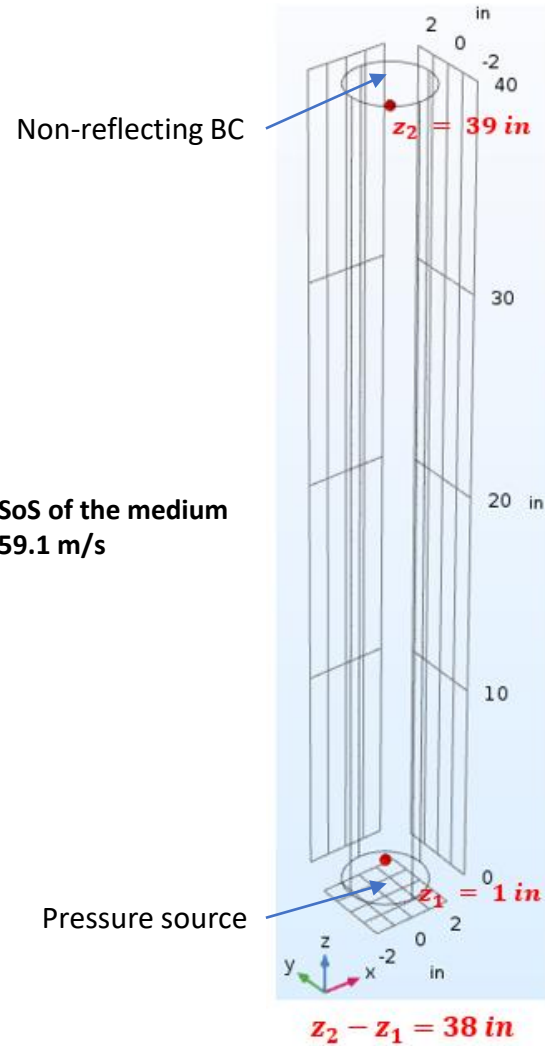
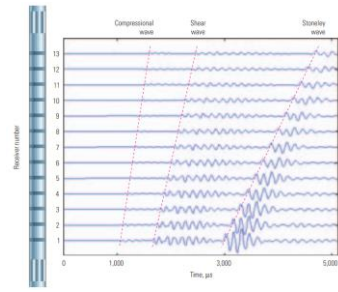


- Discrete bubble approach



- + Does not require a mixture model
- + Allows for scattering
- Computationally expensive

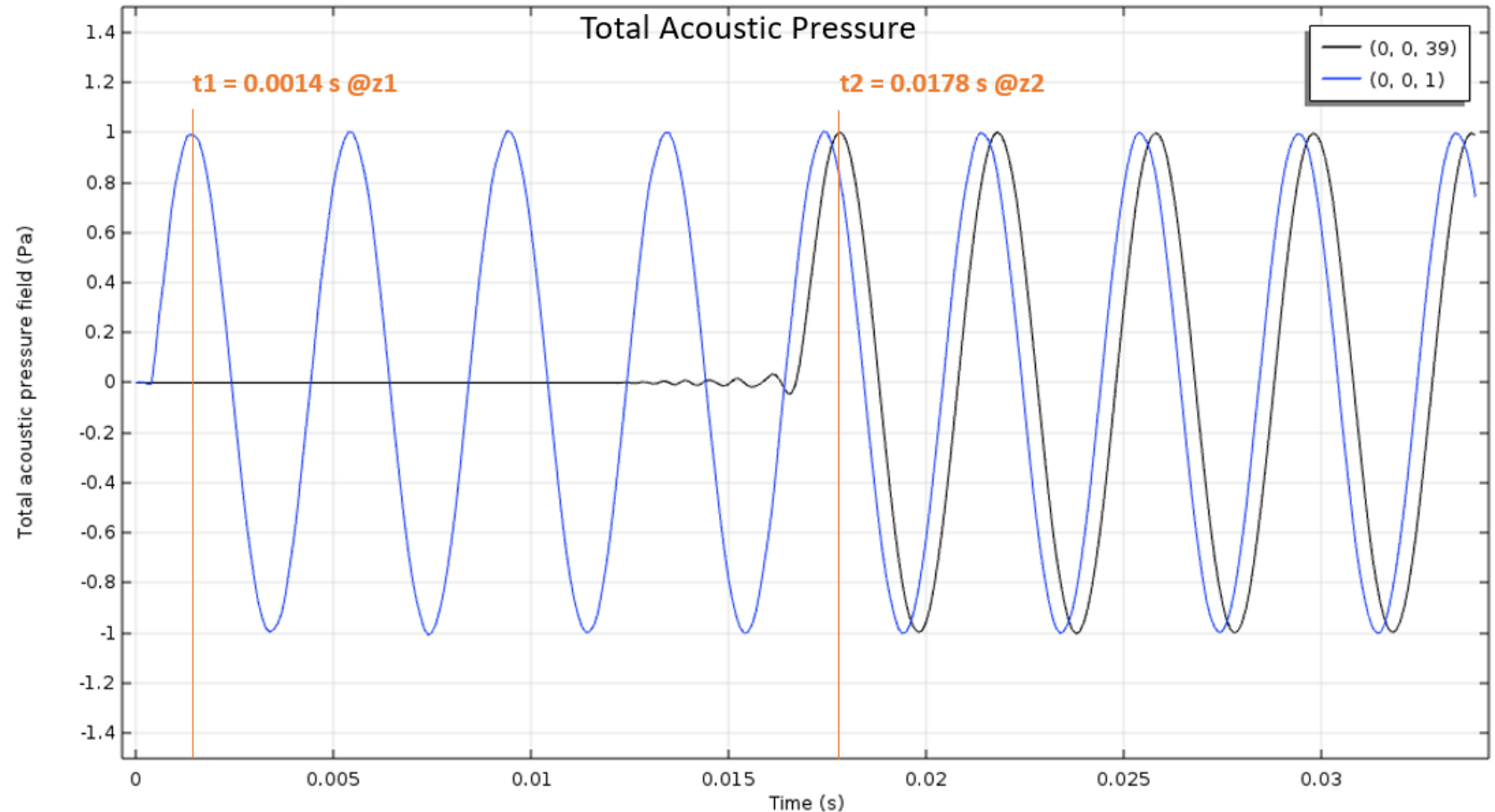
# Speed of Sound (SoS) Determination



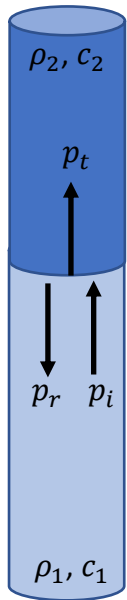
Calculated Speed of Sound (SoS) using signal arrival time at distinct probe locations

$$\text{SoS} = (39-1)[\text{in}] * 0.02549[\text{m/in}] / (0.0178 - 0.0014)[\text{s}]$$

$$\text{SoS} = 59.06 \text{ m/s}$$



# Reflection & Transmission Validation

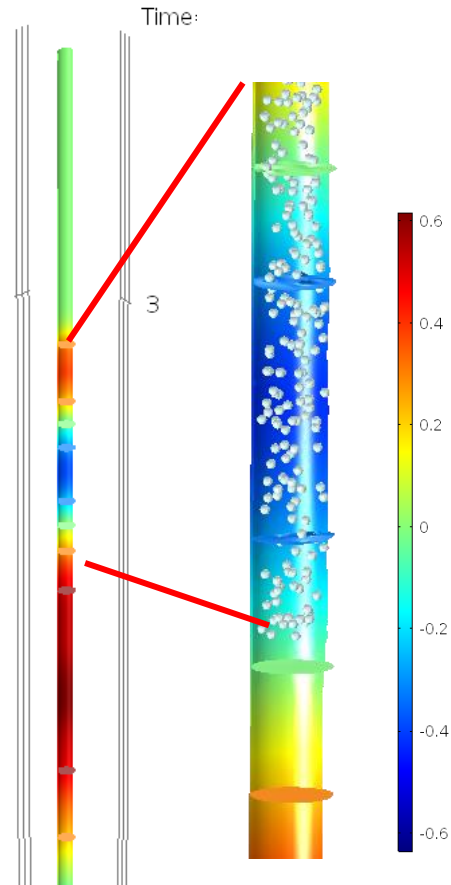


## Analytic Model

$$Z_i = \rho_i c_i$$

$$R_{12} = \frac{Z_2 - Z_1}{Z_2 + Z_1}$$

$$T_{12} = 1 + R_{12} = \frac{2Z_2}{Z_2 + Z_1}$$



Liquid into Mixture (bubbles)

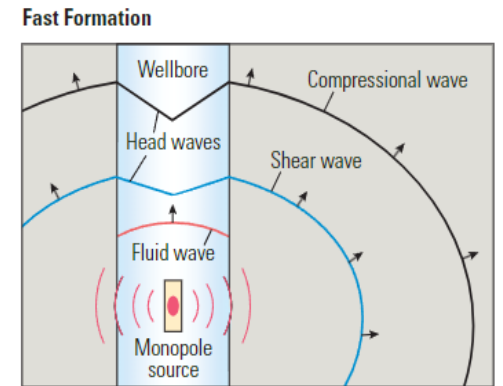
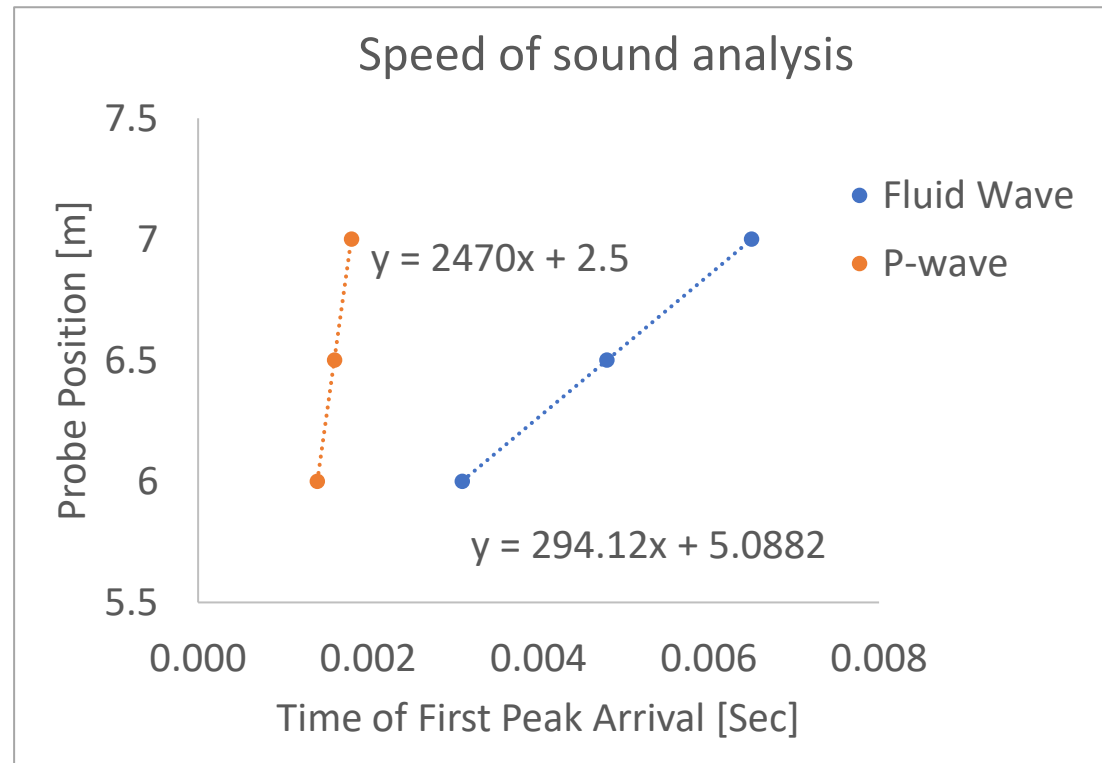
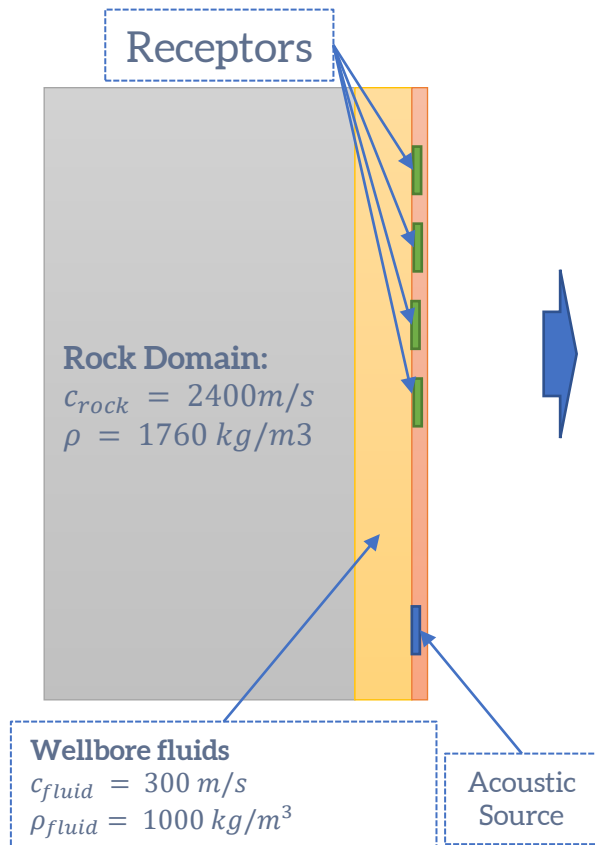
Impedance Ratio ( $Z_2/Z_1$ ) 0.2369

| Approach             | Incident<br>$P_i$ (Pa) | Reflected<br>$P_r$ (Pa) | Transmitted<br>$P_t$ (Pa) | $(P_t - P_r)/P_i$ |
|----------------------|------------------------|-------------------------|---------------------------|-------------------|
| Analytic Model       | 1                      | -0.61695                | 0.383050018               | 1                 |
| Sim. Homogeneous     | 1                      | -0.628                  | 0.38                      | 1.008             |
| Sim. Discrete Bubble | 1                      | -0.605                  | 0.375                     | 0.98              |

- Similar *initial* incident reflected & transmitted pressure amplitudes are predicted
- Agree well with analytic theory

# Wave Propagation in Wellbore: Pressure Acoustics

This simulation consists of a pressure acoustic model considering properties of density and speed of sound similar to the rock formation and a wellbore fluid of around 0.15 % gas fraction. No solid mechanics modeling involved.



# Wave Propagation in Wellbore: Multiphysics

## Multiphysics: Pressure Acoustics + Solid Mechanics

### Fluid Domain

$\rho = 1000 \text{ kg/m}^3$

$c = 300 \text{ m/s}$

$L_x = 0.5 \text{ m}$

$L_y = 5 \text{ m}$

### Rock

$\rho = 1760 \text{ kg/m}^3$

$c_{\text{comp}} = 1880 \text{ m/s}$

$c_{\text{shear}} = 767 \text{ m/s}$

$L_x = 1.5 \text{ m}$

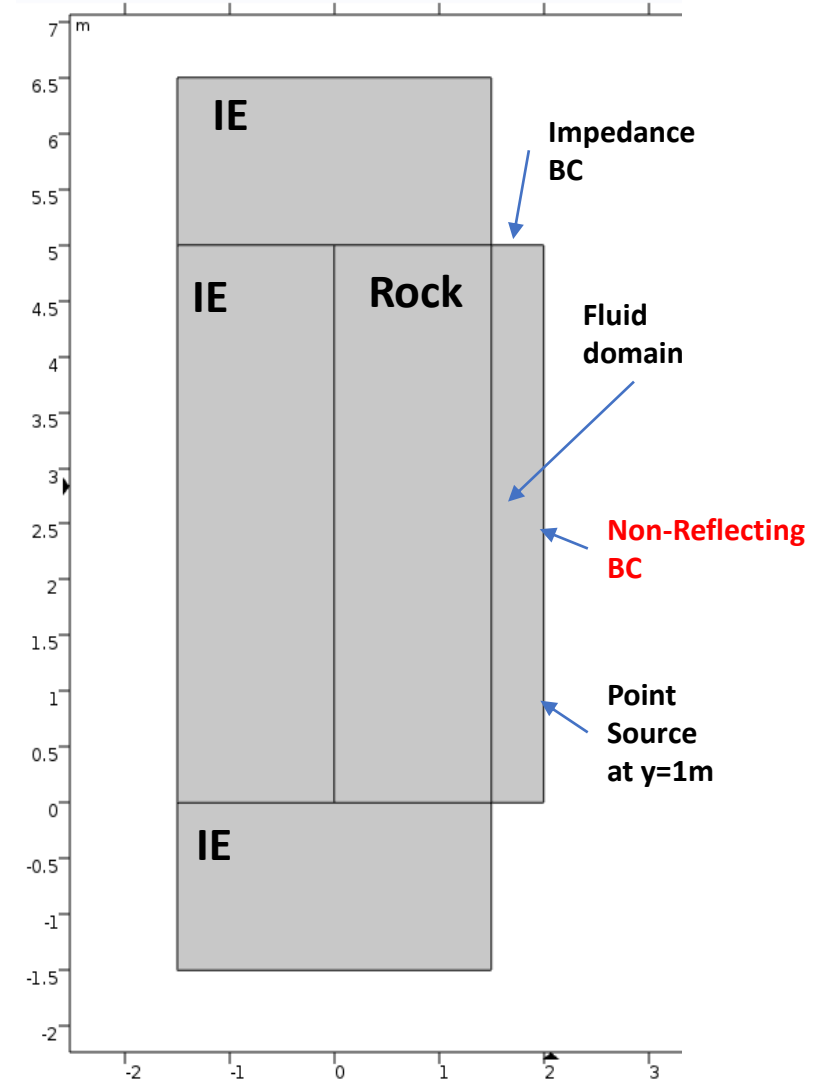
$L_y = 5 \text{ m}$

### Absorbing Domain with (Infinite Element)

- Rock properties
- $\rho = 1760 \text{ kg/m}^3$
- $c_{\text{comp}} = 1880 \text{ m/s}$
- $c_{\text{shear}} = 767 \text{ m/s}$
- IE thickness 1.5 m from solid border

### Source:

- Monopole point source
- $F_0 = 1000 [\text{Hz}]$
- Single 10 Pa amplitude
- $\text{if}(t < T_0, A \cdot \sin(\omega_0 \cdot t), 0)$





# Computational Acoustics: Solid Mechanics

- Elastic waves in rocks propagate with a velocity that is given by elastic stiffnesses and the density ( $\rho$ ) of the solid material. (Fjær et al, 2008)
- Speed of sound of compressional wave ( $c_p$ ) and shear wave ( $c_s$ ) are defined based on the mechanical properties

$$c_p = \sqrt{\left(K + \frac{4}{3}G\right) / \rho}$$

Speed of sound of Shear Wave

$$c_s = \sqrt{G / \rho}$$

| DESCRIPTION              | VARIABLE    | $D(E, \nu)$   | $D(E, G)$                               | $D(K, G)$  | $D(\lambda, \mu)$                           |
|--------------------------|-------------|---|---|--|---|
| Young's modulus          | $E =$       | $E$   | $E$                                     | $\frac{9KG}{3K + G}$                             | $\mu \frac{3\lambda + 2\mu}{\lambda + \mu}$ |
| Poisson's ratio          | $\nu =$     | $\nu$   | $\frac{E}{2G} - 1$                      | $\frac{1}{2} \left(1 - \frac{3G}{3K + G}\right)$ | $\frac{\lambda}{2(\lambda + \mu)}$          |
| Bulk modulus             | $K =$       | $\frac{E}{3(1 - 2\nu)}$                             | $\frac{EG}{3(3G - E)}$                  | $K$  | $\lambda + \frac{2\mu}{3}$                  |
| Shear modulus            | $G =$       | $\frac{E}{2(1 + \nu)}$                              | $G$                                     | $G$  | $\mu$                                       |
| Lamé parameter $\lambda$ | $\lambda =$ | $\frac{E\nu}{(1 + \nu)(1 - 2\nu)}$                  | $\frac{G(E - 2G)}{3G - E}$              | $K - \frac{2G}{3}$                               | $\lambda$                                   |
| Lamé parameter $\mu$     | $\mu =$     | $\frac{E}{2(1 + \nu)}$                              | $G$                                     | $G$  | $\mu$                                       |
| Pressure-wave speed      | $c_p =$     | $\sqrt{\frac{E(1 - \nu)}{\rho(1 + \nu)(1 - 2\nu)}}$ | $\sqrt{\frac{G(4G - E)}{\rho(3G - E)}}$ | $\sqrt{\frac{K + 4G/3}{\rho}}$                   | $\sqrt{\frac{\lambda + 2\mu}{\rho}}$        |
| Shear-wave speed         | $c_s =$     | $\sqrt{\frac{E}{2\rho(1 + \nu)}}$                   | $\sqrt{G/\rho}$                         | $\sqrt{G/\rho}$                                  | $\sqrt{\mu/\rho}$                           |

$$CC(\tau) = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} a(t)b(t + \tau)dt$$

$$\rho^2(v, \tau) = \frac{\int_{t=0}^{T_w} \left[ \sum_{m=1}^M r_m \left[ t + \left( \frac{z_m}{v} \right) + \tau \right] \right]^2 dt}{\sum_{m=1}^M \int_{t=0}^{T_w} \left\{ r_m \left[ t + \left( \frac{z_m}{v} \right) + \tau \right] \right\}^2 dt}$$

$v$ : wave velocity, m/s

$\tau$ : time delay compared to the first wave arrival (m=1), s

$M$ : number of receivers

$T_w$ : time window, s

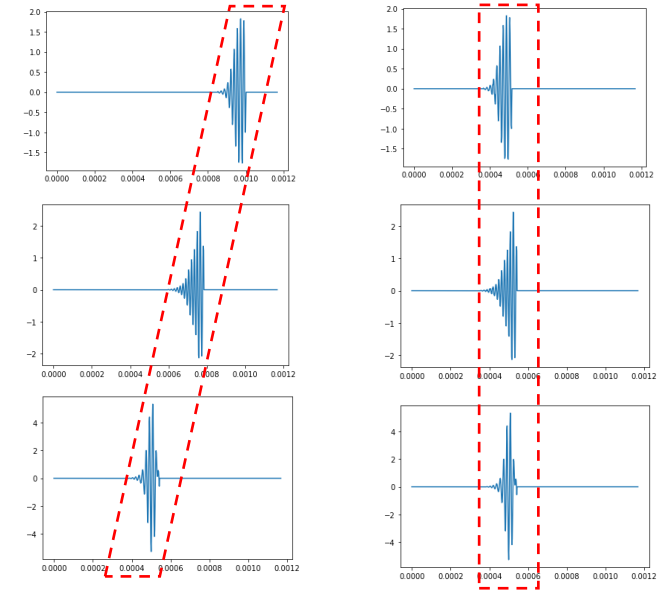
$r_m(t)$ : wave form recorded by receiver  $m$

$z_m$ : distance of receiver  $m$  from the first receiver, m

## Cross Correlation

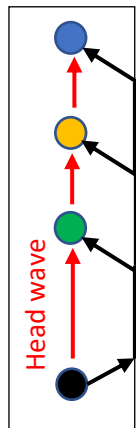
## Semblance

At each velocity, move-out correction is applied on the waveforms within the time window



## Wave velocities

Each time window is tested with a range of velocities.

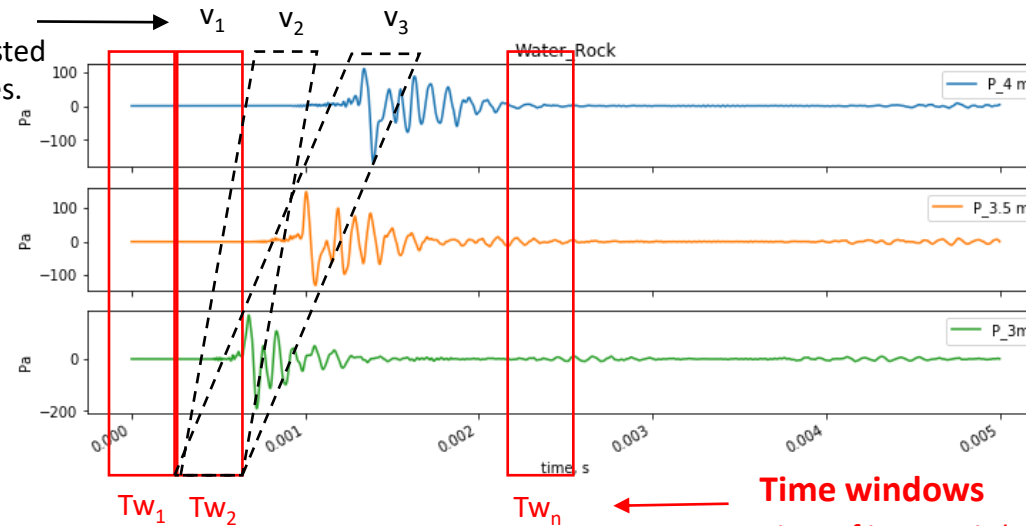


Receiver 3

Receiver 2

Receiver 1

Source



## Time windows

Time of interest is broken into several time windows.