



CCPC

Consortium for Computational
Physics and Chemistry

U.S. DEPARTMENT OF ENERGY
BIOENERGY TECHNOLOGIES OFFICE

CFP Regenerator Model Development

NETL Multiphase Workshop

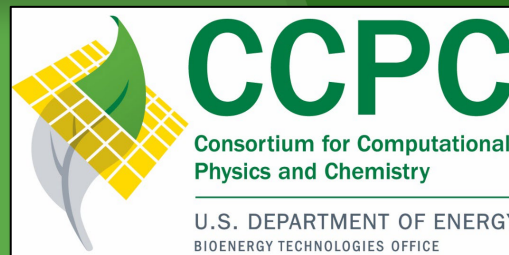
August 13-14, 2024

Bruce Adkins

Oak Ridge National Laboratory

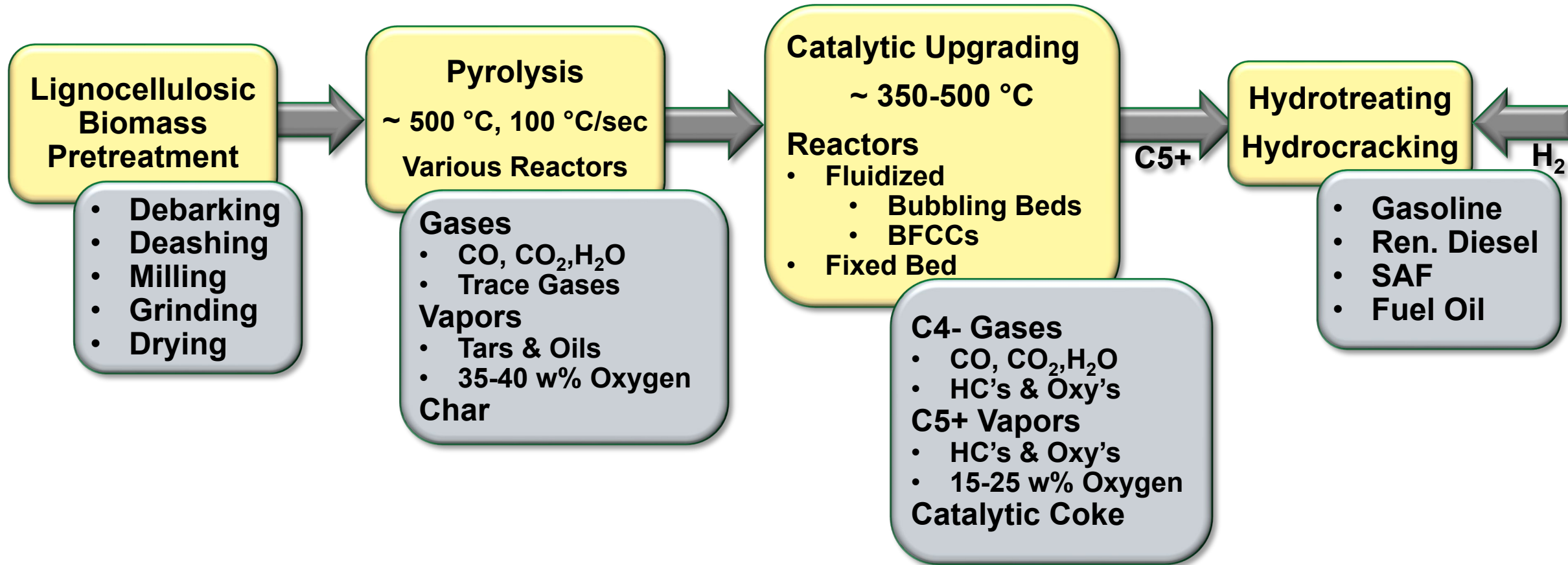
Yupeng Xu, Mehrdad Shahn timer and Jordan Musser

National Energy Technology Laboratory

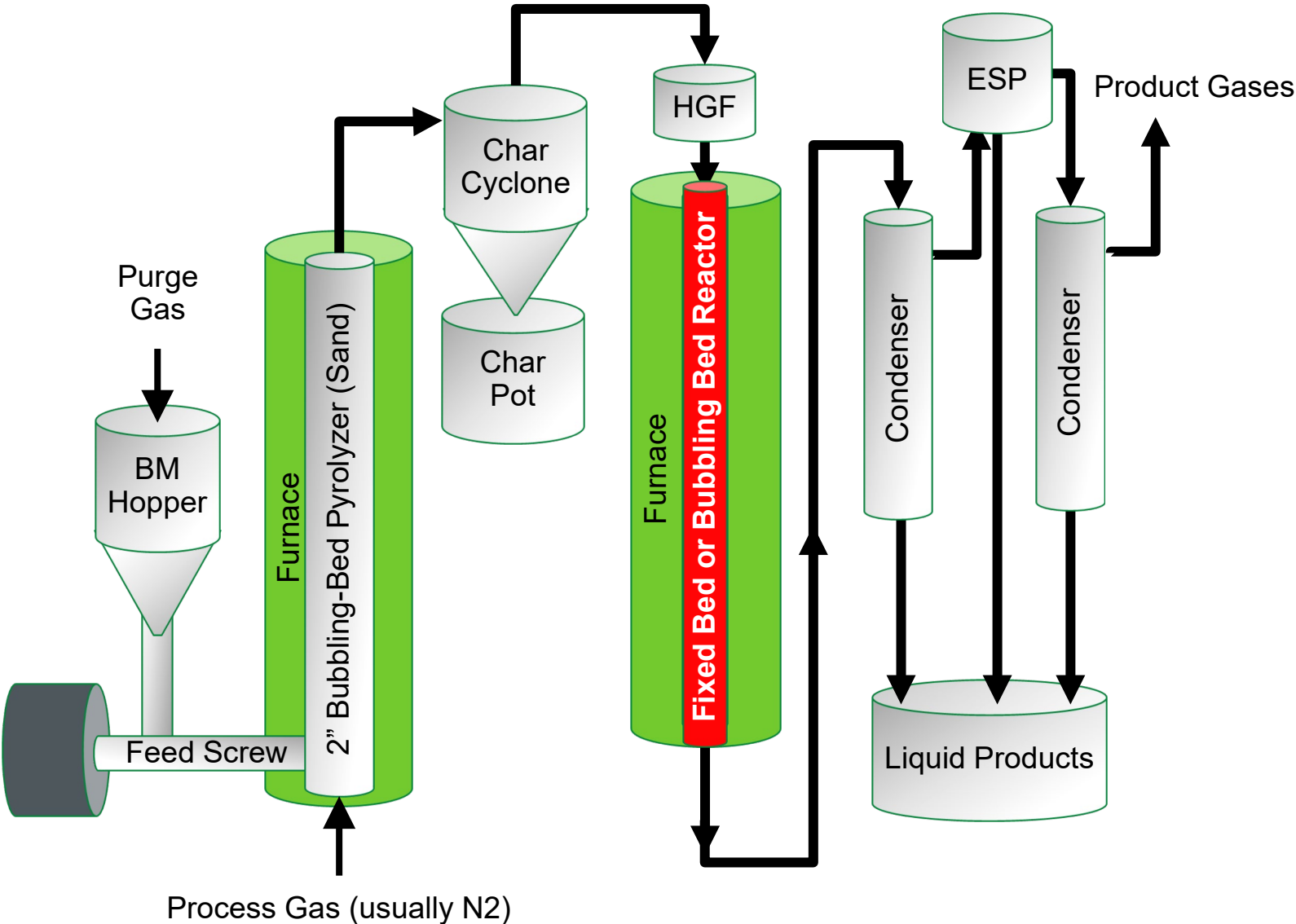


U.S. DEPARTMENT OF
ENERGY

Catalytic Fast Pyrolysis (CFP)



NREL's "2FBR": A Flexible CFP Unit



ZSM-5 Based Catalysts Used in 2FBR Bubbling-Bed Upgrader



**80% ZSM-5
20% Alumina**

**+/- P-promotion
(2.5 wt%)**

**Geldart B
D_p = 500 – 800 μm**

**Spent Catalyst:
9-13 wt% CoC
(Coke on Catalyst)**

1

Extensive laboratory characterization of coked catalyst: TPO, NMR, microscopy....

2

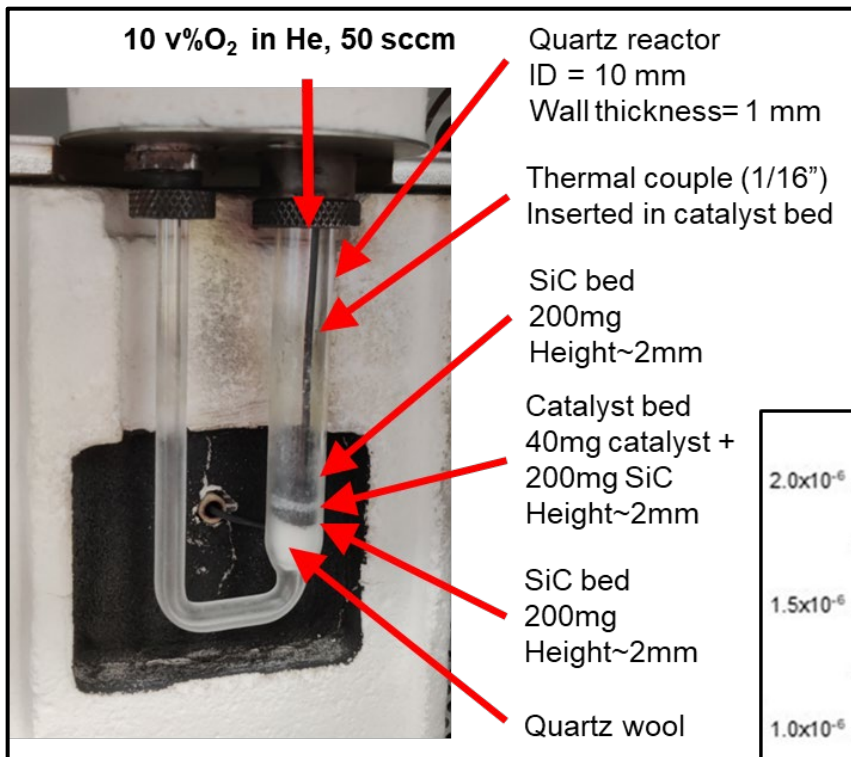
Develop kinetics for coke oxidation from TPO data using FEM fixed bed models

3

Extend to FCC catalyst, i.e. Geldart A particles with much lower CoC

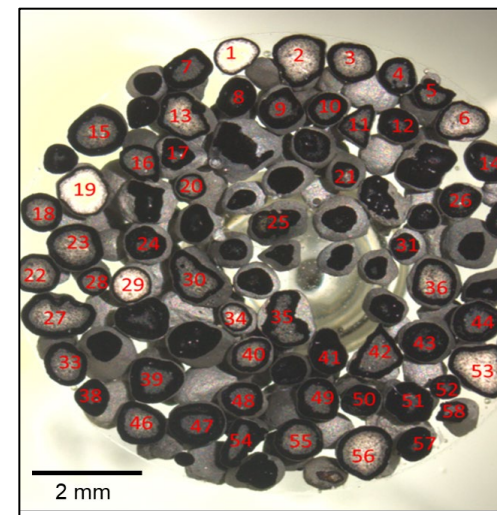
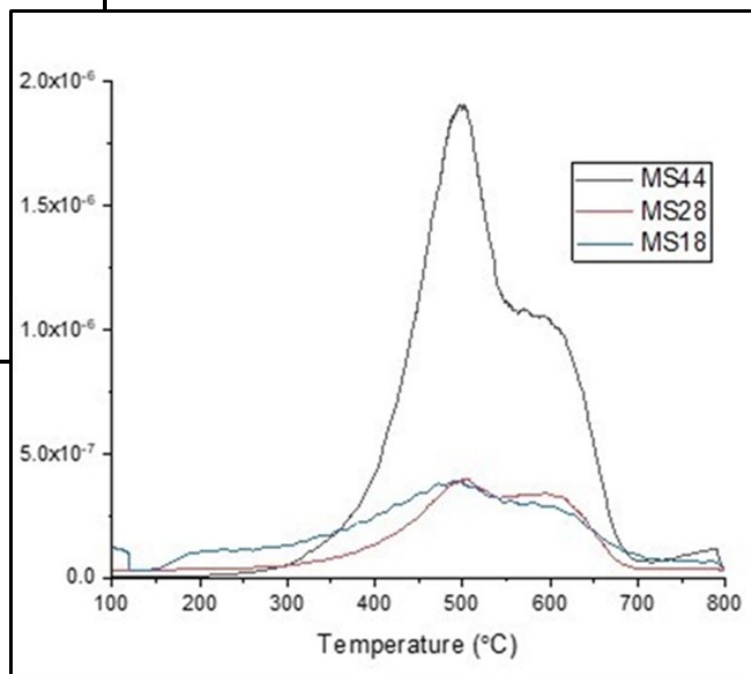
MODEL THE BFCC REGENERATOR

Coke Characterization and Combustion Behavior

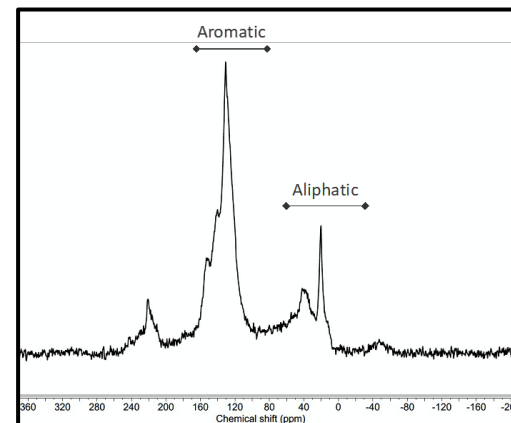


TPO: “Low” and “High” Temperature Carbon

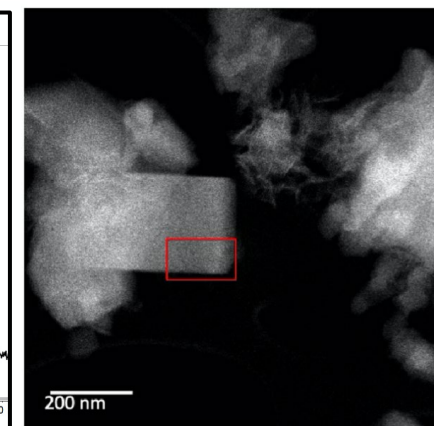
Whole Pellets (~600 μm)
vs Crushed (< 100 mesh)



¹³C-NMR



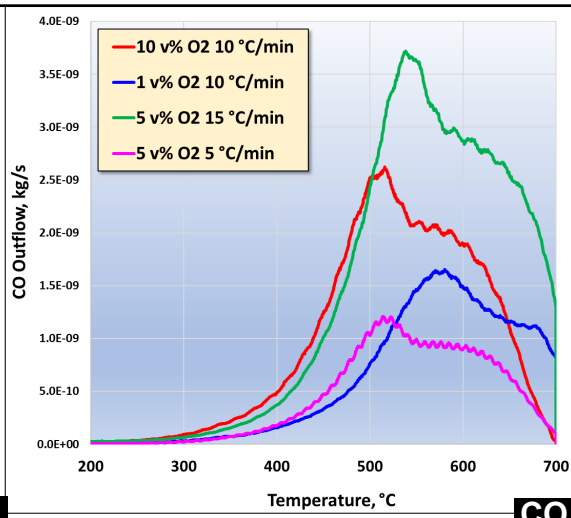
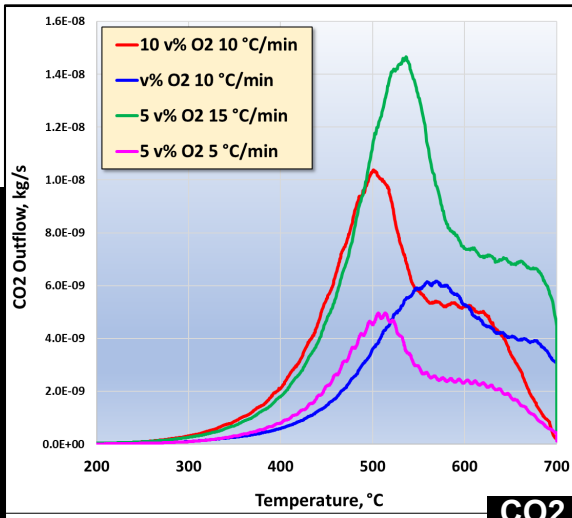
STEM-EELS



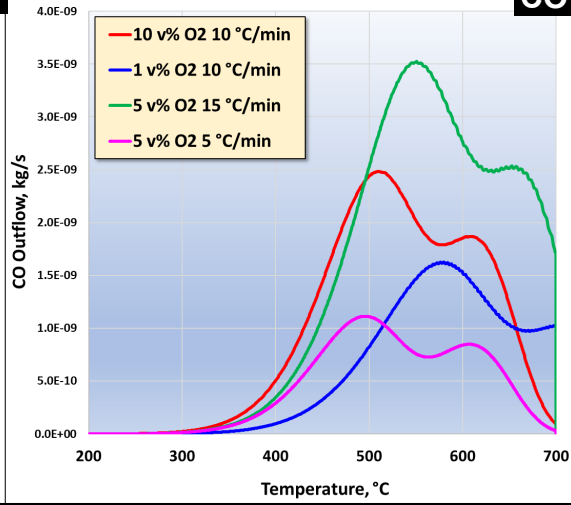
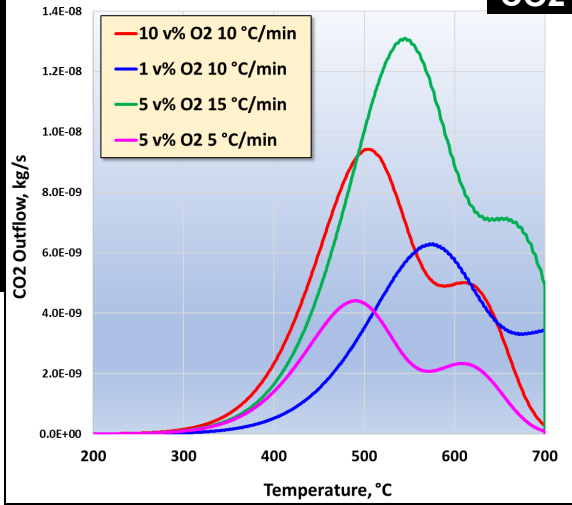
Consortia Acknowledgements:
CDM: Catalyst Deactivation Mitigation
ACSC: Advanced Catalyst Synthesis and Characterization

Quality of Fit: Four TPO Runs

Data



Model



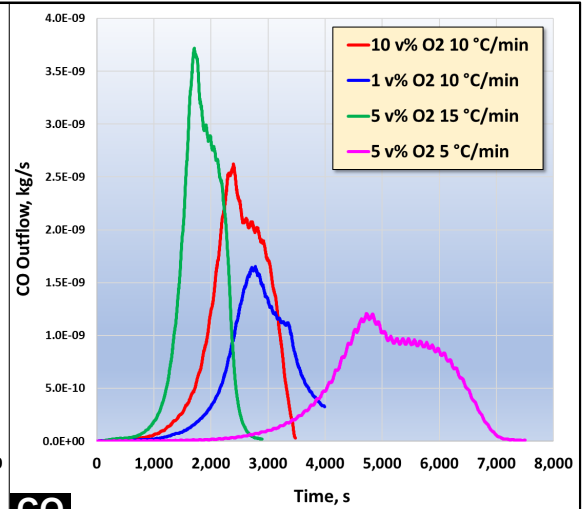
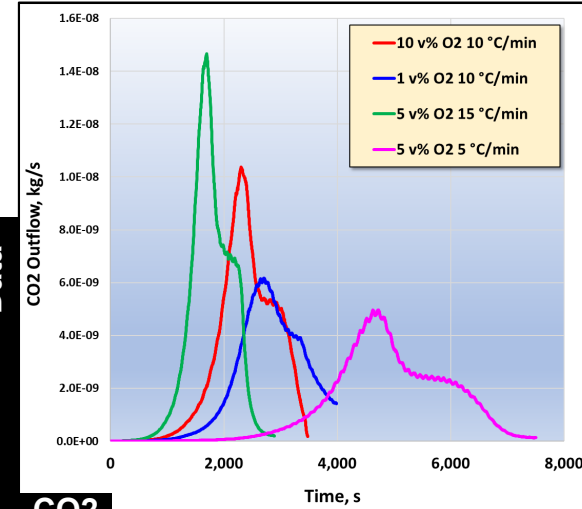
CO₂

CO

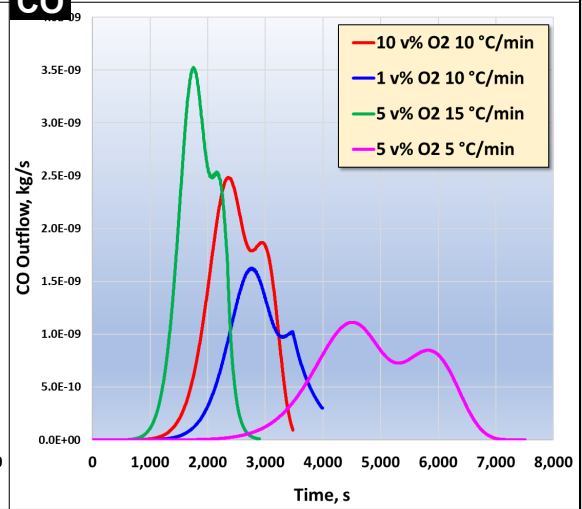
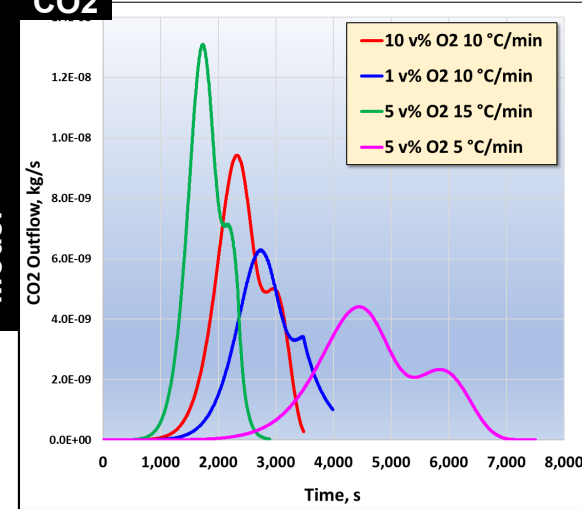
Temperature Domain

Crushed -100 Mesh

Data



Model



Time Domain

Unpromoted Catalyst Coke Combustion Kinetic Model

	Reaction	Rate Equation	Units
1	Low temperature CO ₂ formation on surface	$R_{CO2_low} = a_{CO2_low} cC_{low} cO_2^{b_{CO2_low}} e^{\frac{-Ea_{CO2_low}}{RT}}$	mol/(m ² .s)
2	High temperature CO ₂ formation on surface	$R_{CO2_hi} = a_{CO2_hi} cC_{hi} cO_2^{b_{CO2_hi}} e^{\frac{-Ea_{CO2_hi}}{RT}}$	
3	Low temperature CO formation on surface	$R_{CO_low} = a_{CO_low} cC_{low} cO_2^{b_{CO_low}} e^{\frac{-Ea_{CO_low}}{RT}}$	
4	High temperature CO formation on surface	$R_{CO_hi} = a_{CO_hi} cC_{hi} cO_2^{b_{CO_hi}} e^{\frac{-Ea_{CO_hi}}{RT}}$	
5	CO oxidation	$R_{CO_CO2} = a_{CO_CO2} \rho_p cCO cO_2^{b_{CO_CO2}} e^{\frac{-Ea_{CO_CO2}}{RT}}$	mol/(m ³ .s)

1. Pool the CO and CO₂ outflow data from TPO runs and fit model parameters using a “0D” (gradientless) spreadsheet model and SOLVER
2. Use 2D full-gradient COMSOL FEM model to adjust the CO oxidation constant to account for mass and heat transfer effects in catalyst particles and in bed

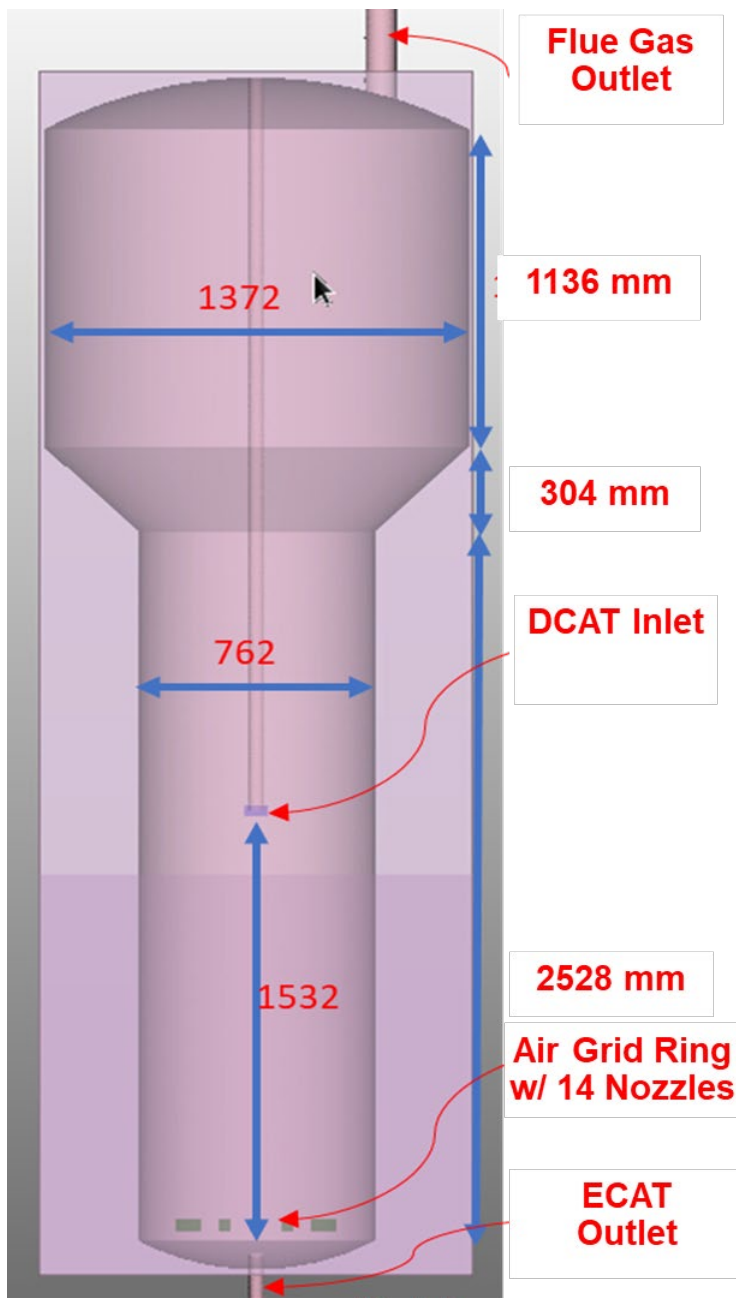
Parameter	Units	Value
a_{CO_CO2}	m ³ /(kg.s)	0.2925
a_{CO2_low}	1/s	1,087
a_{CO2_hi}		5,102
a_{CO_low}		33,881
a_{CO_hi}		594,715
b_{CO_CO2}	-	0.0695
b_{CO2_low}		0.5384
b_{CO2_hi}		0.4793
b_{CO_low}		0.6650
b_{CO_hi}		0.9739
Ea_{CO_CO2}	J/mol	14,680
Ea_{CO2_low}		88,103
Ea_{CO2_hi}		118,987
Ea_{CO_low}		109,677
Ea_{CO_hi}		143,340

Translate Model to Barracuda: 80 μm BFCC Particles with 1 wt% CoC

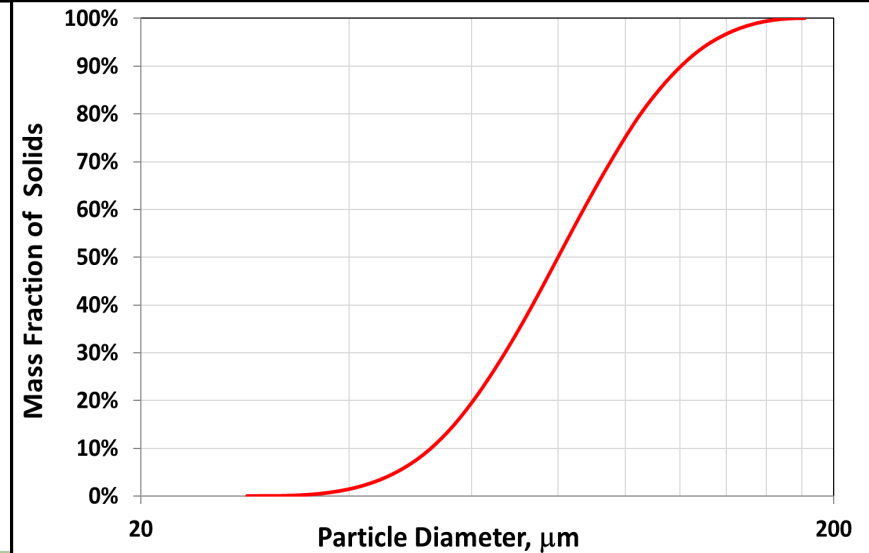
- Assume the coke profile inside the 80 μm particle is uniform
→ AVOID MODELING THE PARTICLE INTERIORS
 - The 80% ZSM-5, 20% Al₂O₃ formulation is too high in Z/M (too many active sites and too low in mesoporosity: Thiele number is too high). This very likely leads to the core-shell coke profile. THE REAL BFCC CATALYST SHOULD HAVE LOWER Z/M!!!
- Convert reaction expressions to volume concentrations (mass/volume) instead of surface concentrations (mass/area)
 - Used the “single particle in one grid cell” method to validate the conversions

Parameter	Units	COMSOL	Barracuda
$a_{\text{CO}_2_{\text{CO}_2}}$	m ³ /(kg.s)	0.2925	0.6107
$a_{\text{CO}_2_{\text{low}}}$	1/s	1,087	90,689
$a_{\text{CO}_2_{\text{hi}}}$		5,102	425,663
$a_{\text{CO}_{\text{low}}}$		33,881	2.827E+06
$a_{\text{CO}_{\text{hi}}}$		594,715	4.962E+07
$b_{\text{CO}_2_{\text{CO}_2}}$	-	0.0695	
$b_{\text{CO}_2_{\text{low}}}$		0.5384	
$b_{\text{CO}_2_{\text{hi}}}$		0.4793	
$b_{\text{CO}_{\text{low}}}$		0.6650	
$b_{\text{CO}_{\text{hi}}}$		0.9739	
$Ea_{\text{CO}_2_{\text{CO}_2}}$	J/mol	14,680	
$Ea_{\text{CO}_2_{\text{low}}}$		88,103	
$Ea_{\text{CO}_2_{\text{hi}}}$		118,987	
$Ea_{\text{CO}_{\text{low}}}$		109,677	
$Ea_{\text{CO}_{\text{hi}}}$		143,340	

BFCC Regenerator: 5 mTPD Demo Unit



Fixed Parameter	Units	Value
Biomass Feedrate	mT/day	5.0
Catalyst Circ Rate	(dry basis)	45.0
Catalyst/Biomass	-	9.0
Coke Yield	wt%	9.0
DCAT Coke on Catalyst (CoC)		1.00
DCAT CoC "Low" Form	wt%	0.61
DCAT CoC "High" Form		0.39
Base Catalyst Inventory	kg	325
Stoichiometric Airflow	kg/s	0.06
Nominal Pressure	kPa	274
Catalyst Particle Density	kg/m ³	1,380

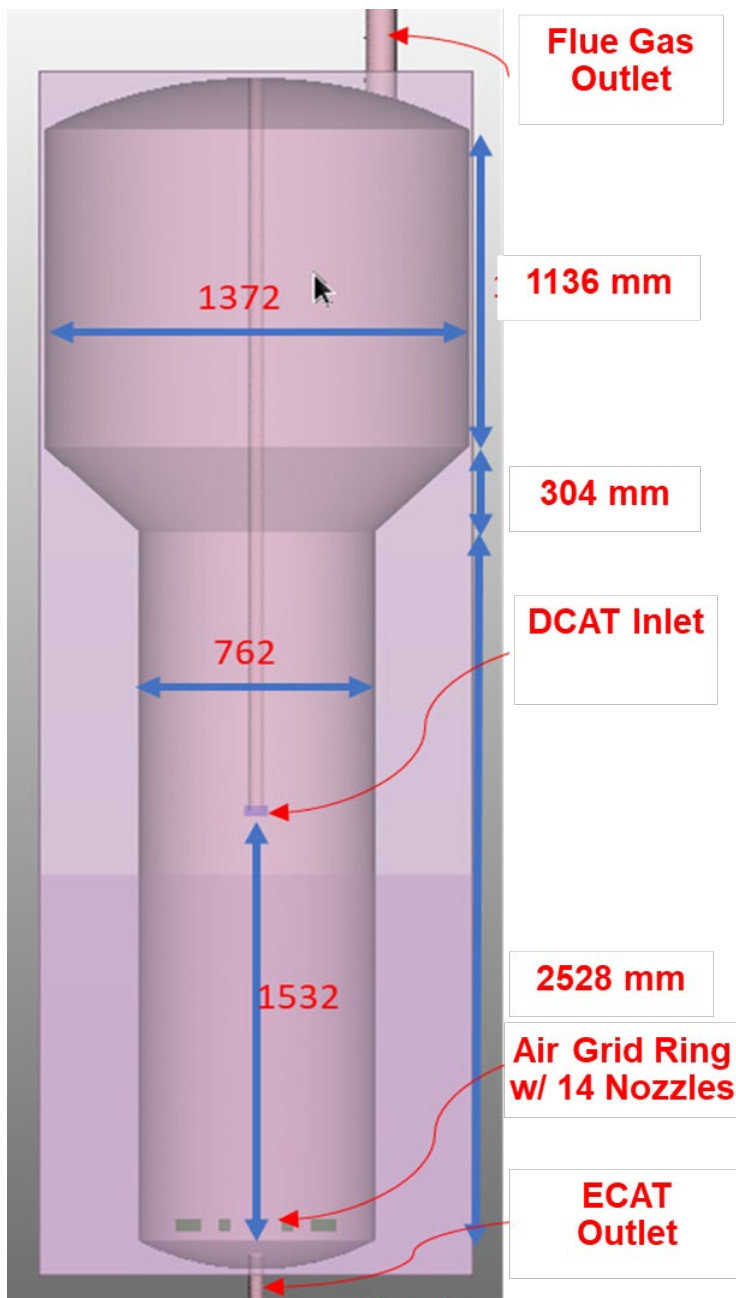


Variables Studied

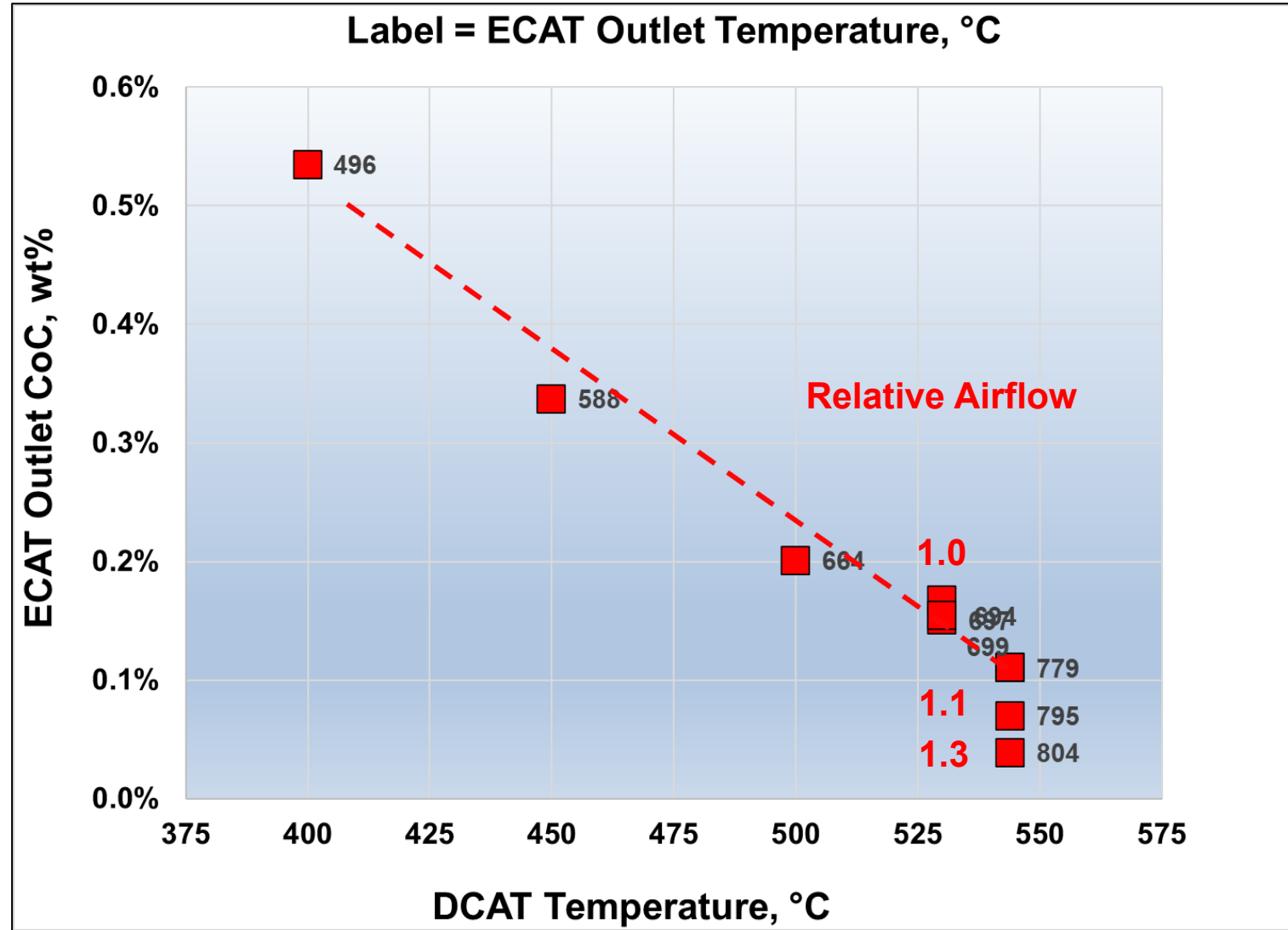
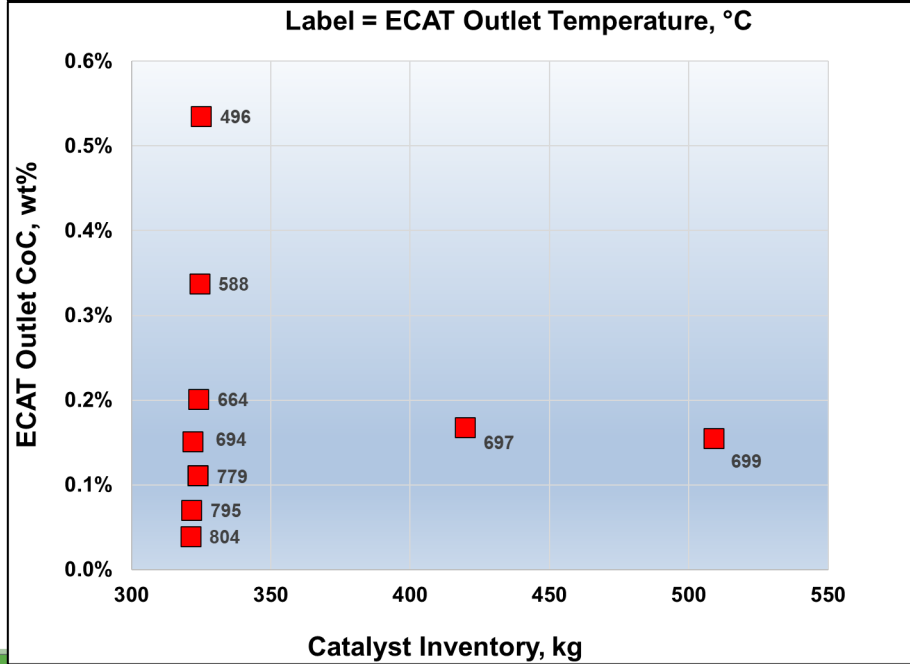
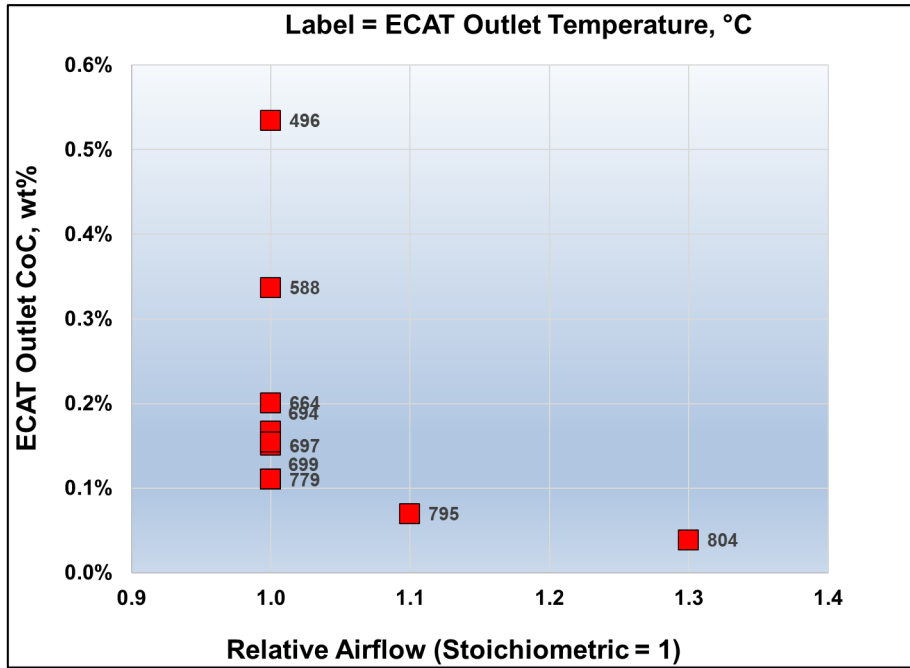
Variables	Units	Range
Relative Airflow (Stoichiometric = 1)	-	1.0, 1.1, 1.3
Relative Catalyst Inventory (Base = 1)		1.0, 1.3, 1.6
DCAT Temperature <i>Effect of Riser Outlet Temp (ROT) and/or catalyst cooler</i>	°C	450, 500, 530, 544

Important Outputs

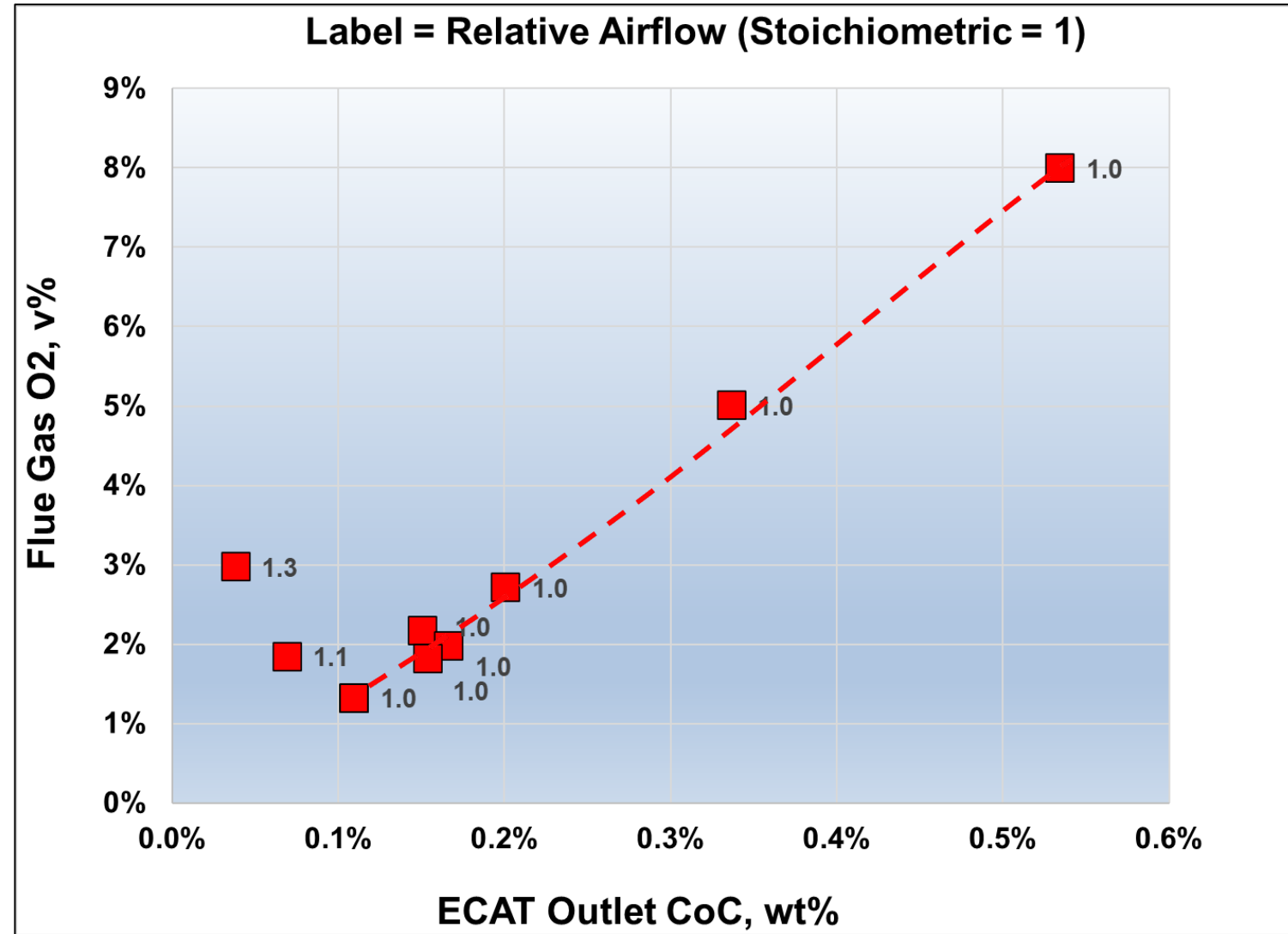
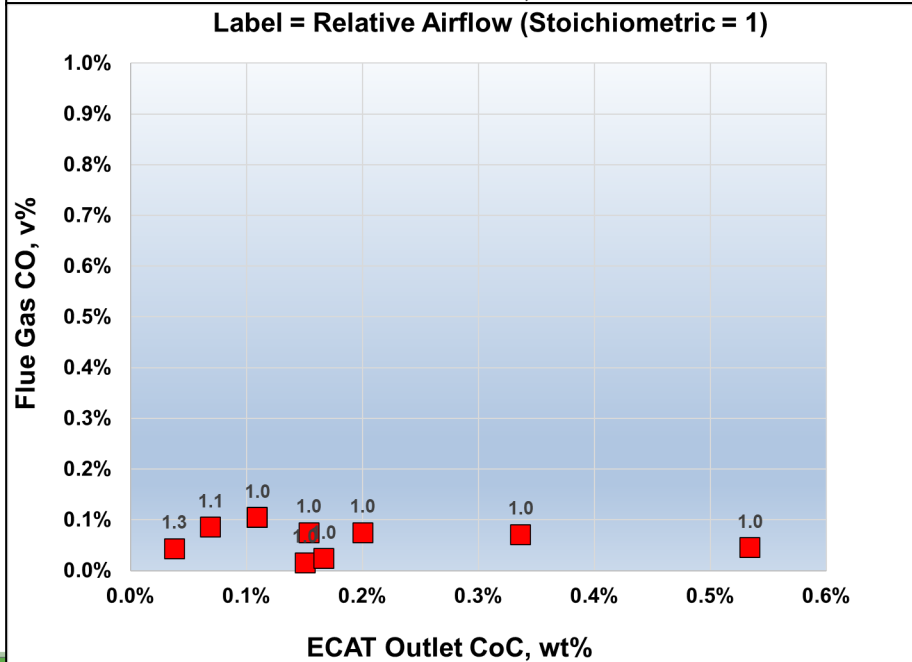
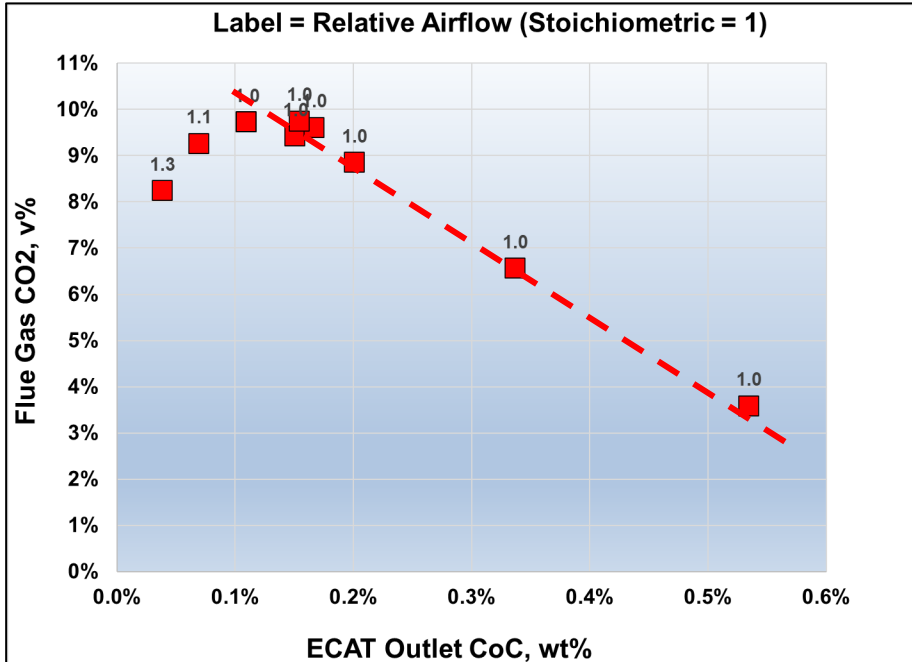
Variables	Units	Significance
ECAT CoC	wt%	Sets the activity of the catalyst returning to the riser
Flue Gas CO	v%	An indication of the potential for afterburn (CO combustion in freeboard)



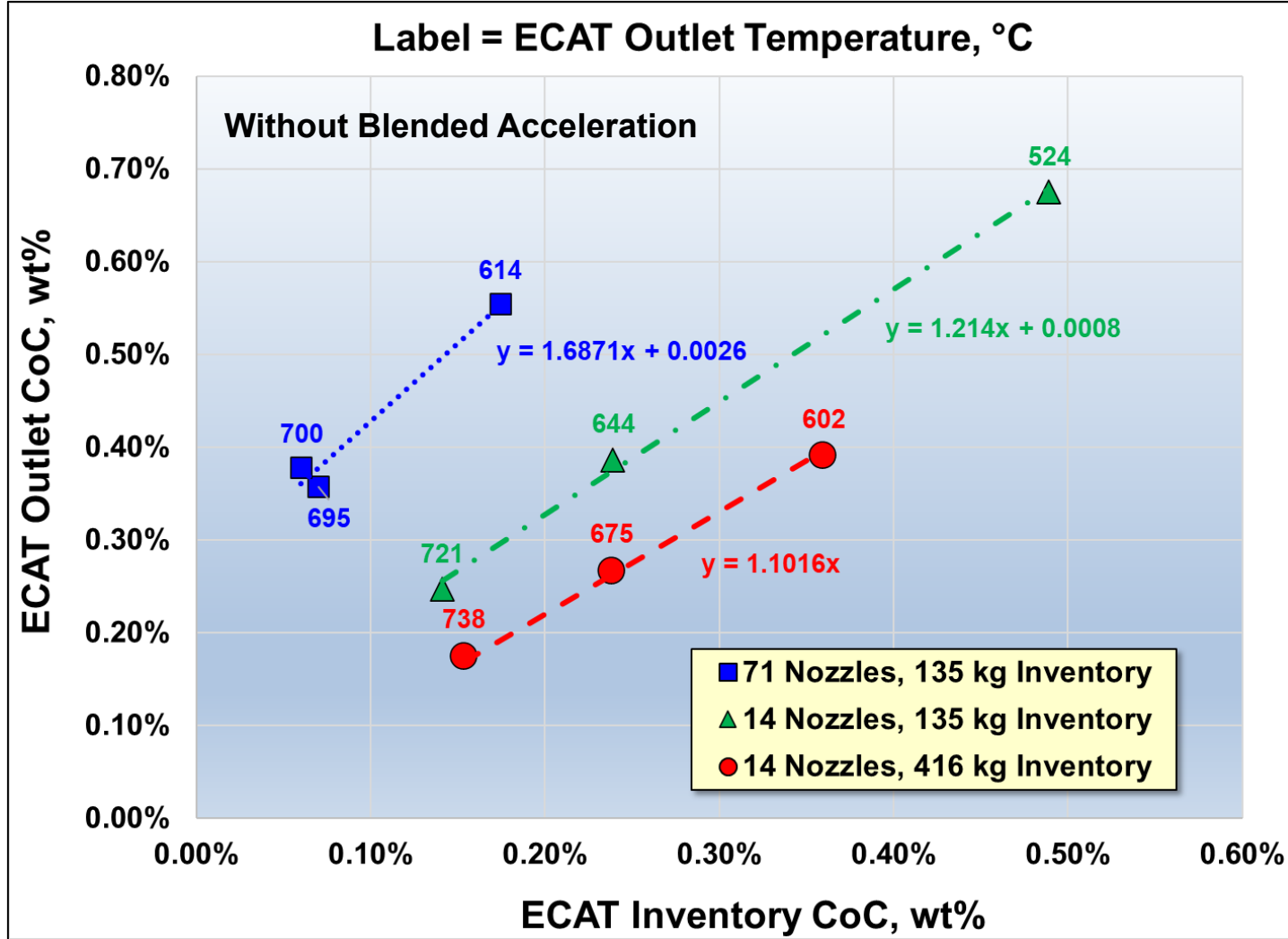
ECAT Carbon on Catalyst (CoC)



Flue Gas Composition



Catalyst Flow Segregation



The Blended Acceleration Model

P. J. O'Rourke and D. M. Snider. A new blended acceleration model for the particle contact forces induced by an interstitial fluid in dense particle/fluid flows. *Powder Technology*, 256(): 39–51, 2014

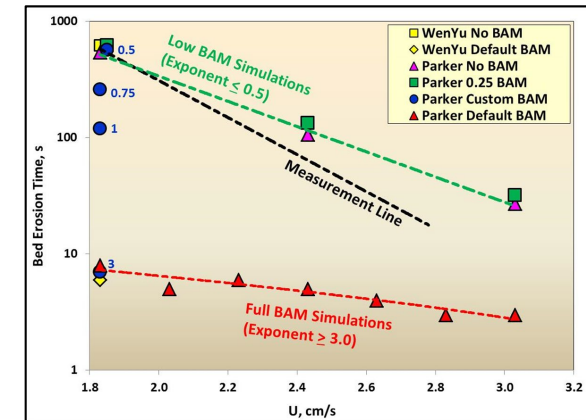
Weighting parameter for blending the MP-PIC and average particle accelerations:

$$wt_{frac} = 1 - (1 - \theta_p / \theta_{p,cp})^n$$

Default value is $n = 6$

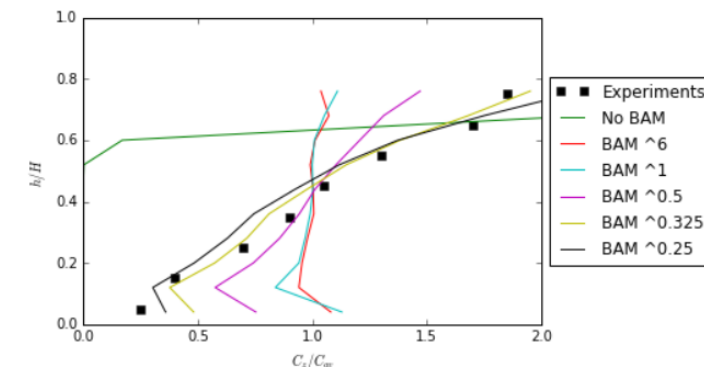
Mixing of Biomass and FCC Catalyst

Adkins and Kapur, *Barracuda Users Conference (2015)*



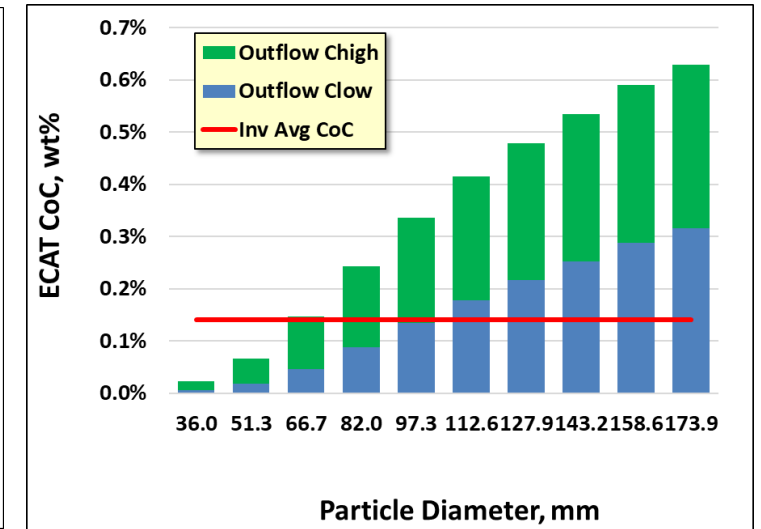
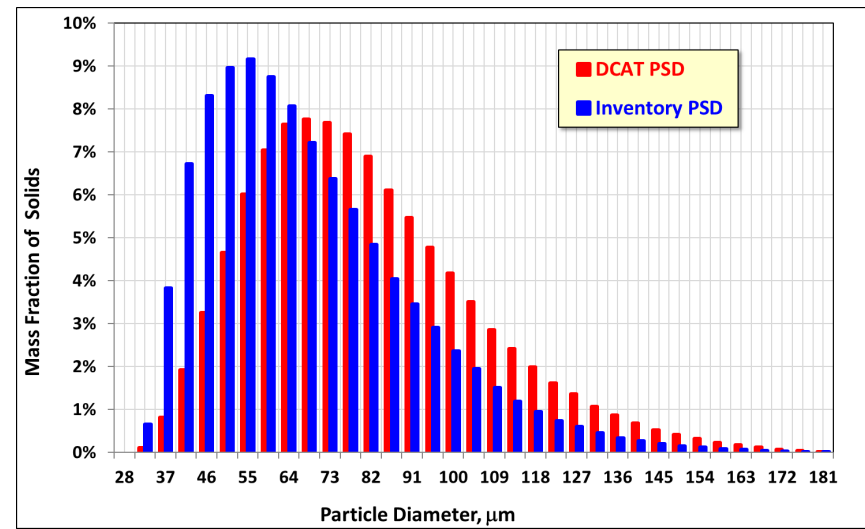
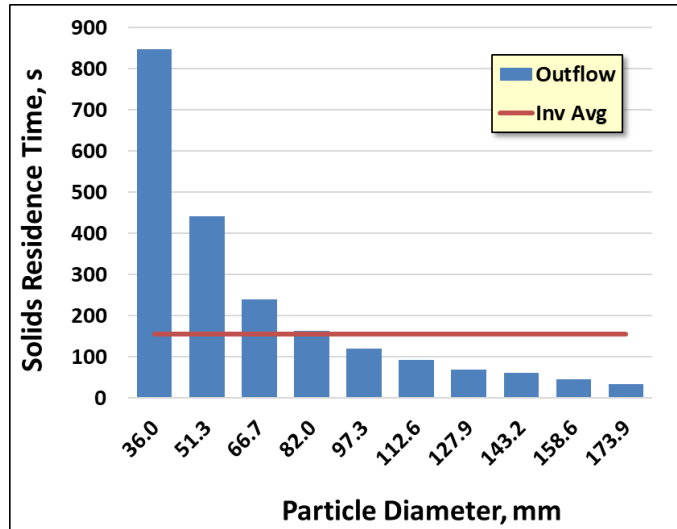
Mixing of Coal Char and Sand

Zhang et al, *Powder Technology*, 228(): 206-209, 2012

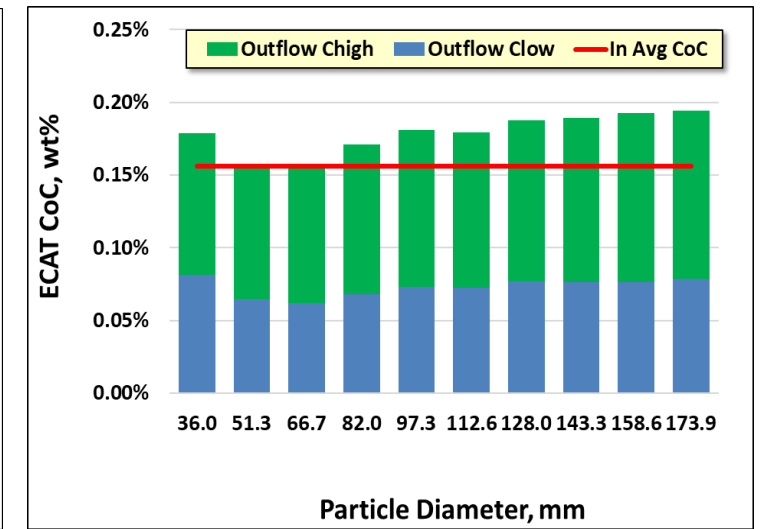
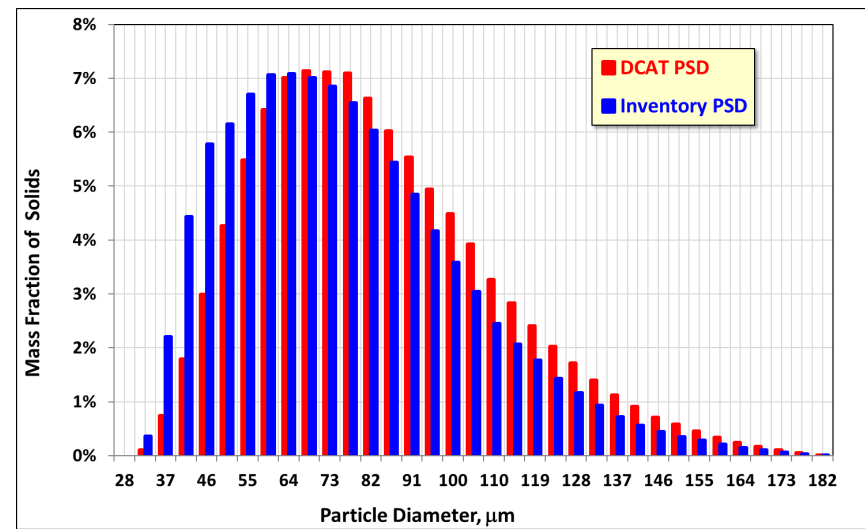
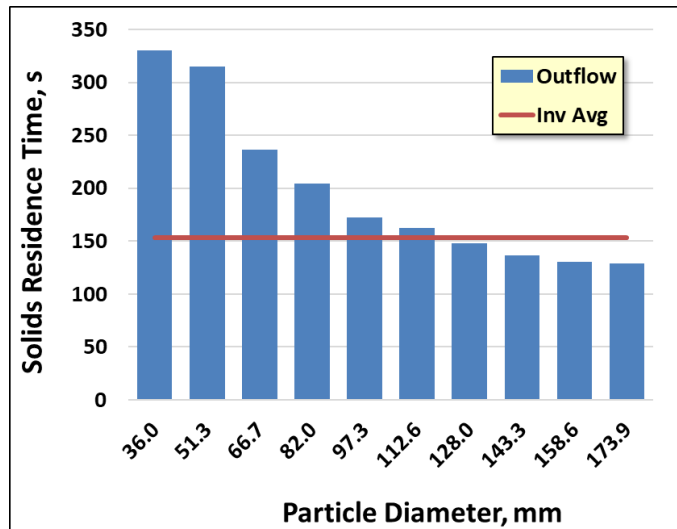


Effect of Blended Acceleration (n = 6)

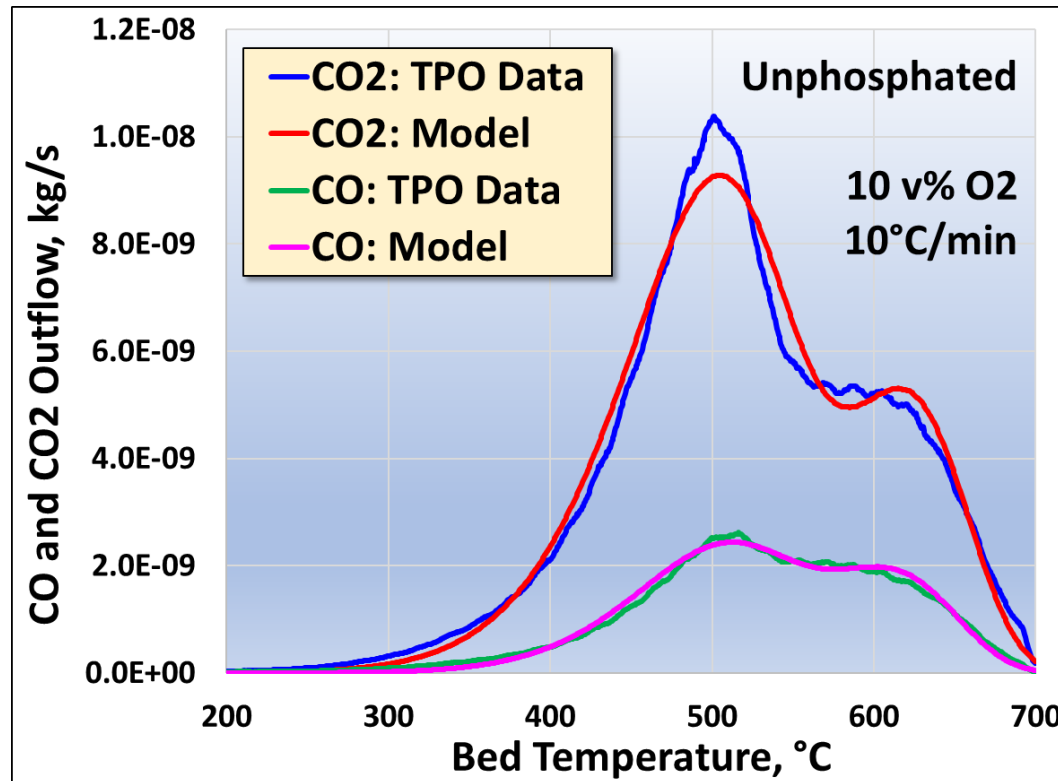
No Blended Acceleration



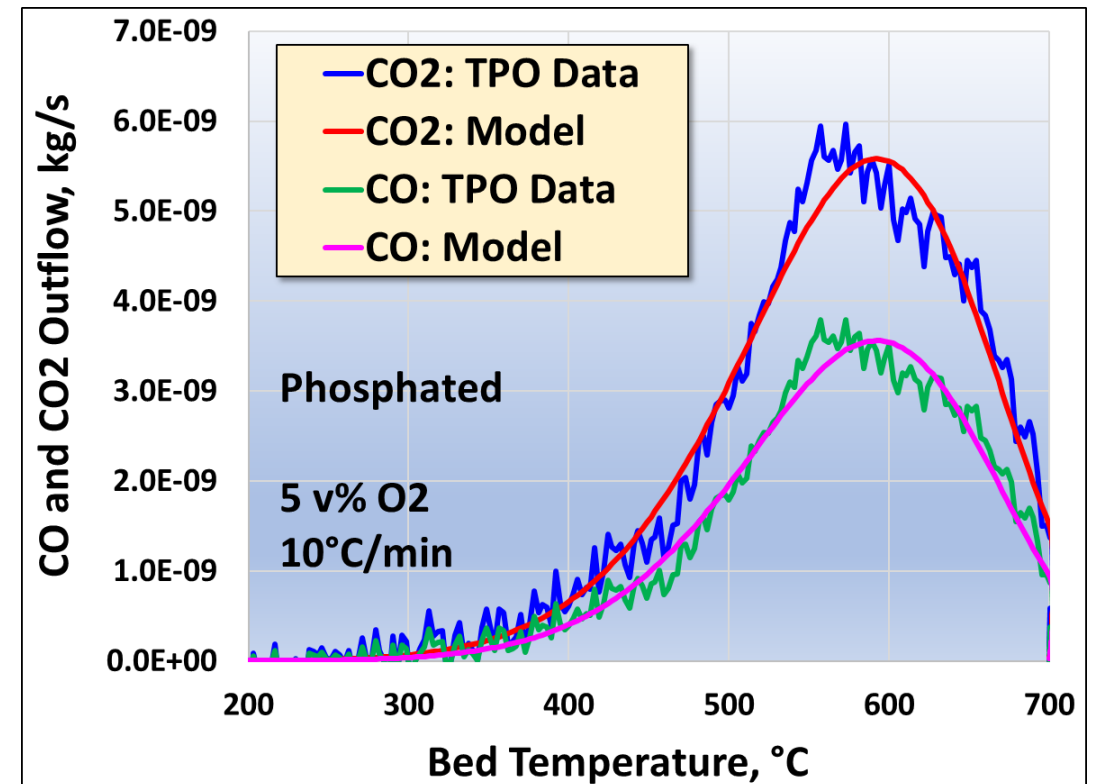
Blended Acceleration (n = 6)



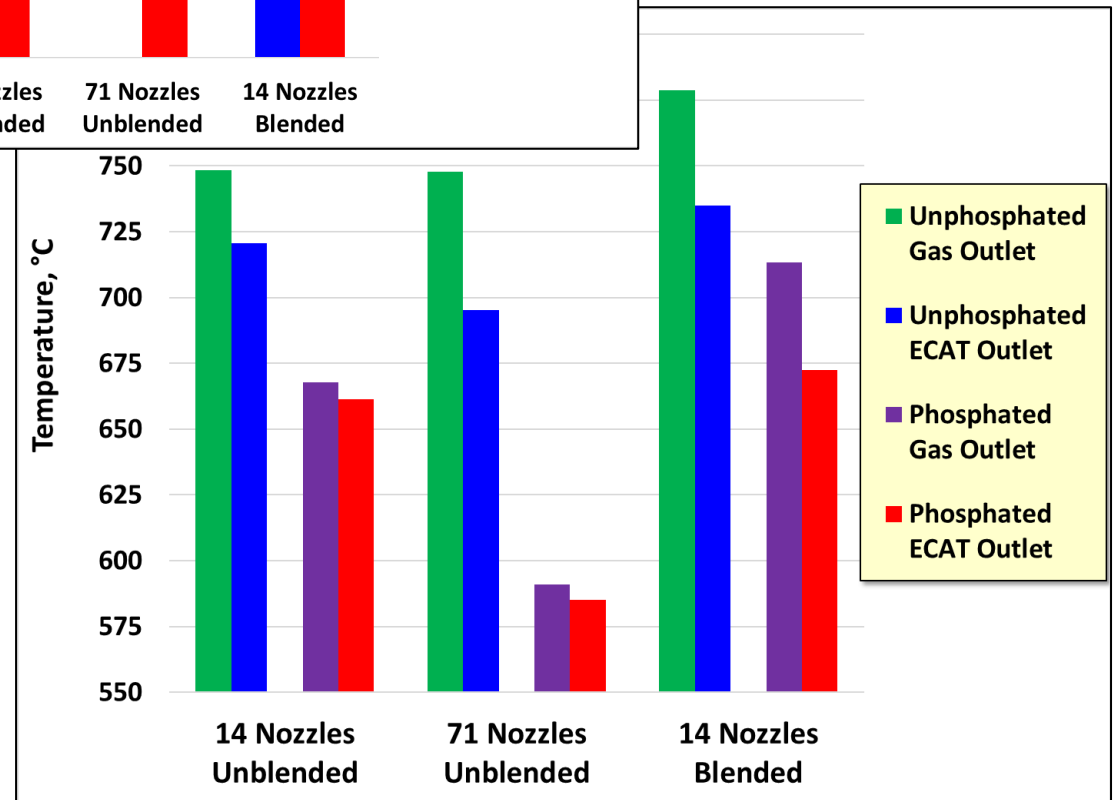
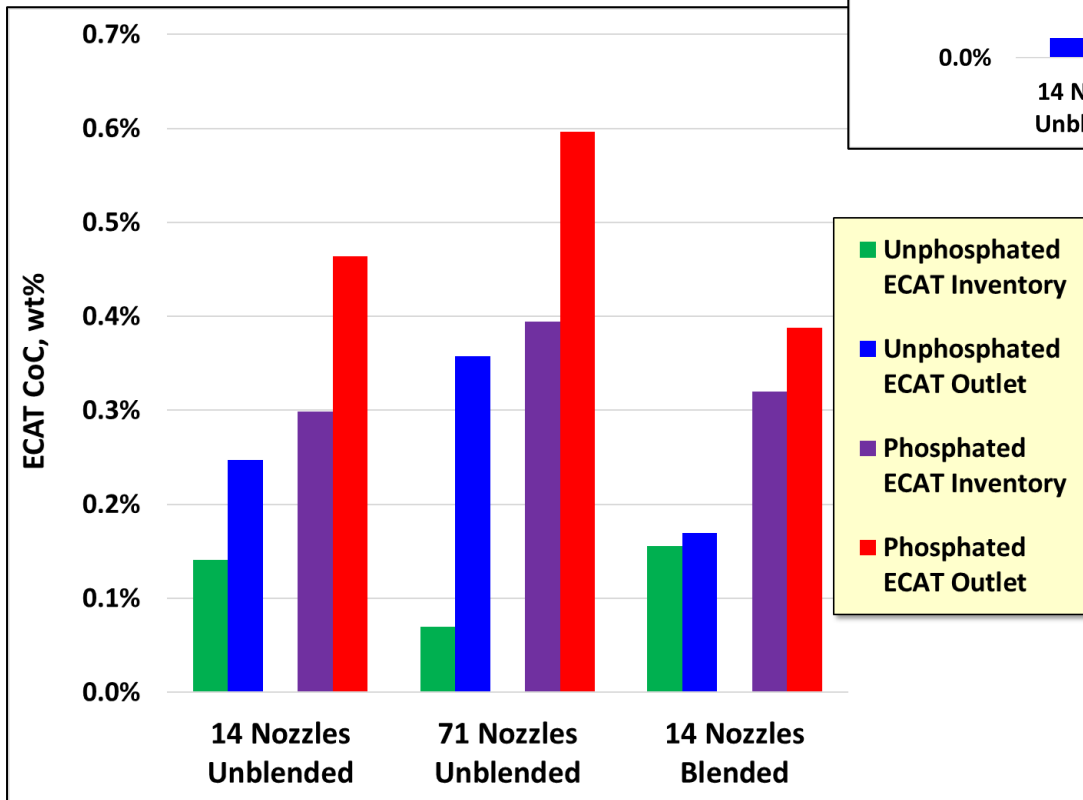
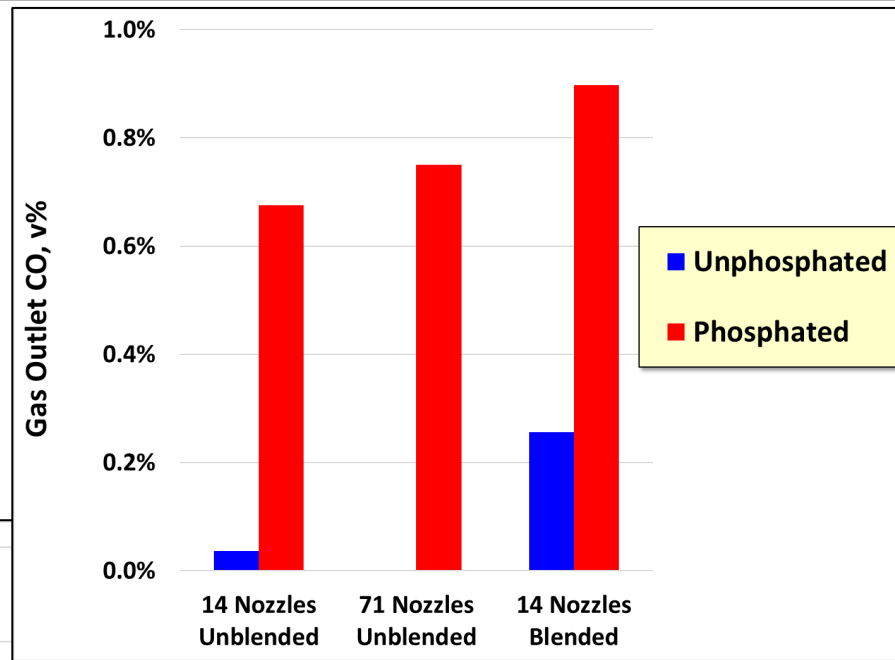
Effect of Phosphation



Parameter	Units	Value
a_{CO_CO2}	m ³ /(kg.s)	0.1852
a_{CO2}	1/s	40.851
a_{CO}		171.58
b_{CO_CO2}	-	0.06993
b_{CO2}		0.6776
b_{CO}		1.0
Ea_{CO_CO2}	J/mol	20,729
Ea_{CO2}		76,029
Ea_{CO}		83,117



135 kg Inventory DCAT Temperature 580°C



Conclusions

- **Unphosphated catalyst**

- Initial results indicate that excessively high temperatures ($\geq 780^{\circ}\text{C}$) could be needed to reduce ECAT CoC below 0.1 wt%.
 - Tradeoff: ECAT activity vs long-term hydrothermal deactivation of zeolite (also activity)
 - Full analysis should include the complete heat balance
- At demo scale (5 mTPD) risk of afterburn is low
 - Need to consider commercial scale

- **Phosphated catalyst**

- Combustion behavior is different! Higher CO/CO₂ ratio, lower regenerator temperatures, higher ECAT CoC → Needs higher DCAT temperature
- More TPO data needed at other O₂ levels

- **Segregating Flow**

- Segregating flow is very important to regenerator performance
- Data needed!

Acknowledgements



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